## COSSORSCOPES



## MANUAL

FOR
COSSORSCOPES
Model 2000
AND

## Model 2100

Continuous development may result in minor changes to design.

## COSSOR INSTRUMENTS LIMITED

The Instrument Company of the Cossor Group: a subsidiary of the Raytheon Company, U.S.A.
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## Changes to the Manual for

## Model 2000 and Model 2100

Page 25 Bcfore INITIAL SETTING OF CONTROLS, insert new Section:
RESETTING CONTROLS WHEN CRT IS REPLACED.
Whenever a new CRT is fitted to Model 2000 or Model 2100, carry out the procedures given on pages 26 and 27, starting from 'Position the Trig. Selector switch to EXT. $\div$. Feed sharp ...'(para. 4) and continuing to the end of the procedure for Time Calibration.
Page 28 Y AMPLIFIERS Delete second and third paragraphs. Substitute:
Position the $\mathrm{Y} 1 \mathrm{~V} / \mathrm{cm}$ switch at $\cdot 001 \mathrm{~V} / \mathrm{cm}$. Reduce the amplitude of the $1 \mathrm{kc} / \mathrm{s}$ signal to $5 \mathrm{mV} \cdot 1.1^{\circ}{ }_{0}$ peak-to-peak. On Model 2000 adjust RV103 and on Model 2100 adjust RV102 to obtain maximum amplitude of the display. Return the Yl A.C.-D.C.-CAL. switch to the D.C. position and rotate the Y1 GAIN (SET CAL.) control to obtain a trace of 5 cm . Position the A.C.-D.C.-CAL. switch at CAL.

On Model 2000, adjust RV102 to obtain a trace of 3 cm ; on Model 2100, ensure that the displaycd trace is $3 \mathrm{~cm}!1 \mathrm{~mm}$. Position the $\mathrm{Y} 1 \mathrm{~V} / \mathrm{cm}$ switch at $\cdot 01 \mathrm{~V} / \mathrm{cm}$ and increase the amplitude of the $1 \mathrm{kc} / \mathrm{s}$ signal to $50 \mathrm{mV} \pm 1^{\circ}$, peak-to-peak. Return the Y/ A.C.-D.C.-CAL. switch to the D.C. position and rotate the Y/ GAIN (SET CAL.) control to obtain a trace of 5 cm . Position the A.C.-D.C.-CAL. switch at CAL.

On Model 2000, do not alter the setting of RV103 but, if necessary, adjust RV102 to obtain a trace of $3 \mathrm{~cm}=1 \mathrm{~mm}$ and to balance out differences between the $\cdot 001 \mathrm{~V} / \mathrm{cm}$ and $\cdot 01 \mathrm{~V} / \mathrm{cm}$ positions. On Model 2100, do not alter the setting of RV102 but ensure that the displayed trace is $3 \mathrm{~cm}: 1 \mathrm{~mm}$.
Position the Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switches at $\cdot 1 \mathrm{~V} / \mathrm{cm}$ and the Y 1 and $\mathrm{Y} 2 \mathrm{~A} . \mathrm{C} .-\mathrm{D} . \mathrm{C} .-\mathrm{CAL}$. switches at CAL. Carry out the same procedure for the Y2 amplifier, as given above for the Y1 amplifier ( $\cdot 1 \mathrm{~V} / \mathrm{cm}$ position).
Position the $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switch at $\cdot 001 \mathrm{~V} / \mathrm{cm}$ and $\cdot 01 \mathrm{~V} / \mathrm{cm}$, in turn, and carry out the procedure given above for the corresponding positions of the Y1 V/cm switch. For these positions, adjust RV202 for RV103 on Model 2000, and RV202 for RV102 on Model 2100, in order to obtain maximum amplitude of the display.

## CIRCUIT COMPONENTS

Page
50 Model 2000 Delete R117 and R118.
51 Model 2000 Delete R217 and R218.
52 Model 2000 Add R332 $68 \mathrm{k} \Omega$ 上 $10 \%{ }_{\circ} 0 \cdot 5 \mathrm{~W}$ ITB. $3507 / \mathrm{BTS} / 68310$.
58 Model 2000 After RV102, add: RV103 $4.7 \mathrm{k} \Omega-20 \% 0 \cdot 25 \mathrm{~W}$ ISB. 8034.
After RV201, add: RV202 $4.7 \mathrm{k} \Omega+20^{\circ}{ }_{6} 0.25 \mathrm{~W}$ ISB. 8034 .
59 Model 2000 Delete V306, V307 and V308.
61 Model 2100 Delete R117 and R118.
62 Model 2100 Delete R217 and R218.
63 Model 2100 Add R332 $68 \mathrm{k} \Omega+10^{\circ} 0.5 \mathrm{~W}$ ITB. $3507 / \mathrm{BTS} / 68310$.
Against R441, amend details to read $10 \mathrm{k} \Omega=10^{\circ}{ }_{0} 0.5 \mathrm{~W}$ ITB. $3507 / \mathrm{BTT} / 10310$.
68 Model 2100 Add C330 1000 pF 500 V ITB. $6044 / 5$.
69 Model 2100 After RV101, add: RV102 $4.7 \mathrm{k} \Omega \pm 20^{\circ}{ }_{\circ} 0.25 \mathrm{~W}$ ISB. 8034.
After RV201, add: RV202 $4.7 \mathrm{k} \Omega+20^{\circ} 0.25 \mathrm{~W}$ ISB. 8034 .
70 Model 2100 Delete V307, V308 and V309.
71 Model 2100 Amend the Part Number of MR313 to read: ITB. 9015.
CIRCUIT DIAGRAMS

Y| Amplifier (Model 2000)
Delete R117 and R118 in the cathode circuit of V101B and insert pre-set potentiometer RV102, 4.7 K, between the cathode of V101B and earth. Take the wiper of RV103 to R111.

Interchange the pin numbers of the A and B halves of V102.
Amend $\mathrm{Y}^{\prime} 1$ and $\mathrm{Y}^{\prime} 2$ to read $\mathrm{Y}^{\prime \prime} 1$ and $\mathrm{Y}^{\prime \prime} 2$.
Y2 Amplifier (Model 2000)
Add connexion from positive plate of C 219 and annotate this connexion: V300, pin 3.
Delete R217 and R218 in the cathode circuit of V201B and insert pre-set potentiometer RV202, 4.7 K , between the cathode of V201B and earth. Take the wiper of RV202 to R211.

Interchange the pin numbers of the A and B halves of V202 for the grids and cathodes only.
Amend $Y^{\prime \prime} 1$ and $Y^{\prime \prime} 2$ to read $Y^{\prime} 1$ and $Y^{\prime} 2$.
Y1 Amplifier (Model 2100)
Delete R117 and R118 in the cathode circuit of V101B and insert pre-set potentiometer RV102, 4.7 K , between the cathode of V101B and earth. Take the wiper of RV102 to R111.

Interchange the pin numbers of the A and B halves of V102.
Y2 Amplifier (Model 2100)
Delete R217 and R218 in the cathode circuit of V201B and insert pre-set potentiometer RV202, $4 \cdot 7 \mathrm{~K}$, between the cathode of V201B and earth. Take the wiper of RV202 to R211.
Interchange the pin numbers of the A and B halves of V202 for the grids and cathodes only.
Amend $Y^{\prime} 1$ and $Y^{\prime} 2$ to read $Y^{\prime \prime} 1$ and $Y^{\prime \prime} 2$.
Power supplies (Model 2000).
Delete V306, V307, V308 and earth connexion. Insert R332, 68 K , between V305 and -ve 100 V rail. Interchange the pin numbers of the A and B halves of V304.
Power Supplies (Model 2100)
Amend R 317 to read 220 K . Amend R324 to read 560 K .
Interchange the pin numbers of the A and B halves of V304.
Delete V307, V308, V309 and earth connexion. Insert R332, 68 K , between V306 and -ve 100 V rail. Add capacitor C330, 1000 p , between the 180 V line (connected to L301) and earth.
Amend heater feed to V 300 to read $6.3 \mathrm{~V}, 3.6 \mathrm{~A}$ (transformer secondary al, a2).

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## INTRODUCTION

Models 2000 and 2100 are compact versatile oscilloscopes for general-purpose measurements. Physically, the two instruments are almost identical and the circuitry for each Model is very similar. Both Models employ a modern double-gun CRT which provides a brilliant display with excellent definition. The CRT for Model 2100, however, is fitted with a spiral post-deflexion anode and is operated at a higher voltage so that faster writing speeds can be attained than with Model 2000. With this CRT, the bandwidth of Model 2100 is also increased over that of Model 2000 by approximately $1 \mathrm{Mc} / \mathrm{s}$. Two identical amplifiers with built-in pre-amplifiers are provided for Y deflexion.

The triggering system provides four modes of operation, Auto, Slow, Fast and TV Frame. In the Auto mode, the scan will lock automatically to a diverse range of waveforms, manual adjustment of the TRIG.-LEVEL control being unnecessary. A TRIG.-REP. potentiometer controls the trigger threshold of the calibrated time-base and permits it to free-run if desired. In the other modes, the waveform voltage level, at which the time-base will commence to scan, can be set by the TRIG.LEVEL control. Triggering can be selected on either the rising or the falling curve of the waveform in all modes and from EXT, Y1 and $50 \sim$. A sync. separator enables a composite TV waveform to be locked to a line or frame pulse. Four overlapping ranges of time-base delay are available.

A d.c. coupled X amplifier of variable gain provides calibrated sweep expansion on all time ranges, and, alternatively, may be used to amplify external signals. An Intensity Mod. switch selects internally generated 50 musec markers or external Z-modulation signals. The graticule can be illuminated, and the illumination can be changed from normal to red simply by rotating the graticule through 90 deg . Both Model 2000 and Model 2100 can be fitted with standard Cossor cameras.

## SPECIFICATION

| CATHODE-RAY TUBE | 4 in. ( 10 cm ) double-gun tube with green fluorescence, operating at 1.5 kV for Model 2000 and at 4 kV for Model 2100. Blue or long afterglow tubes available to special order. Individual BRIGHTNESS and FOCUS controls provided for each beam. |
| :---: | :---: |

Y1 AMPLIFIER
Frequency response d.c. to $5 \mathrm{Mc} / \mathrm{s}$ for Model 2000 and d.c. to $6 \mathrm{Mc} / \mathrm{s}$ for Model 2100, better than $30 \%$ down.
Rise-time $70 \mathrm{~m} \mu \mathrm{sec}$ for Model 2000, $60 \mathrm{~m} \mu \mathrm{sec}$ for Model 2100.
Output deflexion not less than 6 cm .
Sensitivity calibrated $100 \mathrm{mV} / \mathrm{cm}$ to $100 \mathrm{~V} / \mathrm{cm}$, in steps of 1,3 and 10 .
Variable $3: 1$ on each range.
Input Attenuator impedance $1 \mathrm{M} \Omega, 30 \mathrm{pF}$ on all ranges.

Y2 AMPLIFIER
Identical with Y1 amplifier.

Y PRE-AMPLIFIERS (two) Sensitivity. $1 \mathrm{mV} / \mathrm{cm}$, bandwidth $10 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}$, and $10 \mathrm{mV} / \mathrm{cm}$, bandwidth $5 \mathrm{c} / \mathrm{s}$ to $1 \mathrm{Mc} / \mathrm{s}$, better than $30 \%$ down.
Input impedance $1 \mathrm{M} \Omega$.
In normal operation, positive input signals deflect both traces upwards.

TIME-BASE
21 calibrated ranges from $3 \mathrm{sec} / \mathrm{cm}$ to $1 \mu \mathrm{sec} / \mathrm{cm}$.
Sweep expansion $\times 10$.
Effectively d.c. coupled bright-up pulse to CRT grid gives uniform brightness along the trace length and sweep bright-up on all ranges.

TRIGGER
Four modes of operation, Auto, Slow, Fast and TV Frame. Positive or negative from $50 \mathrm{c} / \mathrm{s}$, internal or external.
Adjustable TRIG.-LEVEL and TRIG.-REP. controls permit initiation of scan from any part of the waveform. Range of level control $\pm 30 \mathrm{~V}$ for external signals.
Sensitivity. Internal 3 mm deflexion.
External 0.1 V.

Delay. Four overlapping ranges cover $4 \mu \mathrm{sec}$ to 2.5 msec (extendable to 50 msec .

Variable control DELAY FINE is uncalibrated.

X AMPLIFIER

## CALIBRATION

## GENERAL

POWER SUPPLY

SIZE AND WEIGHT

OPTIONAL EXTRA
D.C. to $1 \mathrm{Mc} / \mathrm{s}, 30 \%$ down. Variable sensitivity $0.5 \mathrm{~V} / \mathrm{cm}$ to $2 \mathrm{~V} / \mathrm{cm}$.

Voltage. By internally generated waveform switched through the amplifier. Accuracy within $\pm 3 \%$. When input attenuator is accurately set on $0.1 \mathrm{~V} / \mathrm{cm}$ range, ranges $0.3 \mathrm{~V} / \mathrm{cm}$ to $100 \mathrm{~V} / \mathrm{cm}$ are within $\pm 5 \%$.

Time. Directly calibrated in time $/ \mathrm{cm}$, accuracy within $\pm 5 \%$ on basic ranges.

High-frequency time marker. $50 \mathrm{~m} \mu \mathrm{sec}( \pm 3 \%)$ intensity modulation for accurate measurement of pulse rise-time. Synchronized to time-base.

Illuminated graticule with variable control.
External Z-modulation terminal.
Direct access to Y plates.
Sweep saw-tooth ( 100 V ) available at front panel.
Fittings for attachment of Camera Model 1428 or Model 1458.

Mains 110 V and 220 V , with taps $\pm 5 \mathrm{~V}, \pm 10 \mathrm{~V}$, and $\pm 20 \mathrm{~V}$.
Frequency $50 \mathrm{c} / \mathrm{s}$ to $60 \mathrm{c} / \mathrm{s}$.
Consumption 100 W (approx.).

Height 15 in. ( 38.1 cm ).
Depth 17 in. $(43.2 \mathrm{~cm})$.
Width 11 in. $(27.9 \mathrm{~cm})$.
Weight $34.5 \mathrm{lb}(15.7 \mathrm{~kg})$.

Probe Model 2005 (for Y1 and Y2 amplifiers).
Input Impedance $10 \mathrm{M} \Omega, 9 \mathrm{pF}$.
Attenuation $\times 10$.

# INSTRUCTIONS FOR USING MODEL 2000 AND MODEL 2100 

## POWER SUPPLY

Warning Do not touch any part of the circuit while the mains supply is connected to the instrument. The mains fuse is in the unswitched side of the mains supply and will be " live " when the supply is connected, even though the instrument is switched off.
Ensure that the mains voltage selector at the rear of the instrument is positioned correctly for the mains supply from which the Cossorscope is to be operated.
With the instrument Mains switch in the off position (up), connect the mains supply to the Cossorscope.

## CONTROLS - INITIAL SETTING

Position the controls as stated below:
BRIGHTNESS and FOCUS mid-position of travel.
Trig.-Selector +Yl .

Trig.-System
TRIG.-REP.
AUTO.

Delay Range fully clockwise.

OFF.
Time/cm
10 msec.
TIME MULTIPLIER
Y1 and Y2 SHIFT
Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$
$\cdot 1 \mathrm{~V} / \mathrm{cm}$
A.C.-D.C.-CAL. (Y1 and Y2)

Intensity Mod.
CAL.

X SHIFT

## NORMAL.

mid-position of travel.
Switch on the Cossorscope and ensure that the name-plate is illuminated. Rotate the TRIG.-REP. control in a counter-clockwise direction until the time-base locks, that is, just past the point where free-running ceases.
Note Usually when the sweep speed is changed, readjustment of the TRIG.-REP. control is not necessary.
Using the displayed square wave adjust the BRIGHTNESS and FOCUS controls for optimum spot geometry, and use the SHIFT control to position the traces as desired.

Do not allow the white line, which is marked on each BRIGHTNESS control, to appear in front of the escutcheon, except when using external signals via the X amplifier to the X plates. With external signals so applied, advance the BRIGHTNESS controls because no internal bright-up pulse is applied to the grids of the CRT.
For normal operation, set the Yl SHIFT control (on the left-hand side) to position one trace in the bottom half of the CRT screen and set the Y2 SHIFT control (on the right-hand side) to position the other trace in the top half of the CRT screen.

## CALIBRATION OF Y AMPLIFIERS

On each Y channel, adjust the Y GAIN (SET CAL.) control so that the displayed square wave ( $50 \mathrm{c} / \mathrm{s}$ for Model 2000 and a nominal $1 \mathrm{kc} / \mathrm{s}$ for Model 2100), which is internally pre-set to 0.3 V peak-to-peak, has an amplitude of 3 cm .
To calibrate the pre-amplifiers, turn the Y1 and Y2 V/cm switches to the required pre-amplifier position, that is, to $\cdot 01 \mathrm{~V} / \mathrm{cm}$ or $\cdot 001 \mathrm{~V} / \mathrm{cm}$, and adjust the Y GAIN (SET CAL.) controls so that the displayed square wave has an amplitude of 3 cm . Do this separately for each pre-amplifier sensitivity position.
Whenever the Y GAIN (SET CAL.) controls are moved from their calibration settings or a preamplifier is switched in or out of circuit, re-calibrate the Y amplifiers, as described above, before making measurements.

## INPUT TO Y AMPLIFIERS

Do not apply any input above 500 V to either of the Y amplifiers. If the d.c. path ( $1 \mathrm{M} \Omega$ ) to earth through the attenuator is likely to cause interference to the apparatus that is being tested, put the A.C.-D.C.-CAL. switches to the A.C. position.

To terminate an input to the coaxial socket of the amplifiers, connect a resistor, value $50 \Omega$ less than the terminating value required, between the Y input terminal (maroon) and the earth terminal (black). When the terminating value required is $50 \Omega$, connect the Y1 and Y2 INPUT terminals direct to the EARTH terminals because the $50 \Omega$ is connected internally, as indicated on the escutcheon of the instrument.
When using the $\cdot 001 \mathrm{~V} / \mathrm{cm}$ range, unless the signal source is of low impedance, connect the input lead via a screened coaxial input socket and screen the 4 mm input terminal with the adapter provided.

## TIME-BASE CONTROLS

Trig.-System

Five-position switch for selection of four modes of operation: AUTO; SLOW; FAST; TV FRAME. The fifth position EXT.TB is used for deflecting the trace horizontally with external signals.
AUTO: easiest mode to use and suitable for general-purpose working. In the absence of a trigger signal, time-base free-runs at a maximum repetition rate of $100 \mathrm{c} / \mathrm{s}$. The sweep locks automatically to a trigger signal, the P.R.F. increasing with the amplitude of the applied signal. Preferred mode when it is required to lock to sine waves in the frequency range of $1 \mathrm{Mc} / \mathrm{s}$ to $5 \mathrm{Mc} / \mathrm{s}$.
N.B. The TRIG.-LEVEL control is inoperative in this mode.

SLOW: in this mode, with the TRIG.-REP. control set correctly, the time-base will not trigger unless a trigger signal is applied. The exact part of the signal to trigger the time-base can be selected by using the Trig.-Selector switch and the TRIG.-LEVEL control.

FAST: for stable triggering from high-frequency and fast risetime waveforms with unwanted low-frequency signals present, for example, square-wave edge with $50 \mathrm{c} / \mathrm{s}$ ripple. Selection of part of the signal for triggering is made by using the Trig.-Selector switch and TRIG.-LEVEL control.

TV FRAME: introduces a sync. separator into the circuit. The TRIG.-LEVEL control may then be used to eliminate the video signal and the sync. separator removes the line pulse from a composite TV signal. Time-base is triggered from TV Frame pulse or low-frequency signal with high-frequencies present.
N.B. The minimum amplitude of the TV signal for correct triggering is 3 cm ( 1 cm sync. only).

EXT.TB: position enabling use as an X input terminal to be made of the EXT.TB IN/INT.TB OUT terminal, which is located at the bottom right-hand side of the front panel and at which the time-base waveform appears in the other four positions of the Trig.-System switch. Can be used, for example, for driving frequency-swept oscillators.

To stop the time-base when using this position, turn the TRIG.REP. control fully counter-clockwise.

Time/cm

Multiplier
x SHIFT

X EXPANSION

Seven-position switch for selection of sweep speeds: $1 \mathrm{sec} / \mathrm{cm}$, $100 \mathrm{msec} / \mathrm{cm}, 10 \mathrm{msec} / \mathrm{cm}, 1 \mathrm{msec} / \mathrm{cm}, 100 \mu \mathrm{sec} / \mathrm{cm}, 10 \mu \mathrm{sec} / \mathrm{cm}$, $1 \mu \mathrm{sec} / \mathrm{cm}$.

Three-position switch multiplying all 7 sweep speeds, selected by the Time $/ \mathrm{cm}$ switch, by factors of 1,2 or 3 .

Used for horizontal positioning of the traces, clockwise rotation of the control giving movement to the right and counter-clockwise rotation giving movement to the left. Sufficient control is available to move any part of the trace to the centre of the CRT screen.

Variable control calibrated ( $\times 1, \times 10$ ) at each end of travel, clockwise rotation causing expansion of the displayed waveform about the centre of the CRT screen.

Delay Range

Trig.-Selector

TRIG.-LEVEL

TRIG.-REP.

Five-position switch: OFF, and four delay positions, 1, 2, 3 and 4 (maximum) introducing delay between the triggering signal and the start of the time-base. When the switch is in one of the delay positions, AUTO mode should not be used.
For delay, adjust the TRIG.-REP. control correctly, as described above (Controls-Initial Setting), and rotate the TRIG.-LEVEL control fully counter-clockwise. Then turn the TRIG.-LEVEL control clockwise until the time-base triggers.

Six-position switch for selection of the signal source from which it is desired to trigger the time-base. Switch positions are in three pairs:
EXT. The signal applied to the EXT. TRIGGER terminal (bottom left-hand side).
Y1. The signal applied to the YI amplifier.
$50 \sim$. The mains supply waveform.
Each pair permits triggering either from the positive-going (marked + ) or from the negative-going (marked -) edge of the signal.

Used to select the position on the triggering signal at which triggering will occur and is inoperative in the AUTO mode. For triggering during negative levels, position the control to the left. For triggering during positive levels, position the control to the right. The smaller the trigger signal, the nearer to the central position will the control be set.
See "Delay Range" above for use of this control when using delay ranges.

Allows the time-base to operate in a triggered or free-running condition.

## INTENSITY MODULATION

The Intensity Mod. switch has three positions:

NORMAL
$20 \mathrm{Mc} / \mathrm{s}$

EXT.

Traces brightened during the sweep period only.
As for NORMAL, but modified by a $20 \mathrm{Mc} / \mathrm{s}$ sine wave, which is synchronized to the time-base to provide 50 musec marker pips along the traces.
Used for measuring fast rise-times and for accurate time measurement, generally at the fastest sweep speed.

Used for brightening the traces when an external waveform is applied to the intensity modulation terminal fitted to the back panel of the instrument. The terminal is a.c. coupled through a cathodefollower to the grids of the CRT.

## ILLUMINATED GRATICULE

The graticule can be illuminated by using the GRATICULE control (top left-hand side), clockwise rotation increasing the illumination.

Graticule rotation, which assists in normal measurement work, also provides white or red illumination as desired. Red is especially advantageous when using a visor to observe a faint trace, because it will not affect the dark adaptation of the eye.

Changing the illumination from white to red, or vice versa, is achieved by rotating the graticule through 90 deg.

## MEASUREMENTS

Before making any voltage measurements, position the A.C.-D.C.-CAL. switches to CAL. and, with the attenuators switched to $\cdot 1 \mathrm{~V} / \mathrm{cm}$, or $\cdot 01 \mathrm{~V} / \mathrm{cm}$, or $\cdot 001 \mathrm{~V} / \mathrm{cm}$ according to the sensitivity required, set the Y GAIN (SET CAL.) controls so that the display on the CRT has an amplitude of 3 cm , calibration on the $\cdot 1 \mathrm{~V} / \mathrm{cm}$ range holding good for all ranges $\cdot 1 \mathrm{~V} / \mathrm{cm}$ to $100 \mathrm{~V} / \mathrm{cm}$. For example, switch the sensitivity to $10 \mathrm{~V} / \mathrm{cm}$, then if the trace height is 4.3 cm , the amplitude is 43 V peak-to-peak.

When only one Y amplifier is used, do not position the A.C.-D.C.-CAL. switch to CAL. for the other amplifier, since the $50 \mathrm{c} / \mathrm{s}$ calibration waveform may be picked up by the amplifier in use.

For time measurements, always put the X EXPANSION control to one of the calibrated positions, that is, $\times 1$ or $\times 10$. For example, with the Time $/ \mathrm{cm}$ switch positioned at $100 \mu \mathrm{sec} / \mathrm{cm}$, and Multiplier at $\times 2$, then if the trace occupies 3.5 cm , the duration will be $700 \mu \mathrm{sec}$ when the X EXPANSION control is position at $\times 1$, or $70 \mu \mathrm{sec}$ when the X expansion is $\times 10$.

When using the $\times 10$ position with the Time $/ \mathrm{cm}$ switch positioned at $1 \mu \mathrm{sec} / \mathrm{cm}$, use $20 \mathrm{Mc} / \mathrm{s}$ markers for high accuracy because at this maximum sweep speed, the sweep linearity does not permit measurements to be made accurately off the graticule.

## DELAY

For convenient examination of short pulses or fast edges, use the delay facility to delay the start of the time-base by a time slightly less than that represented by P.R.F. of the pulse, thus enabling the whole of the next pulse, including the start, to be displayed. For example, if a pulse of $1 \mu \mathrm{sec}$ and repetition rate $50 \mathrm{kc} / \mathrm{s}$ is being examined, put the Time $/ \mathrm{cm}$ switch to $1 \mu \mathrm{sec}$, the Delay Range switch to position 2 and adjust the DELAY FINE control so that the pulse succeeding the synchronizing pulse appears on the CRT screen.

For more detailed examination, adjust the X EXPANSION control in conjunction with the Delay controls.

When the setting of either the Delay Range switch or the DELAY FINE control is altered, readjust the TRIG.-LEVEL control as necessary.

Longer periods of delay may be obtained by increasing the value of C 410 at the rate of $0.004 \mu \mathrm{~F}$ for each 1 msec of delay required, for example, to increase the delay to 50 msec , increase C 410 to $0 \cdot 2 \mu \mathrm{~F}$.

Fig. I Block Schematic Diagram of Model 2000

MODEL 2000

BLOCK

Fig. 2 Block Schematic Diagram of Model 2100

BLOCK SCHEMATIC DIAGRAM MODEL 2100

## CIRCUIT DESCRIPTION FOR MODEL 2000

## POWER SUPPLY

## Mains Supply

The mains supply is applied via F300 and S301 to the primary circuit of T300, which includes two 110 V windings. These 110 V windings can be connected in series or in parallel, and a 20 V winding can be connected as series aiding or opposing in 5 V steps. Interconnexions are made with plugs on the voltage selector panel at the rear of the instrument and enable the Cossorscope to be used with a.c. supplies, $50 \mathrm{c} / \mathrm{s}$ to $60 \mathrm{c} / \mathrm{s}$, in the ranges $90 \mathrm{~V}-130 \mathrm{~V}$, and $200 \mathrm{~V}-240 \mathrm{~V}$.
There are six secondary windings on T300, three for l.t. supplies, two for h.t. supplies and one for the e.h.t. supply. The h.t. windings are connected to bridge rectifiers.

## +ve 300 V Supply

Four silicon diodes, MR300-MR303, form the bridge rectifier for the +ve 300 V supply. The reservoir capacitor is C300, and smoothing is achieved with L300 and C301.

## +ve 170 V Supply

A cathode-follower V300A, with its anode connected direct to the + ve 300 V rail, provides + ve 170 V at low impedance for use in the time-base generator.
The ASTIGMATISM control, RV304, is inserted between the + ve 300 V and + ve 170 V supplies.

## -ve 100 V Supply

Selenium rectifiers, MR304-MR307 manufactured as a single block, form the bridge rectifier for the -ve 100 V supply. The reservoir capacitor is C302, and smoothing is achieved with the filter network R300, C303.

## E.H.T. Supply

The secondary winding for the e.h.t. supply is connected to a conventional voltage-doubler, MR308, MR309, giving a nominal output of -ve 1600 V . The positive end of this supply is taken to the anode of the pentode V300B. Potentiometer RV301 adjusts the voltage of the control grid of V300B and is used to pre-set the e.h.t. potential at -ve 1600 V .
The circuit arrangement stabilizes the negative output voltage with respect to the load current. A fixed proportion of any load change of the -ve 1600 V supply is fed to the grid of the pentode and appears in correct phase at the anode to compensate the original change on the -ve 1600 V line. Rail ripple is also reduced with this method of stabilization, particularly as C312 feeds the ripple, without substantial attenuation, to the pentode grid.
Potentials for the BRIGHTNESS controls, RV302 and RV303, and the FOCUS controls, RV300 and RV306, are taken from the e.h.t. resistor chain, which also supplies a stabilized voltage of -ve 250 V (across V305-V308) for the TRIG.-REP. control, RV404.

## PRE-AMPLIFIERS

Pre-amplifiers for the Y1 and Y2 channels are identical. Triode-pentode valves are employed for this purpose, V101 for the Y1 channel and V201 for the Y2 channel. The circuit description given below is for the YI channel only.
The anode load of the pre-amplifier V101B is equivalent to $r_{a}+(\mu+1) R_{k}$, where $r_{a}$ is the anode impedance, $\mathrm{R}_{k}$ the cathode resistance and $\mu$ the amplification factor of the triode V101A. The h.t. supply to the amplifier is stabilized by V100 and is further smoothed by Cl09. This supply also provides the screen voltage to V101B. Since the cathode of the triode half of V101 is of lower impedance than the anode of the pentode half of the valve, the output is taken from the cathode of V101A, the triode section. Current through V101A is limited by R113, R114 when the pre-amplifier is not in use, and VI01A cathode is earthed via Si01.

There are two pre-amplifier positions $.01 \mathrm{~V} / \mathrm{cm}$ and $\cdot 001 \mathrm{~V} / \mathrm{cm}$, selected by S101. In the $\cdot 01 \mathrm{~V} / \mathrm{cm}$ position, the cathode resistors R118, R117 of the pentode half of V101, are by-passed by a fixed capacitor and a variable capacitor, total value about 150 pF , to give added gain at the higher frequencies. The variable capacitor is adjusted for optimum transient response. In the $\cdot 001 \mathrm{~V} / \mathrm{cm}$ position, the cathode resistors of V101B are by-passed by C113 in series with R149 and, at the same time, positive feedback occurs from the main amplifier via $\mathrm{Cl} 36, \mathrm{RI} 49$ and $\mathrm{Cl13}$, to the cathode of V 101 B , thus improving the higher frequency response.
In order to avoid phase reversal of the displayed signals when using the pre-amplifier positions, the output from the cathode of V101A is fed to the grid, which is opposite to that used in the long-tailed pair for the main amplifier only. Both the input and output of the pre-amplifier are a.c. coupled. When the pre-amplifier positions are in use, the grid of V103 not in use, is automatically shorted to earth by the input attenuator. When the pre-amplifier is not in use, its output is shorted to earth to ensure that no spurious signals are fed to the main amplifier.

## MAIN AMPLIFIER

For each Y amplifier, there are two input terminals, a coaxial socket and a wire-and-plug terminal. Hence, a coaxial input can be terminated because the other terminal can be earthed or connected through a resistance to earth. An internal resistor value $50 \Omega, 2 \mathrm{~W}$ is wired for this purpose and, therefore, any added external termination should be $50 \Omega$ less than the desired termination resistance. When using the coaxial socket for low-level signals, the other terminal may also be screened with the special adapter provided. Since the Y amplifiers are identical, the description given below is for the Y1 channel only.
The input attenuator is basically a simple ladder network of constant input impedance, each position of the attenuator being automatically compensated by a variable capacitor. However, when the attenuator is switched to the $\cdot 3 \mathrm{~V} / \mathrm{cm}$ and $\cdot 1 \mathrm{~V} / \mathrm{cm}$ positions, the amplifier input capacitance is added to the capacitance at the input terminals, and compensation for this effect is achieved by switching out one, or both, of two additional variable capacitors, $\mathrm{C} 101, \mathrm{Cl} 103$, in these positions.
When the A.C.-D.C.-CAL. switch is in the D.C. position, the input is connected direct to the amplifier, except when the pre-amplifier is in use. In the A.C. position, the switch introduces a d.c. blocking capacitor C100 in the input lead. When the switch is in the CAL. position, the output from the calibration waveform generator is fed to the amplifier at a level that will give 3 cm deflexion, but only if the attenuator is in one of the positions, $\cdot 1 \mathrm{~V} / \mathrm{cm}, \cdot 01 \mathrm{~V} / \mathrm{cm}$ and $\cdot 001 \mathrm{~V} / \mathrm{cm}$.
The input stage of the main amplifier employs a long-tailed pair V103, V104 with a variable gain control RV100 between the cathodes. The cathode currents of V103 and V104 pass together with
current bled by R128 and R150, through the two triodes of V102, the second stage. First and second stages are d.c. coupled, correct biasing for V102 being obtained from networks R121, R129, and R125, R132.

Optimum high-frequency response is obtained by combining the effects of three networks: fixed coils L100, L101 in series with anode loads of V103 and V104; variable capacitors C117, C118, which adjust positive feedback around V 102 and are used to trim the square-wave response to optimum; and components R126, R127, Cl 29 , which introduce negative feedback, except at high frequencies. A protection circuit, R133 and C116, prevents damage to the input valves if a high-voltage lowimpedance d.c. source should be inadvertently connected to the input when the attenuator is in the most sensitive positions. Components R112 and C127 form a filter network to prevent high frequencies, for example, $20 \mathrm{Mc} / \mathrm{s}$ oscillations from the marker oscillator V304A, from being fed into the h.t. rail of the amplifier. Heaters of the pre-amplifier valves and of the input long-tailed pair are centre-tapped to earth by R147 and R148, and each end is decoupled to prevent signals being fed along the heater wiring.

## TIME-BASE

## Trigger Amplifier

The switch S400 selects the trigger source: the internal signals fed from the Y1 amplifier via cathodefollower V105A; any signal applied externally; and the $50 \mathrm{c} / \mathrm{s}$ signal. Two positions, positive and negative, are provided for each source of trigger signals, S 400 reversing the connexions to the grids of V401 so that triggering can be achieved with positive or negative signals. Trigger signals are applied to one grid of V401, whilst a voltage, set by the TRIG.-LEVEL control, RV401, is applied to the other grid. As the circuit configuration is that of a long-tailed pair, only the part of the signal that has almost the same d.c. level at the input signal grid as the level set at the other grid will be selected and amplified. The h.t. supply for V401 is taken from the cathode-follower V105B, the grid of V105B being held at + ve 140 V (approx.) by the neons V206, V207.

## Trigger System

Selection of the Trigger system is made by operating S401. In the AUTO, SLOW, and TV FRAME positions of the switch, the d.c. component of the trigger signal is blocked by C442. In the FAST position, only high frequencies are passed on because C441 and R402 form a differentiating network. The resistor R401 isolates the input lead from the capacitance of S401.
In the AUTO position, S401 also connects the wiper of RV401 to earth, thus rendering this control inoperative. The voltage swing of the wiper is decreased when internal trigger signals are used because S400 switches R403 to earth from the slider of RV401. The full range of this control then corresponds to about twice the full-screen deflexion on the CRT.

## Trigger

When S405, the Delay Range switch, is in the OFF position, V402A functions as a cathode-follower for feeding trigger signals from V401 to the trigger-shaper valve, V403.
Except when S401 is positioned at AUTO, V403 functions as a Schmitt trigger circuit and produces a square-wave output of constant amplitude in phase with the input. The potentiometer RV403 is pre-set so that the grids of V403 are at the same potential when the wiper of RV401 is earthed and no trigger signal is applied. When S401 is positioned at TV FRAME, the input signal, amplified
and clipped by V401, is integrated by R492, C439. This arrangement eliminates line sync. pulses, or any high-frequency signals, so that the lower frequencies may be used for triggering purposes. The TV FRAME position is useful, therefore, when triggering from a waveform containing "noise" pulses.

When S401 is positioned at AUTO, V403 functions as a multivibrator because of the inclusion of C438 in the input circuit, and R430 between the two grids of the valve. With V403A in conduction, a negative signal will appear at the grid of V403B and will cut off V403B. The grid of V403A will then begin to fall (time constant C438 $\times$ R430) and V403A will be cut off, causing V403B to go into conduction again. A positive signal will occur at the grid of V403B and will cause the grid potential of V403A to rise so that V403A will then conduct again. The cycle will repeat itself at a frequency mainly determined by C438 and R430, and is nominally $100 \mathrm{c} / \mathrm{s}$.

High-amplitude signals applied to the input side of C438 will override the self-generated signal at the grid of V403A and the circuit will switch at the input signal rate. Smaller input signals, however, will synchronize the multivibrator, which will then generate trigger signals at some sub-multiple of the input frequency. The synchronizing action continues even with very small signals and the output trigger signals, whenever they occur, are locked to the input signals.
The configuration of the circuit is useful because the sweep can be synchronized with repetitive signals over a range of frequencies without readjustment of RV401, the TRIG.-LEVEL control. With no trigger signals, the sweep will trace out a zero base line at a repetition rate of $100 \mathrm{c} / \mathrm{s}$ (approx.).

## Time-base Generator

The trigger signal generated by V403 is differentiated by C414 and R425. Only the negative spikes of the differentiated waveform are passed via MR408 to the grid of V404B. When RV404, the TRIG.-REP. potentiometer, is set correctly, V404A is at the point of cut-off and will remain cut off until the grid of V403B receives a negative trigger signal. The anode of V404A is held at +ve 170 V by the diodes MR403, MR404. Cathode coupling between the two halves of V404 will cause V404A to conduct, thus cutting off V405A.

Prior to the arrival of a trigger signal, the anode load, R433, of V405A is passing almost the whole of the anode current of V406B and V404B. Therefore, when V405A is cut off, and its anode goes positive, the d.c. coupling of R437, and C443, will cause V404A to remain in conduction while the cathode of V405A falls linearly (Miller configuration of V406B) to the new potential on the grid of V405A. When the cathode of V405A has fallen to the new grid potential, the valve goes into conduction again and the circuit returns to its quiescent state, with the Miller capacitor, selected by S402 and S403, rapidly recharging to + ve 170 V .

In the Miller circuit, R448 is included to remove the Miller step, since the anode current of V406B is cut off when V405A cuts off and, hence, the voltage drop across R448 is removed. The grid of V406B falls, therefore, but the anode potential remains constant.

A cathode-follower V405B is used to operate the bright-up circuit. This valve is d.c. coupled to the anode of V405A and the output is taken from the cathode of C307 after removal of the large negative spikes, which are caused by the discharge current of the Miller capacitor.

The sweep waveform generated at the anode of V406B is taken via R446, C433 and S401 to a frontpanel socket SKT403. Resistor R446 prevents stray capacitance of the output lead from affecting the high-frequency operation of the time-base generator. The amplitude of the waveform is approximately 100 V and is suitable for driving an alignment generator.

The output from V406B is also taken, via an attenuator R457, C431, R458, C432, to the X amplifier, V408, V407, a stacked, push-pull circuit, which is similar in operation to the Y amplifier, but the bandwidth is $1 \mathrm{Mc} / \mathrm{s}$. Between the cathodes of the input long-tailed pair, formed by the two halves of V408, the potentiometer RV408 can be operated to expand the sweep about the electrical centre of the CRT screen by a factor of $\times 10$.

Note The electrical centre is almost identical with the physical centre of the CRT screen. Pre-set potentiometers, RV410 and RV411, are included in the anodes of V407 to compensate for the differences in sensitivities and electrical centres of the two pairs of X plates.

## Trigger Delay

The cathode-follower V402B can be switched by S405 to operate with V402A in order to delay the trigger signal for any period between $4 \mu \mathrm{sec}$ and 2.5 msec . When the trigger delay facility is selected, the input waveform to V402A is differentiated by C404, C412 and R412, and the negative half of the differentiated waveform is removed by MR401. The positive half of the waveform is a.c. coupled to V402A, and the resistor chain, R413, R418, provides -ve 10 V (approx.) bias to the grid of that valve.

With no input signal, V402B will be conducting because its grid is held at + ve 0.5 V by MR402 and MR409. When the positive input pulse arrives at the grid of V402A, that valve will conduct and the negative signal, which occurs at its anode, will cut off V402B because of the coupling by the selected capacitor, C407-C410, between the anode of V402A and the grid of V402B.
While the selected capacitor, C407-C410, is recharging through R502 and RV402, the valve V402B will remain cut off and when the capacitor is charged to -ve 10 V , the circuit will revert to its quiescent state with V402 in conduction. The negative edge of the pulse, thus produced at the anode of V402B by the changeover to the original conditions, is used to trigger the time-base.
The trigger pulse is delayed from the input pulse by a time dependent on R502 and RV402 and the selected coupling capacitor, C407-C410. Hence S405, which selects the coupling capacitor, is used as the Delay Range switch and RV402 is adjusted for fine control of delay.

## BRIGHT-UP AND 20 MC/S GENERATOR

Although the cathode of V405B is a.c. coupled to the bi-stable bright-up circuit of V304, the bright-up circuit functions as though it were d.c. coupled because the positive pulse, produced when S300A is positioned at NORMAL, is of almost the same amplitude as that of the input at the grid of V304A. Capacitor C307 differentiates the input waveform but, because of feedback via R316, the positive peak is held at the initial level for the duration of the pulse. Potentiometer RV307 is used to pre-set the feedback exactly. Hence, a positive pulse is available at the common cathodes of V304 and is suitable for feeding to the grid of the CRT to brighten up the trace. Valve V304 takes only about 1 mA anode current and the h.t. supply to this valve is derived from three neons, V301-V303, in the e.h.t. resistor chain.

When S300A is in the $20 \mathrm{Mc} / \mathrm{s}$ position, V304A becomes a $20 \mathrm{Mc} / \mathrm{s}$ oscillator for as long as its grid is sufficiently positive with respect to -ve 1600 V , and the output from the cathode is fed to the CRT grid for intensity modulation. The oscillatory waveform will be stationary on the trace because the oscillator is gated on by the bright-up waveform. These marker pips can be used for measuring fast rise-times at the highest sweep speeds and for accurate time measurements when the trace is expanded on the highest sweep speed.

When S300A is in the EXT. position, external bright-up signals may be applied to the grid of V304B, a cathode-follower, and the other half (V304A) of the valve will be disconnected at the anode.

Components MR310, MR311, are inserted into the circuit to ensure that V304 rests in the correct quiescent state when the instrument is initially switched on.

## CALIBRATOR

A large waveform of $50 \mathrm{c} / \mathrm{s}$ is taken from the junction of MR302 and MR303, and is fed via the highvalue resistor R483 to the grid of V406A. The positive excursion of this waveform is limited by MR406 at a nominal 65 V , the potential of the neon V409, and during this excursion, V406A passes a current that is determined by R486 and RV406. When the input becomes negative, this current passes through MR407 and hence, the switched current is determined by R486, RV406, and the neon voltage. A square-wave output is taken from the anode of V406A and, after attenuation, is fed to the attenuator switches S101, S201. When these switches are positioned to $\cdot 1 \mathrm{~V} / \mathrm{cm}$, square waves are displayed on the CRT screen. However, when the switches are in either the $.01 \mathrm{~V} / \mathrm{cm}$ or $\cdot 001 \mathrm{~V} / \mathrm{cm}$ position, the square wave is differentiated by Cl 28 and the differentiated waveform is used for calibrating purposes.

# CIRCUIT DESCRIPTION FOR MODEL 2100 

## POWER SUPPLY

## Mains Supply

The mains supply is applied via F300 and S301 to the primary circuit of T300, which includes two 110 V windings. These 110 V windings can be connected in series or in parallel, and a 20 V winding can be connected as series aiding or opposing in 5 V steps. Interconnexions are made with plugs on the voltage selector panel at the rear of the instrument and enable the Cossorscope to be used with a.c. supplies, $50 \mathrm{c} / \mathrm{s}$ to $60 \mathrm{c} / \mathrm{s}$, in the ranges $90 \mathrm{~V}-130 \mathrm{~V}$, and $200 \mathrm{~V}-240 \mathrm{~V}$.

There are six secondary windings on T300, three for l.t. supplies, two for h.t. supplies and one for the e.h.t. supply. The h.t. windings are connected to bridge rectifiers.

## +ve 300 V Supply

Four silicon diodes, MR300-MR303, form the bridge rectifier for the + ve 300 V supply. The reservoir capacitor is C300, and smoothing is achieved with L300 and C301.

## +ve 180 V Supply

A cathode-follower V 406 A , with its anode connected direct to the + ve 300 V rail, provides + ve 180 V at low impedance for use in the time-base generator.
The ASTIGMATISM control, RV304, is inserted between the + ve 300 V and +ve 180 V supplies.

## -ve 100 V Supply

Selenium rectifiers, MR304-MR307 manufactured as a single block, form the bridge rectifier for the -ve 100 V supply. The reservoir capacitor is C302, and smoothing is achieved with the filter network R300, C303.

## E.H.T. Supplies

The secondary winding for the negative e.h.t. supply is connected to a conventional voltage-doubler, MR308, MR309, giving a nominal output of -ve 1150 V . The positive end of this supply is taken to the anode of the pentode V300B. Potentiometer RV301 pre-sets the voltage of the control grid of V300B and controls the voltage on the -ve 1150 V line.
The circuit arrangement stabilizes the negative output voltage with respect to the load current. A fixed proportion of any load change of the -ve 1150 V supply is fed to the grid of the pentode and appears in correct phase at the anode to compensate the original change on the -ve 1150 V line. Rail ripple is also reduced with this method of stabilization, particularly as C312 feeds the ripple, without substantial attenuation, to the pentode grid.
For the positive e.h.t. supply, the secondary winding of T300, used for the negative e.h.t. supply, is also connected to a voltage-quadrupler consisting of MR310-MR313 and associated capacitors. A positive output of 3 kV is fed to the spiral post-deflexion anode of the CRT.
Potentials for the BRIGHTNESS controls, RV302 and RV303, and the FOCUS controls, RV300 and RV306, are taken from the e.h.t. resistor chain, which also supplies a stabilized voltage of -ve 250 V (across V305-V308) for the TRIG.-REP. control, RV404.

## PRE-AMPLIFIERS

Pre-amplifiers for the Y1 and Y2 channels are identical. Triode-pentode valves are employed for this purpose, V101 for the Y1 channel and V201 for the Y2 channel. The circuit description given below is for the Y1 channel only.
The anode load of the pre-amplifier V101B is equivalent to $r_{a}+(\mu+1) R_{k}$, where $r_{a}$ is the anode impedance, $R_{k}$ the cathode resistance and $\mu$ the amplification factor of the triode V101A. The h.t. supply to the amplifier is stabilized by V100 and is further smoothed by C109. This supply also provides the screen voltage to V101B. Since the cathode of the triode half of V101 is of lower impedance than the anode of the pentode half of the valve, the output is taken from the cathode of V101A, the triode section. Current through V101A is limited by R113, R114, when the pre-amplifier is not in use, and V101A cathode is earthed via S101.
There are two pre-amplifier positions, $\cdot 01 \mathrm{~V} / \mathrm{cm}$ and $\cdot 001 \mathrm{~V} / \mathrm{cm}$, selected by S 101 . In the $\cdot 01 \mathrm{~V} / \mathrm{cm}$ position, the cathode resistors R118, R117 of the pentode half of V101 are by-passed by a fixed capacitor and a variable capacitor, total value about 150 pF , to give added gain at the higher frequencies. The variable capacitor is adjusted for optimum transient response. In the $\cdot 001 \mathrm{~V} / \mathrm{cm}$ position, the cathode resistors of V101B are by-passed by C113 in series with R149 and, at the same time, positive feedback occurs from the main amplifier via C136, R149 and C113, to the cathode of V101B, thus improving the higher frequency response.
In order to avoid phase reversal of the displayed signals when using the pre-amplifier positions, the output from the cathode of V101A is fed to the grid, which is opposite to that used in the long-tailed pair for the main amplifier only. Both the input and output of the pre-amplifier are a.c. coupled. When the pre-amplifier positions are in use, the grid of V103, not in use, is automatically shorted to earth by the input attenuator. When the pre-amplifier is not in use, its output is shorted to earth to ensure that no spurious signals are fed to the main amplifier.

## MAIN AMPLIFIER

For each Y amplifier, there are two input terminals, a coaxial socket and a wire-and-plug terminal. Hence, a coaxial input can be terminated because the other terminal can be earthed or connected through a resistance to earth. An internal resistor value $50 \Omega, 2 \mathrm{~W}$ is wired for this purpose and, therefore, any added external termination should be $50 \Omega$ less than the desired termination resistance When using the coaxial socket for low-level signals, the other terminal may also be screened with the special adapter provided. Since the Y amplifiers are identical, the description given below is for the Y1 channel only.
The input attenuator is basically a simple ladder network of constant input impedance, each position of the attenuator being automatically compensated by a variable capacitor. However, when the attenuator is switched to the $\cdot 3 \mathrm{~V} / \mathrm{cm}$ and $\cdot 1 \mathrm{~V} / \mathrm{cm}$ positions, the amplifier input capacitance is added to the capacitance at the input terminals, and compensation for this effect is achieved by switching out one, or both, of two additional variable capacitors, $\mathrm{Cl} 101, \mathrm{C} 103$, in these positions.
When the A.C.-D.C.-CAL. switch is in the D.C. position, the input is connected direct to the amplifier, except when the pre-amplifier is in use. In the A.C. position, the switch introduces a d.c. blocking capacitor C 100 in the input lead. When the switch is in the CAL. position, the output from the calibration waveform generator is fed to the amplifier at a level that will give 3 cm deflexion, but only if the attenuator is in one of the positions, $\cdot 1 \mathrm{~V} / \mathrm{cm}, \cdot 01 \mathrm{~V} / \mathrm{cm}$ and $\cdot 001 \mathrm{~V} / \mathrm{cm}$.
The input stage of the main amplifier employs a long-tailed pair V103, V104 with a variable gain control RV100 between the cathodes. The cathode currents of V103 and V104 pass together with current bled by R128 and R150, through the two triodes of V102, the second stage. First and second stages are d.c. coupled, correct biasing for V102 being obtained from networks R121, R129, and R125, R132.

Optimum high-frequency response is obtained by combining the effects of four networks: fixed coils L101, L102 in series with anode loads of V103 and V104; variable capacitors C117, C118, which adjust positive feedback around V102 and are used to trim the square-wave response to optimum; two fixed coils L103, L104, in the leads between the output anodes and the Y-deflexion plates; and components R126, R127, C129, which introduce negative feedback, except at high frequencies.
A protection circuit, R133 and C116, prevents damage to the input valves if a high-voltage lowimpedance d.c. source should be inadvertently connected to the input when the attenuator is in the most sensitive positions. Components R112 and C127 form a filter network to prevent high frequencies, for example, $20 \mathrm{Mc} / \mathrm{s}$ oscillations from the marker oscillator V304A, from being fed into the h.t. rail of the amplifier. Heaters of the pre-amplifier valves and of the input long-tailed pair are centre-tapped to earth by R147 and R148, and each end is decoupled to prevent signals being fed along the heater wiring.

## TIME-BASE

## Trigger Amplifier

The switch S 400 selects the trigger source: the internal signals fed from the Y1 amplifier via cathodefollower V105A; any signal applied externally; and the $50 \mathrm{c} / \mathrm{s}$ signal. Two positions, positive and negative, are provided for each source of trigger signals, S400 reversing the connexions to the grids of V401 so that triggering can be achieved with positive or negative signals. Trigger signals are applied to one grid of V401, whilst a voltage, set by the TRIG.-LEVEL control, RV401, is applied to the other grid. As the circuit configuration is that of a long-tailed pair, only the part of the signal that has almost the same d.c. level at the input signal grid as the level set at the other grid will be selected and amplified.

## Trigger System

Selection of the trigger system is made by operating S401. In the AUTO, SLOW, and TV FRAME positions of the switch, the d.c. component of the trigger signal is blocked by C442. In the FAST position, only high frequencies are passed on because C441 and R402 form a differentiating network. The resistor R401 isolates the input lead from the capacitance of S401.

In the AUTO position, S401 connects the wiper of RV401 to earth, thus rendering this control inoperative. The voltage swing of the wiper is decreased when internal trigger signals are used because S400 switches R403 to earth from the slider of RV401. The full range of this control then corresponds to about twice the full-screen deflexion on the CRT.

## Trigger

When S405, the Delay Range switch, is in the OFF position, V402A functions as a cathode-follower for feeding trigger signals from V401 to the trigger-shaper valve, V403.
Except when S401 is positioned at AUTO, V403 functions as a Schmitt trigger circuit and produces a square-wave output of constant amplitude in phase with the input. The potentiometer RV403 is pre-set so that the grids of V403 are at the same potential when the wiper of RV401 is earthed and no trigger signal is applied. When S401 is positioned at TV FRAME, the input signal, amplified and clipped by V401, is integrated by R492, C439. This arrangement eliminates line sync. pulses, or any high-frequency signals, so that the lower frequencies may be used for triggering purposes. The TV FRAME position is useful, therefore, when triggering from a waveform containing "noise" pulses.

When S401 is positioned at AUTO, V403 functions as a multivibrator because of the inclusion of C438 in the input circuit, and R430 between the two grids of the valve. With V403A in conduction, a negative signal will appear at the grid of V403B and will cut off V403B. The grid of V403A will then begin to fall (time constant C438 $\times$ R430) and V403A will be cut off, causing V403B to go into conduction again. A positive signal will occur at the grid of V403B and will cause the grid potential of V403A to rise so that V403A will then conduct again. The cycle will repeat itself at a frequency that is mainly determined by C438 and R430, and is nominally $100 \mathrm{c} / \mathrm{s}$.

High-amplitude signals applied to the input side of C438 will override the self-generated signal at the grid of V403A and the circuit will switch at the input signal rate. Smaller input signals, however, will synchronize the multivibrator, which will then generate trigger signals at some sub-multiple of the input frequency. The synchronizing action continues even with very small signals and the output trigger signals, whenever they occur, are locked to the input signals.

This configuration of the circuit is useful because the sweep can be synchronized with repetitive signals over a range of frequencies without readjustment of RV401, the TRIG.-LEVEL control. With no trigger signals, the sweep will trace out a zero base line at a repetition rate of $100 \mathrm{c} / \mathrm{s}$ (approx.).

## Time-base Generator

The trigger signal generated by V403 is differentiated by C414 and R425. Only the negative spikes of the differentiated waveform are passed via MR408 to the grid of V404B. When RV404, the TRIG.REP. potentiometer, is set correctly, V404A is at the point of cut-off and will remain cut off until the grid of V403B receives a negative trigger signal. The anode of V404A is held at + ve 180 V by the diodes MR403, MR404. Cathode coupling between the two halves of V404 will cause V404A to conduct, thus cutting off V405A.

Prior to the arrival of a trigger signal, the anode load, R433, of V405A is passing almost the whole of the anode current of V406B and V404B. Therefore, whenV405A is cut off, and its anode goes positive, the d.c. coupling of R437, and C443, will cause V404A to remain in conduction while the cathode of V405A falls linearly (Miller configuration of V406B) to the new potential on the grid of V405A. When the cathode of V405A has fallen to the new grid potential, the valve goes into conduction again and the circuit returns to its quiescent state, with the Miller capacitor, selected by S402 and S403, rapidly recharging to + ve 180 V .

In the Miller circuit, R448 is included to remove the Miller step, since the anode current of V406B is cut off when V405A cuts off and, hence, the voltage drop across R448 is removed. The grid of V406B falls, therefore, but the anod potential remains constant.

A cathode-follower V405B is used to operate the bright-up circuit. This valve is d.c. coupled to the anode of V405A and the output is taken from the cathode to C307 after removal of the large negative spikes, which are caused by the discharge current of the Miller capacitor.

The sweep waveform generated at the anode of V406B is taken via R446, C433 and S401 to a frontpanel socket SKT403. Resistor R446 prevents stray capacitance of the output lead from affecting the high-frequency operation of the time-base generator. The amplitude of the waveform is approximately 100 V and is suitable for driving an alignment generator.

The output from V406B is also taken, via an attenuator R457, C431, R458, C432, to the X amplifier, V408,:V407, a stacked, push-pull circuit, which is similar in operation to the $Y$ amplifier, but the bandwidth is $1 \mathrm{Mc} / \mathrm{s}$. Between the cathodes of the input long-tailed pair, formed by the two halves of V408, the potentiometer RV408 can be operated to expand the sweep about the electrical centre of the CRT screen by a factor of $\times 10$. Potentiometer RV407 controls the bias on V407 and, therefore, adjusts the sweep linearity as displayed on the CRT screen.
Note The electrical centre is almost identical with the physical centre of the CRT screen. Pre-set potentiometers, RV410 and RV411, are included in the anodes of V407 to compensate for the differences in sensitivities and electrical centres of the two pairs of X plates.

## Trigger Delay

The cathode-follower V402B can be switched by S405 to operate with V402A in order to delay the trigger signal for any period between $4 \mu \mathrm{sec}$ and 2.5 msec . When the trigger delay facility is selected, the input waveform to V402A is differentiated by C404 and R412, and the negative half of the differentiated waveform is removed by MR401. The positive half of the waveform is a.c. coupled to V402A, and the resistor chain, R413, R418, provides -ve 10 V (approx.) bias to the grid of that valve.
With no input signal, V402B will be conducting because its grid is held at +ve 0.5 V by MR402 and MR409. When the positive input pulse arrives at the grid of V402A, that valve will conduct and the negative signal, which occurs at its anode, will cut off V402B because of the coupling by the selected capacitor, C407-C410, between the anode of V402A and the grid of V402B.
While the selected capacitor, C407-C410, is recharging through R502 and RV402, the valve V402B will remain cut off and when the capacitor is charged to -ve 10 V , the circuit will revert to its quiescent state with V402 in conduction. The negative edge of the pulse, thus produced at the anode of V402B by the changeover to the original conditions, is used to trigger the time-base.
The trigger pulse is delayed from the input pulse by a time dependent on R502 and RV402 and the selected coupling capacitor, C407-C410. Hence S405, which selects the coupling capacitor, is used as the Delay Range switch and RV402 is adjusted for fine control of delay.

## BRIGHT-UP AND 20 MC/S GENERATOR

Although the cathode of V405B is a.c. coupled to the bi-stable bright-up circuit of V304, the brightup circuit functions as though it were d.c. coupled because the positive pulse, produced when S300A is positioned at NORMAL, is of almost the same amplitude as that of the input at the grid of V304A. Capacitor C307 differentiates the input waveform but, because of feedback via R316, the positive peak is held at the initial level for the duration of the pulse. Potentiometer RV307 is used to pre-set the feedback exactly. Hence, a positive pulse is available at the common cathodes of V304 and is suitable for feeding to the grid of the CRT to brighten up the trace. Valve V304 takes only about 1 mA anode current and the h.t. supply to this valve is derived from three neons, V301-V303, in the e.h.t. resistor chain.

When S 300 B is in the $20 \mathrm{Mc} / \mathrm{s}$ position, the positive bias voltage will be removed trom the cathode of V300A, allowing the circuit to function as a pulsed, grounded-grid oscillator. Since V300A is driven by the bright-up waveform, the $20 \mathrm{Mc} / \mathrm{s}$ oscillations will be synchronized to the time-base generator. These oscillations pass via C328 to the CRT cathode and will appear, therefore, as stationary pips on the displayed trace.

When S300A is in the EXT. position, external bright-up signals may be applied to the grid of V304B, a cathode-follower, and the other half (V304A) of the valve will be disconnected at the anode.
Components MR310, MR311, are inserted into the circuit to ensure that V304 rests in the correct quiescent state when the instrument is initially switched on.

## CALIBRATOR

A neon switching circuit, incorporating two miniature neons, is used for the calibrator. This circuit will only operate with one, or both, of the A.C.-D.C.-CAL. switches in the CAL. position. When V411 is conducting, C434 will become charged through R479, R483 and V411. The capacitor will build up sufficient voltage to cut off V411, and V409 will then strike. Capacitor C434 will discharge through R490, and V411 will then strike. The resultant square wave is taken from the junction of R485 and R486 to S101 and S201. Pre-set potentiometer RV406 adjusts the amplitude of the waveform that is fed to the Y amplifiers.

# SERVICING FOR MODEL 2000 AND MODEL 2100 

## Caution Do not touch any part of the circuit while the power supply is connected to the instrument. Whenever the Cossorscope is switched off, allow at least two minutes to elapse before touching any part of the wiring.

## INITIAL SETTING OF CONTROLS

Rotate the GRATICULE control, X EXPANSION control and TRIG.-REP. control fully counterclockwise.
Set both BRIGHTNESS controls and both FOCUS controls to mid-position of travel.
Rotate the Y 1 and Y2 GAIN (SET CAL.) controls to ' O '.
Position the Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switches at $3 \mathrm{~V} / \mathrm{cm}$.
Position the Y1 and Y2 A.C.-D.C.-CAL. switches at D.C.
Position the Intensity Mod. switch at NORMAL.
Set Y1 SHIFT, Y2 SHIFT, X SHIFT and TRIG.-LEVEL controls to mid-position of travel.
Position the Trig.-System switch at SLOW and the Trig.-Selector switch at EXT.+.
Position the Time/cm switch at 1 msec and the Multiplier switch at $\times 1$.
Position the Delay Range switch at OFF and set the DELAY FINE control to the mid-position of travel. Set RV408 for minimum resistance and RV407 to mid-position of travel.

## POWER SUPPLY

Ensure that the mains voltage selector is correctly positioned for the mains supply that is to be applied to the instrument Mains switch.

On Model 2000 only, adjust RV301 to obtain an e.h.t. voltage of -ve 1600 V. Ensure that the voltage on the anode (pin 6) of V300 is between + ve 150 V and + ve 300 V .
On Model 2100 only, adjust RV301 to obtain an e.h.t. voltage of -ve 1150 V . Ensure that the voltage on the anode (pin 6) of V300 is between + ve 200 V and + ve 400 V , with minimum brightness of the two traces. Using an electrostatic voltmeter, measure the p.d.a. voltage and ensure that, with normal operating brightness, this voltage is $+\mathrm{ve} 3 \mathrm{kV} \pm 15 \%$.

## PRELIMINARY ADJUSTMENTS

Rotate both BRIGHTNESS controls in an upward direction until a spot from each gun of the CRT appears on the CRT screen. Using the Y SHIFT controls, position the Y1 spot at 1 cm below the central horizontal line of the graticule, and the $Y 2$ spot at 1 cm above the same line. Adjust the X SHIFT control to centre the spots in the CRT screen. Set both FOCUS controls and the ASTIGMATISM control, RV304, for optimum definition of the spots. Rotate the Y1 and Y2 GAIN (SET CAL.) controls to 9.

Rotate the TRIG.-REP. control in a clockwise direction and ensure that a free-running time-base occurs. Then rotate this control counter-clockwise, just past the point where free-running occurs, so that the time-base does not free-run. Connect a $1 \mathrm{kc} / \mathrm{s}$ signal, at 10 V peak-to-peak level, to the Y1 INPUT and EXT. TRIGGER sockets. Short-circuit the centre tag of the TRIG.-LEVEL potentiometer to earth. Adjust RV403 (located under V403) so that the time-base is triggered. Reduce the input signal to 1 V and reset RV403 to produce a stable triggered trace, which should occur with the potentiometer near the mid-position of travel. Remove the short-circuit from the TRIG.-LEVEL potentiometer and adjust this control for a stable triggered trace. Switch the Trig.-Selector from EXT. + to EXT. - and ensure that the polarity of the trace becomes reversed. If necessary, readjust RV403 slightly. Disconnect the $1 \mathrm{kc} / \mathrm{s}$ input signal.

With the TRIG.-REP. control rotated fully clockwise, adjust the BRIGHTNESS controls for normal brilliance of trace. Rotate the TRIG.-REP. control counter-clockwise to stop the time-base. Adjust RV307 to black out the spots. Ensure that the traces brighten in all positions of the Time/cm switch.

Position the Trig.-Selector switch to $50 \mathrm{c} / \mathrm{s}+$. Connect the Y INPUT socket to the yellow/black wire on the Trig.-Selector switch, and ensure that rotation of the TRIG.-LEVEL control will window the + ve slope of the $50 \mathrm{c} / \mathrm{s}$ signal. Position the Trig.-Selector switch at $50 \mathrm{c} / \mathrm{s}$ - and repeat this procedure for the -ve slope of the $50 \mathrm{c} / \mathrm{s}$ signal.

Position the Trig.-Selector switch at EXT. +. Feed sharp pulses, for example, $1 \mu \mathrm{sec}$ at $1 \mathrm{kc} / \mathrm{s}$, to both Y amplifiers and to the EXT. TRIGGER socket. Position the Time $/ \mathrm{cm}$ switch at $1 \mathrm{msec} / \mathrm{cm}$. Adjust the TRIG.-REP. and TRIG.-LEVEL controls for a stable trace. Set RV410 and RV411 so that the pulses, at the centre of the CRT screen, are aligned on both traces, and the pulses, 4 cm to the right and 4 cm to the left of the centre, are within 0.25 mm of each other, measured horizontally. If necessary, reverse the leads to $X^{\prime} 1$ and $X^{\prime \prime} 1$, or $X^{\prime} 2$ and $X^{\prime \prime} 2$, to achieve these conditions.

Note The potentiometers RV410, RV411 may be shunted with a low-value resistor, if the extreme end of travel of the control has to be used.

On Model 2100 only, feed pulses, at a repetition rate of $50 \mathrm{kc} / \mathrm{s}$, to the Y2 INPUT and EXT. TRIGGER sockets. Adjust the input so that the amplitude of the display is 3 cm . Position the Time $/ \mathrm{cm}$ switch at $100 \mu \mathrm{sec}$. Adjust the TRIG.-REP. and TRIG.-LEVEL controls for a stable display. Set RV412 for optimum linearity along the horizontal axes.

## X AMPLIFIER

## Square Wave

Position the Trig.-System switch to EXT. TB. Rotate the TRIG.-REP. control fully counterclockwise. Use the output of a $10 \mathrm{kc} / \mathrm{s}$ square-wave generator to trigger a monitor oscilloscope, separate from Cossorscope Model 2000 or Model 2100, and feed the time-base output from the monitor oscilloscope to the Y1 INPUT socket of Model 2000 or Model 2100. Feed the output of the $10 \mathrm{kc} / \mathrm{s}(0 \cdot 1 \mu \mathrm{sec}$ rise-time) square-wave generator to the EXT. TB IN socket of Model 2000 or Model 2100. Position the X EXPANSION control to $\times 10$. Adjust the output of the $10 \mathrm{kc} / \mathrm{s}$ squarewave generator to give 4 cm of X deflexion. Position the Y1 V/cm switch and the Y1 GAIN (SET CAL.) control for convenient Y deflexion. Adjust C446 for long time constant. Adjust C419 and C436 for short time constant ensuring that their capacitances are approximately equal.

## Frequency Response

Disconnect the time-base signal from the Y1 INPUT socket, and the $10 \mathrm{kc} / \mathrm{s}$ square wave from the EXT. TB IN socket. Feed a $1 \mathrm{kc} / \mathrm{s}$ sine-wave signal to the EXT. TB IN socket and adjust the input signal so that the X scan is 4 cm . With a constant input, vary the frequency and ensure that the output is not less than 2.8 cm at $1 \mathrm{Mc} / \mathrm{s}$. Remove the feed to EXT. TB IN socket.

## TIME-BASE LINEARITY

Position the Intensity Mod. switch at EXT., the Trig.-System switch at SLOW and the Trig.Selector switch at EXT. + . Position the Time/cm switch at $1 \mu \mathrm{sec}$ and set the X EXPANSION control to $\times 1$.
Feed $1 \mathrm{Mc} / \mathrm{s}$ pulses into the Y2 INPUT and EXT. TRIGGER sockets. Adjust the TRIG.-REP. and TRIG.-LEVEL controls for a stable trace. Set C431 so that the end of the fly-back coincides with the start of the X scan.

## TIME CALIBRATION

With the Intensity Mod. switch positioned at NORMAL, the Time/cm switch at $100 \mu \mathrm{sec}$ and the Multiplier switch at $\times 1$, feed pulses at a $10 \mathrm{kc} / \mathrm{s}$ repetition rate into the Y2 INPUT and EXT. TRIGGER sockets. Set RV407 to give one pulse per cm. Position the X EXPANSION control to $\times 10$. Change the input to the Y2 amplifier to pulses at $100 \mathrm{kc} / \mathrm{s}$ repetition rate. Ensure that the pulse repetition rates for time calibration are within $\pm 0.5$ per cent. Set RV409 so that eight pulses occupy 8 cm of trace. Position the X EXPANSION control to $\times 1$ and change the input to the Y2 amplifier to pulses at $10 \mathrm{kc} / \mathrm{s}$ repetition rate. Readjust RV407 if necessary.
On all time ranges except $1 \mu \mathrm{sec}$, use appropriate input signals and adjust RV407 and RV409 to balance out differences between ranges. On the $1 \mu \mathrm{sec}$ range, set C435 for correct timing over the 8 cm in the middle of the scan.

## 20 MC/S MARKER

Feed a $5 \mathrm{Mc} / \mathrm{s}$ sine wave into the Y2 INPUT socket and feed pulses at $100 \mathrm{kc} / \mathrm{s}$, synchronized to the $5 \mathrm{Mc} / \mathrm{s}$ signal, into the EXT. TRIGGER socket. Position the Time $/ \mathrm{cm}$ switch at $10 \mu \mathrm{sec}$, the Multiplier switch at $\times 1$ and the Intensity Mod. switch at $20 \mathrm{Mc} / \mathrm{s}$. Adjust the TRIG.-REP. and TRIG.LEVEL controls for a stable trace. Set the cores in L301 and L302 to produce four bright-up pulses per waveform, the resultant display appearing as two or three parallel straight lines. Disconnect the feed to the Y2 INPUT and EXT. TRIGGER sockets.

## EXTERNAL BRIGHTNESS MODULATION

Position the Intensity Mod. switch at EXT. and the Time/cm switch at 1 msec . Feed a $1 \mathrm{kc} / \mathrm{s}$ square wave into the EXT. Z. MOD. terminal (at rear) and into the EXT. TRIGGER socket. Ensure that the trace is split up into bright spots with signals of less than 20 V peak-to-peak.

## DELAY

Position the Intensity Mod. switch at NORMAL. Feed pulses at a $10 \mathrm{kc} / \mathrm{s}$ repetition rate into the EXT. TRIGGER socket. Feed pulses at $1 \mathrm{Mc} / \mathrm{s}$ repetition rate and $100 \mathrm{kc} / \mathrm{s}$ repetition rate together into the Y2 INPUT socket. Ensure that the pulse repetition rates are within $\pm 5$ per cent. With the DELAY FINE control set fully counter-clockwise, ensure that the delay is less than $5 \mu \mathrm{sec}$.
With suitable input signals and using a triggering pulse, that always has a longer repetition period than the maximum delay for the delay range in use, ensure that the delay ranges overlap.
With the Delay Range switch in position 4, ensure that the delay (maximum) is not less than 2.5 msec . Ensure that jitter at maximum delay is better than 1 part in 1000, for example, on the 2 msec range, the jitter should not exceed $2 \mu \mathrm{sec}$.
With the Delay Range switch at position 3, and DELAY FINE control set to mid-position of travel, ensure that a 2 V square wave, applied in conjunction with adjustment of the TRIG.-LEVEL control, will trigger the delay circuit. Rotate the Delay Range switch to the OFF position.

## TRIGGER SYSTEM

Feed a $1 \mathrm{kc} / \mathrm{s}$ square wave, 1 V peak-to-peak, into the Y2 INPUT and EXT. TRIGGER sockets. Using the TRIG.-LEVEL control, ensure that stable triggering occurs for all positions of the Trig.System switch.
Position the Trig.-System switch at SLOW and the Trig.-Selector switch at $50 \mathrm{c} / \mathrm{s}+$, thus producing a triggered trace. Position the Trig.-System switch at FAST to remove the triggered trace. Ensure that operation of the TRIG.-LEVEL control does not produce a trace. Carry out this procedure with the Trig.-Selector switch positioned at $50 \mathrm{c} / \mathrm{s}-$.
Position the Trig.-System switch at AUTO and the Trig.-Selector switch at EXT. +. Reduce the input $1 \mathrm{kc} / \mathrm{s}$ square wave to 50 mV . Ensure that the trace is stable and that polarity is reversed when the Trig.-Selector is switched from EXT. + to EXT. -. Rotate the TRIG.-LEVEL control for each polarity and ensure that this control has no effect on the trace.

## Y AMPLIFIERS

Position the Trig.-Selector switch at Y1 + , the Trig.-System switch at AUTO, the Time/cm switch at 10 msec , the Multiplier switch at $\times 3$, the Y1 A.C.-D.C.-CAL. switch at D.C. and the Y1 V/cm switch at $\cdot 1 \mathrm{~V} / \mathrm{cm}$. Feed a $1 \mathrm{kc} / \mathrm{s}$ signal of $0.5 \mathrm{~V} \pm 1 \%$ peak-to-peak amplitude to the Y1 INPUT socket. Adjust the TRIG.-REP. control to obtain a triggered trace and rotate the YI GAIN (SET CAL.) control to obtain a trace of 5 cm . Position the Yl A.C.-D.C.-CAL. switch at CAL. and adjust RV406 to obtain a trace of 3 cm .
Position the $\mathrm{Y} 1 \mathrm{~V} / \mathrm{cm}$ switch at $\cdot 01 \mathrm{~V} / \mathrm{cm}$. Reduce the amplitude of the $1 \mathrm{kc} / \mathrm{s}$ signal to $50 \mathrm{mV} \pm 1 \%$ peak-to-peak. Return the Y1 A.C.-D.C.-CAL. switch to the D.C. position and rotate the Y1 GAIN (SET CAL.) control to obtain a trace of 5 cm . Position the Y1 A.C.-D.C.-CAL. switch at CAL. On Model 2000 only, adjust RV102 to obtain a trace of 3 cm . Repeat this procedure with the $\mathrm{Y} 1 \mathrm{~V} / \mathrm{cm}$ switch positioned at $\cdot 001 \mathrm{~V} / \mathrm{cm}$. Adjust RV102 to balance out differences between the $\cdot 01 \mathrm{~V} / \mathrm{cm}$ and $\cdot 001 \mathrm{~V} / \mathrm{cm}$ ranges. Position the $\mathrm{Y} 1 \mathrm{~V} / \mathrm{cm}$ switch at $\cdot 1 \mathrm{~V} / \mathrm{cm}$ and the Y1 A.C.-D.C.-CAL. switch at D.C. On Model 2100 only, ensure that the displayed trace is $3 \mathrm{~cm} \pm 5 \%$. Carry out this procedure with the $\mathrm{Y} 1 \mathrm{~V} / \mathrm{cm}$ switch positioned at $\cdot 001 \mathrm{~V} / \mathrm{cm}$.
Position the $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switch at $\cdot 1 \mathrm{~V} / \mathrm{cm}$, the Y2 A.C.-D.C.-CAL. switch at CAL. and the Y2 GAIN (SET CAL.) control fully clockwise. Ensure that not less than 3.3 cm of trace can be obtained. Carry out this procedure with the $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switch positioned, in turn, at $\cdot 01 \mathrm{~V} / \mathrm{cm}$ and at $\cdot 001 \mathrm{~V} / \mathrm{cm}$.

## AMPLIFIER TRANSIENT RESPONSE

Position the Y1 and Y2 A.C.-D.C.-CAL. switches at D.C. and the $\mathrm{V} / \mathrm{cm}$ switches at $\cdot 1 \mathrm{~V} / \mathrm{cm}$. Position the Time $/ \mathrm{cm}$ switch at $10 \mu \mathrm{sec}$. Feed the Y1 and Y2 INPUT sockets with a $100 \mathrm{kc} / \mathrm{s}$ square wave that has a rise-time less than $20 \mathrm{~m} \mu \mathrm{sec}$. Obtain a stable display by adjustment of the TRIG.-REP. and TRIG.-LEVEL controls. Position the Y1 trace with 4 cm centrally disposed on a line located 1 cm below the centre horizontal line of the graticule, and position the Y2 trace in a similar manner, but centrally disposed on a line located 1 cm above the centre horizontal line of the graticule. Adjust C117 and C118 for optimum square wave on the Y1 channel, and C217 and C218 for optimum square wave on the Y2 channel. Ensure that overshoot, or undershoot, does not exceed 3 per cent.

## PRE-AMPLIFIER TRANSIENT RESPONSE

Position the Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switches at $01 \mathrm{~V} / \mathrm{cm}$. Feed a $10 \mathrm{kc} / \mathrm{s}$ square wave with a rise-time of less than $100 \mathrm{~m} \mu \mathrm{sec}$ into the Y1 and Y2 INPUT sockets. Adjust C137 for Y1 channel, and C237 for Y2 channel, for optimum square waves. With the Y1 and Y2 V/cm switches positioned at $\cdot 001 \mathrm{~V} / \mathrm{cm}$, feed a smaller input to the Y amplifiers and ensure that there is no overshoot.

## AMPLIFIER FREQUENCY RESPONSE

Position the Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switches at $\cdot 1 \mathrm{~V} / \mathrm{cm}$. Feed a $50 \mathrm{kc} / \mathrm{s}$ sine wave to the Y 1 and Y 2 INPUT sockets. Set the amplitude of the sine wave to give a raster of 4 cm . Keeping the input voltage constant, increase the frequency and ensure that the amplitude does not fall below 2.8 cm , at $5 \mathrm{Mc} / \mathrm{s}$ for Model 2000, and at $6 \mathrm{Mc} / \mathrm{s}$ for Model 2100. Carry out this procedure, in turn, for the $\cdot 01 \mathrm{~V} / \mathrm{cm}$ and $\cdot 001 \mathrm{~V} / \mathrm{cm}$ positions of the Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switches, using a $1 \mathrm{kc} / \mathrm{s}$ signal to set up the 4 cm raster. Ensure that the amplitude does not fall below 2.8 cm , at $1 \mathrm{Mc} / \mathrm{s}$ for the $.01 \mathrm{~V} / \mathrm{cm}$ range and at $200 \mathrm{kc} / \mathrm{s}$ for the $\cdot 001 \mathrm{~V} / \mathrm{cm}$ range.

## ATTENUATORS

With the Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switches positioned at $\cdot 1 \mathrm{~V} / \mathrm{cm}$, set the Y 1 and Y 2 GAIN (SET CAL.) controls to obtain traces of 3 cm . Feed appropriate known signals to the Y amplifiers on $\cdot 3 \mathrm{~V} / \mathrm{cm}$, $1 \mathrm{~V} / \mathrm{cm}, 3 \mathrm{~V} / \mathrm{cm}, 10 \mathrm{~V} / \mathrm{cm}, 30 \mathrm{~V} / \mathrm{cm}$, and $100 \mathrm{~V} / \mathrm{cm}$ ranges, in turn, and ensure that the vertical deflection is within $\pm 3 \%$ of its true value.
With the Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switches positioned at $.3 \mathrm{~V} / \mathrm{cm}$, apply to the Y amplifiers a $10 \mathrm{kc} / \mathrm{s}$ square wave with a rise-time of less than $0 \cdot 1 \mu \mathrm{sec}$ and of suitable amplitude to display 4 cm of scan. For Yl amplifier, adjust C102 in conjunction with stray capacitance (wired around R100) to obtain optimum square wave. For Y2 amplifier, adjust C202 in conjunction with stray capacitance (wired around R200) to obtain optimum square wave. Then adjust C122, C123, C124, C125 and C126, in turn, for the Y1 channel and C222, C223, C224, C225 and C226, in turn, for the Y2 channel, on ranges $1 \mathrm{~V} / \mathrm{cm}, 3 \mathrm{~V} / \mathrm{cm}, 10 \mathrm{~V} / \mathrm{cm}, 30 \mathrm{~V} / \mathrm{cm}$, and $100 \mathrm{~V} / \mathrm{cm}$ in that order.

## AMPLIFIER INPUT CAPACITY

Position the Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switches at $\cdot 1 \mathrm{~V} / \mathrm{cm}$. Feed a $1 \mathrm{kc} / \mathrm{s}$ signal through a probe, for example, Cossor Model 2005, to the Y1 and Y2 amplifiers. Align the trimmer capacitor in the probe to give optimum square wave.
Position the Y 1 and $\mathrm{Y} 2 \mathrm{~V} / \mathrm{cm}$ switches at $\cdot 3 \mathrm{~V} / \mathrm{cm}$, and adjust C 101 for the Y 1 channel and C201 for the Y2 channel to obtain optimum square waves.
Position the Y1 and Y2 V/cm switches at $1 \mathrm{~V} / \mathrm{cm}$, and adjust C103 for the Y1 channel and C203 for the Y2 channel to obtain optimum square waves. Ensure that all ranges except $\cdot 01 \mathrm{~V} / \mathrm{cm}$ and $\cdot 001 \mathrm{~V} / \mathrm{cm}$ give optimum square waves.

## VOLTAGE READINGS FOR MODEL 2000

Warning Standard safety measures must be taken whenever any point at high potential relative to earth is metered.
The table of voltage readings given below provides a useful guide when servicing Model 2000. Some variation of the figures can be expected because of component tolerances, and allowance should be made accordingly. All readings were taken with an Avometer Model 8, set to the highest range compatible with reading accuracy. Readings are relative to earth and are positive except where the polarity is stated.

Cossorscope Model 2000 was set up for normal working with a mains input supply of 225 V a.c. and with the voltage selector positioned at 225 V . The two spots were centred in the CRT screen and the Trig.-System switch was positioned at AUTO. The TRIG.-REP. control was set for triggering and the Delay Range switch was positioned at OFF. On each Y channel, the A.C.-D.C.CAL. switch was positioned at CAL. and the $\mathrm{V} / \mathrm{cm}$ switch was positioned at $1 \mathrm{~V} / \mathrm{cm}$.

The symbol $\rightarrow$ at the heater pins indicates that the heater is elevated to 170 V d.c.

| Valve | Type | Pin 1 | Pin 2 | Pin 3 | Pin 4 | Pin 5 | Pin 6 | Pin 7 | Pin 8 | Pin 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V101 | ECF80 | $\begin{aligned} & \text { at } \\ & 45 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{gl} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g} 2 \\ & 45 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | h | $\begin{aligned} & \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \text { ap } \\ & 14 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{kp}, \mathrm{~g} 3, \mathrm{~s} \\ & 2.8 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l} \hline \mathrm{kt} \\ 16 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \text { gt } \\ & 14 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |
| V102 | ECC88 | $\begin{array}{\|l\|} \hline \mathrm{a}^{\prime \prime} \\ 245 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime \prime} \\ & 122 \cdot 5 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & 127 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\bar{h}$ | $\begin{aligned} & \hline \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \\ & \text { a.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 245 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime} \\ & 122.5 \mathrm{~V} \end{aligned}$ <br> d.c. | $\begin{array}{\|l} \hline \mathrm{k}^{\prime} \\ 127 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | s |
| V1.03 | EF184 | $\begin{array}{\|l} \hline \mathrm{k} \\ 1.5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{gl} \\ & 0 \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{k} \\ 1.5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | h | $\begin{aligned} & \hline \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\stackrel{s}{ }$ | $\begin{aligned} & \mathrm{a} \\ & 120 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{g} 2 \\ 122.5 \mathrm{~V} \end{array}$ <br> d.c. | $\begin{array}{\|l\|} \hline \text { g3 } \\ 1.5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ |
| V104 | EF184 | $\begin{array}{\|l\|} \hline \mathrm{k} \\ 1.5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{gl} \\ & 0 \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{k} \\ 1.5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\mathrm{h}$ | $\begin{aligned} & \mathrm{h} \\ & \overrightarrow{6 \cdot 3} \mathrm{~V} \\ & \text { a.c. } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 120 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{g} 2 \\ 122 \cdot 5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{g} 3 \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |
| V105 | ECC81 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 300 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 175 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{h} \\ & 0 \end{aligned}$ | h <br> a.c. <br> a.c | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 300 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime} \\ & 125 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |  | $\begin{aligned} & \text { hct } \\ & ++ \end{aligned}$ |
| V201 | ECF80 | $\begin{array}{\|l} \hline \text { at } \\ 45 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{gl} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l} \hline \mathrm{g} 2 \\ 45 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\underset{*}{\mathrm{~h}}$ | $\begin{aligned} & \hline \mathrm{h} \\ & 6.3 \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \text { ap } \\ & 14 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{kp,g} 3, \mathrm{~s} \\ & 2 \cdot 8 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{kt} \\ 16 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{gt} \\ & 14 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |
| V202 | ECC88 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 245 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 122 \cdot 5 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & 127 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \hline \mathrm{h} \\ & 6.3 \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{a}^{\prime} \\ & 245 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & 122.5 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{k}^{\prime} \\ 127 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | s |
| V203 | EF184 | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{gl} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\mathrm{h}$ | $\begin{aligned} & \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\underline{s}$ | $\begin{aligned} & \text { a } \\ & 120 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{g} 2 \\ 122.5 \mathrm{~V} \\ \text { d.c. } \end{array}$ | $\begin{aligned} & \mathrm{g} 3 \\ & 1 \cdot 5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |
| V204 | EF184 | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{gl} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |  | $\stackrel{\mathrm{h}}{6 \cdot 3 \mathrm{~V}}$ a.c. | $\mathrm{s}$ | $\begin{aligned} & \mathrm{a} \\ & 120 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \text { g2 } \\ 122 \cdot 5 \\ \text { d.c. } \end{array}$ | $\begin{aligned} & \mathrm{g} 3 \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |
| V205 | ECC81 | $\begin{aligned} & a^{\prime \prime} \\ & 300 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 175 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{k}^{\prime \prime} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{h} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{h} \\ & 0 \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 300 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{g}^{\prime} \\ 125 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline \mathrm{k}^{\prime} \\ 126.5 \mathrm{~V} \end{array}$ d.c. | $\begin{gathered} \text { hct } \\ ++ \end{gathered}$ |


| Valve | Type | Pin 1 | Pin 2 | Pin 3 | Pin 4 | Pin 5 | Pin 6 | Pin 7 | Pin 8 | Pin 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V300 | ECF80 | at <br> 300 V <br> d.c. | $\begin{aligned} & \hline \mathrm{gl} \\ & -\mathrm{ve} \\ & 2 \cdot 2 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g} 2 \\ & 125 \cdot 5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | h | h $6 \cdot 3 \mathrm{~V}$ <br> a.c. | ap <br> 220 V <br> d.c. | $\begin{aligned} & \mathrm{kp}, \mathrm{~g} 3, \mathrm{~s} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{kt} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | gt <br> 170 V <br> d.c. |
| V304 | ECC88 | $\begin{array}{\|l\|} \hline \mathrm{a}^{\prime \prime} \\ -\mathrm{ve} \\ 1450 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime \prime} \\ & -\mathrm{ve} \\ & 1570 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & -\mathrm{ve} \\ & 1550 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\mathrm{h}$ | h $6 \cdot 3 \mathrm{~V}$ <br> a.c. | $\begin{aligned} & \hline \mathrm{a}^{\prime} \\ & -\mathrm{ve} \\ & 1440 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & -\mathrm{ve} \\ & 1500 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{k}^{\prime} \\ -\mathrm{ve} \\ 1550 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ |  |
| V401 | ECC88 | $\begin{aligned} & \mathrm{a}^{\prime \prime} \\ & 105 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k} \mathrm{k}^{\prime \prime} \\ & 1 \cdot 8 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\mathrm{h}$ | h <br> 6.3 V <br> a.c. | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 105 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & 0 \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 1.8 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\stackrel{s}{ }$ |
| V402 | ECC88 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 230 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 0 \cdot 5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & 105 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | h | $\begin{aligned} & \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \end{aligned}$ a.c. | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 230 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime} \\ & 105 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 107 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | s |
| V403 | ECC88 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 290 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime \prime} \\ & 107 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{k}^{\prime \prime} \\ 120 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\mathrm{h}$ | $\begin{array}{\|l\|} \hline \mathrm{h} \\ 6 \cdot 3 \mathrm{~V} \\ \text { a.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{a}^{\prime} \\ & 290 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & 107 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 120 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\stackrel{s}{ }$ |
| V404 | ECC88 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 170 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime \prime} \\ & 0 \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{k}^{\prime \prime} \\ 3 \mathrm{~V} \\ \text { d.c. } \end{array}$ | h | h $6.3 \mathrm{~V}$ a.c. | $\begin{aligned} & \hline \mathrm{a}^{\prime} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & -\mathrm{ve} \\ & 10 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 3 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |  |
| V405 | ECC88 | $\begin{aligned} & \mathrm{a}^{\prime \prime} \\ & 300 \mathrm{~V} \\ & \mathrm{~d} \end{aligned}$ d.c. | $\begin{aligned} & \hline \mathrm{g}^{\prime \prime} \\ & 160 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | h | $\stackrel{\mathrm{h}}{6 \cdot 3 \mathrm{~V}}$ a.c. | $\begin{array}{\|l\|} \hline \mathrm{a}^{\prime} \\ 240 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & 176 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |  |
| V406 | ECF80 | $\begin{aligned} & \text { at } \\ & 140 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{gl} \\ 0.15 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{g} 2 \\ & 37 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\mathrm{h}$ | $\begin{array}{\|l\|} \hline \mathrm{h} \\ 6 \cdot 3 \mathrm{~V} \\ \text { a.c. } \\ \hline \end{array}$ | $\begin{aligned} & \text { ap } \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{kp}, \mathrm{~g} 3, \mathrm{~s} \\ & 0 \end{aligned}$ | $\begin{aligned} & \hline \mathrm{kt} \\ & 10 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{gt} \\ & 0 \cdot 1 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ |
| V407 | ECC88 | $\begin{aligned} & a^{\prime \prime} \\ & 215 \mathrm{~V} \end{aligned}$ d.c. | $\begin{array}{\|l\|} \hline \mathrm{g}^{\prime \prime} \\ 65 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline \mathrm{k}^{\prime \prime} \\ 70 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\mathrm{h}$ | $\begin{aligned} & \mathrm{h} \\ & 6 \cdot \overrightarrow{3} \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{a}^{\prime} \\ & 215 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{g}^{\prime} \\ 65 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 70 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ |  |
| V408 | ECC88 | $\begin{aligned} & \text { a" } \\ & 65 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l} \mathrm{g}^{\prime \prime} \\ 0 \end{array}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & 4 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{h} \\ & * \end{aligned}$ | $\begin{aligned} & \hline \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 65 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{g}^{\prime} \\ 0 \end{array}$ | $\begin{aligned} & \mathrm{k}^{\prime} \\ & 4 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | s |

* The reading was taken between the heater pins.
++ The voltage between the strapped pins, 4 and 5 , and pin 9 was 6.3 V a.c.
V100, V200, V205-V207, V301-V303, V305-V308, V409, V410
Nominal burning voltage of miniature neons CC3L is 65 V , but variations can be expected between samples in the range 55 V to 80 V .


## VOLTAGE READINGS FOR MODEL 2100

Warning Standard safety measures must be taken whenever any point at high potential relative to earth is metered.

The table of voltage readings given below provides a useful guide when servicing Model 2100. Some variation of the figures can be expected because of component tolerances, and allowance should be made accordingly. All readings were taken with an Avometer Model 8, set to the highest range compatible with reading accuracy. Readings are relative to earth and are positive except where the polarity is stated.

Cossorscope Model 2100 was set up for normal working with a mains input supply of 225 V a.c. and with the voltage selector positioned at 225 V . The two spots were centred in the CRT screen and the Trig.-System switch was positioned at AUTO. The TRIG.-REP. control was set for triggering and the Delay Range switch was positioned at OFF. On each Y channel, the A.C.-D.C.CAL. switch was positioned at CAL. and the $\mathrm{V} / \mathrm{cm}$ switch was positioned at $1 \mathrm{~V} / \mathrm{cm}$.
The symbol $\rightarrow$ at the heater pins indicates that the heater is elevated to 180 V d.c.

| Valve | Type | Pin 1 | Pin 2 | Pin 3 | Pin 4 | Pin 5 | Pin 6 | Pin 7 | Pin 8 | Pin 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V101 | ECF80 | $\begin{array}{\|l\|} \hline \text { at } \\ 45 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{array}{\|l} \hline \mathrm{gl} \\ 1.5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{array}{\|l} \hline \mathrm{g} 2 \\ 45 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | h | $\begin{aligned} & \mathrm{h} \\ & 6.3 \mathrm{~V} \end{aligned}$ a.c. | $\begin{aligned} & \text { ap } \\ & 14 . \mathrm{V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{kp}, \mathrm{~g} 3, \mathrm{~s} \\ & 2 \cdot 8 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{kt} \\ & 16 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{gt} \\ & 14 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |
| V102 | ECC88 | $\begin{aligned} & \mathrm{a}^{\prime \prime} \\ & 245 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 122 \cdot 5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & 127 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | h | h <br> 6.3 V <br> a.c. | $\begin{array}{\|l\|} \hline \mathrm{a}^{\prime} \\ 245 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & 122 \cdot 5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 127 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | s |
| V103 | EF184 | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{gl} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | h | h $6 \cdot 3 \mathrm{~V}$ a.c. | $\stackrel{s}{ }$ | $\begin{aligned} & \hline \mathrm{a} \\ & 120 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{g} 2 \\ 122 \cdot 5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{g} 3 \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |
| V104 | EF184 | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \end{aligned}$ d.c. | $\begin{aligned} & \mathrm{gl} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \end{aligned}$ d.c. | $\mathrm{h}$ | $\overrightarrow{\mathrm{h}} \overrightarrow{6 \cdot 3 \mathrm{~V}}$ a.c. | $\begin{aligned} & \mathrm{s} \\ & - \end{aligned}$ | $120 \mathrm{~V}$ d.c. | g2 <br> 122.5 V <br> d.c. | g3 1.5 V d.c. |
| V105 | ECC81 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 300 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 175 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{k}^{\prime \prime} \\ & 180 \mathrm{~V} \end{aligned}$ d.c. | $\begin{aligned} & \mathrm{h} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{h} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 300 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime} \\ & 125 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | 126.5 V <br> d.c. | $\begin{aligned} & \text { hct } \\ & ++ \end{aligned}$ |
| V201 | ECF80 | $\begin{aligned} & \text { at } \\ & 45 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{gl} \\ 1.5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{g} 2 \\ & 45 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\mathrm{h}$ | $\begin{aligned} & \mathrm{h} \\ & 6.3 \mathrm{~V} \end{aligned}$ a.c. | $\begin{aligned} & \text { ap } \\ & 14 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \mathrm{kp}, \mathrm{~g} 3, \mathrm{~s} \\ 2 \cdot 8 \mathrm{~V} \\ \text { d.c. } \end{array} \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{kt} \\ 16 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline \mathrm{gt} \\ 14 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ |
| V202 | ECC88 | $\begin{array}{\|l\|} \hline \mathrm{a}^{\prime \prime} \\ 245 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 122.5 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\mathrm{k}^{\prime \prime}$ <br> 127 V <br> d.c. | $\mathrm{h}$ | h <br> $6 \cdot 3 \mathrm{~V}$ <br> a.c. | $\begin{aligned} & \hline \mathrm{a}^{\prime} \\ & 245 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime} \\ & 122 \cdot 5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 127 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | s |
| V203 | EF184 | $\begin{array}{\|l\|} \hline \mathrm{k} \\ 1.5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{gl} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\mathrm{h}$ | h <br> 6.3 V <br> a.c. | $\stackrel{s}{ }$ | $\begin{aligned} & \mathrm{a} \\ & 120 \mathrm{~V} \\ & \mathrm{d.c.c} \end{aligned}$ | $\begin{aligned} & \mathrm{g} 2 \\ & 122 \cdot 5 \mathrm{~V} \end{aligned}$ d.c. | $\begin{aligned} & \hline \mathrm{g} 3 \\ & 1.5 \mathrm{~V} \\ & \mathrm{~d} \cdot \mathrm{c} . \end{aligned}$ |
| V204 | EF184 | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{gl} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k} \\ & 1.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\mathrm{h}$ | h <br> 6.3 V <br> a.c. | $\stackrel{s}{-}$ | $\begin{aligned} & \hline \mathrm{a} \\ & 120 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{g} 2 \\ & 122 \cdot 5 \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|l\|} \hline \text { g3 } \\ 1.5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ |


| Valve | Type | Pin 1 | Pin 2 | Pin 3 | Pin 4 | Pin 5 | Pin 6 | Pin 7 | Pin 8 | Pin 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V300 | ECF80 | $\begin{array}{\|l} \text { at } \\ 300 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{gl} \\ & -\mathrm{ve} \\ & 2 \cdot 2 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{g} 2 \\ 125 \cdot 5 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | h | h $6 \cdot 3 \mathrm{~V}$ à.c. | $\begin{aligned} & \text { ap } \\ & 220 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{kp}, \mathrm{~g} 3, \mathrm{~s} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{kt} \\ & 10 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \text { gt } \\ & 8 \text { V } \\ & \text { d.c. } \end{aligned}$ |
| V304 | ECC88 | $\begin{array}{\|l\|} \hline \mathrm{a}^{\prime \prime} \\ -\mathrm{ve} \\ 850 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime \prime} \\ & -\mathrm{ve} \\ & 1100 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & -\mathrm{ve} \\ & 1080 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\mathrm{h}$ | h $\rightarrow$ $6 \cdot 3 \mathrm{~V}$ a.c. | $\begin{aligned} & \mathrm{a}^{\prime} \\ & -\mathrm{ve} \\ & 900 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & -\mathrm{ve} \\ & 1100 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & -\mathrm{ve} \\ & 1100 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | s |
| V401 | ECC88 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 105 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime \prime} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k}^{\prime \prime} \\ & 1 \cdot 8 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | h | h <br> $6 \cdot 3 \mathrm{~V}$ <br> a.c. | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 105 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k}^{\prime} \\ & 1 \cdot 8 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\stackrel{s}{2}$ |
| V402 | ECC88 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 230 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 0.5 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{k} \mathrm{k}^{\prime \prime} \\ & 105 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | h | $\begin{aligned} & \hline \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 230 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & 105 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{k}^{\prime} \\ & 107 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\underline{s}$ |
| V403 | ECC88 | $\begin{array}{\|l\|} \hline \mathrm{a}^{\prime \prime} \\ 290 \mathrm{~V} \\ \text { d.c. } \end{array}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 107 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & 120 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | h | $\begin{aligned} & \hline \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 290 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime} \\ & 107 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{k}^{\prime} \\ & 120 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\stackrel{s}{ }$ |
| V404 | ECC88 | $\begin{aligned} & \text { a" } \\ & 170 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 0 \end{aligned}$ | $\begin{array}{\|l\|} \hline \mathrm{k}^{\prime \prime} \\ 3 \mathrm{~V} \\ \mathrm{~d} . \mathrm{c} . \\ \hline 1 \times \prime \end{array}$ | $\mathrm{h}$ | $\begin{aligned} & \text { h. } \\ & 6.3 \mathrm{~V} \\ & \text { a.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & -\mathrm{ve} \\ & 10 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 3 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & s \\ & - \end{aligned}$ |
| V405 | ECC88 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 300 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 160 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathbf{k}^{\prime \prime \prime} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |  | $\overrightarrow{\mathrm{h}} \overrightarrow{6 \cdot 3 \mathrm{~V}}$ a.c. | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 240 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime} \\ & 176 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{k}^{\prime} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | s |
| V406 | ECF80 | $\begin{aligned} & \text { at } \\ & 300 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{gl} \\ & 0.15 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{g} 2 \\ & 37 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | h | $\begin{aligned} & \hline \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \\ & \text { a.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { ap } \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{kp}, \mathrm{~g} 3, \mathrm{~s} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{kt} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{gt} \\ & 180 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |
| V407 | ECC88 | $\begin{array}{\|l\|} \hline \mathrm{a}^{\prime \prime} \\ 215 \mathrm{~V} \\ \text { d.c. } \\ \hline \end{array}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime \prime} \\ & 80 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime \prime} \\ & 85 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | h | $\begin{aligned} & \mathrm{h} \\ & \overrightarrow{6 \cdot 3} \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{a}^{\prime} \\ & 215 \mathrm{~V} \\ & \text { d.c. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{g}^{\prime} \\ & 80 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{k}^{\prime} \\ & 85 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ |  |
| V408 | ECC88 | $\begin{aligned} & \hline \mathrm{a}^{\prime \prime} \\ & 80 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime \prime} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k}^{\prime \prime} \\ & 4 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\mathrm{h}$ | $\begin{aligned} & \hline \mathrm{h} \\ & 6 \cdot 3 \mathrm{~V} \\ & \text { a.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{a}^{\prime} \\ & 80 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | $\begin{aligned} & \mathrm{g}^{\prime} \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{k}^{\prime} \\ & 4 \mathrm{~V} \\ & \text { d.c. } \end{aligned}$ | s |

* The reading was taken between the heater pins.
++ The voltage between the strapped pins, 4 and 5 , and pin 9 was 6.3 V a.c.
V100, V200, V205-V207, V301-V303, V305-V309, V409-V411
Nominal burning voltage of miniature neons CC3L is 65 V , but variations can be expected between samples in the range 55 V to 80 V .


Fig. 3 Left-hand Side View of Model 2000


Fig. 4 Enlarged View of Y1 Amplifier Circuit (Model 2000)


Fir. 5 Right-hand Side View of Model 2000


Fig. 6 Enlarged View of Y2 Amplifier Circuit (Model 2000)


Fig. 7 Top View of Model 2000


Fig. 8 Enlarged View of E.H.T. Circuit $\mathcal{E}$ Bright-up and $20 \mathrm{Mc} / \mathrm{s}$ Generator Circuit (Model 2000)


Fig. 9 Bottom View of Model 2000


Fig. 10 Enlarged View of Time-base Circuit (Trig. Amplifier) Model 2000


Fig. 11 Enlarged View of Time-base Circuit (X Amplifier) Model 2000

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Fig. 12 Left-hand Side View of Model 2100


Fig. 13 Enlarged View of Y1 Amplifier Circuit (Model 2100)


Fig. 14 Right-hand Side View of Model 2100


Fig. 15 Enlarged View of Y2 Amplifier Circuit (Model 2100)


Fig. 16 Top View of Model 2100


Fig. 17 Enlarged View of E.H.T. Circuit \& Bright-up and $20 \mathrm{Mc} / \mathrm{s}$ Generator Circuit (Model 2100)


Fig. 18 Bottom View of Model 2100


Fig. 19 Enlarged View of Time-base Circuit (Trig. Amplifier) Model 2100


Fig. 20 Enlarged View of Time-base Circuit (X Amplifier) Model 2100

## CIRCUIT COMPONENTS-MODEL 2000

N.B. When ordering components, always quote the instrument serial number that is marked at the rear of the instrument.

| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R100 | $667 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.75 W | ITB.3505/C23/667 kת/02 |
| R101 | $233 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C2I/233 k $/$ /02 |
| R102 | $66 \cdot 7 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C21/66.7 k $/ 02$ |
| R103 | $23.3 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB. $3505 / \mathrm{C} 21 / 23.3 \mathrm{k} \Omega / 02$ |
| R104 | $6.67 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C21/6.67 k $/$ /02 |
| R105 | $2.33 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C21/2.33 k $/$ /02 |
| R106 | $1 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3500/C21/10202 |
| R107 | $270 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3500/C21/27402 |
| R108 | $20 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3500/C21/20302 |
| R109 | $2 \cdot 2 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3500/C21/22202 |
| R111 | $4.7 \mathrm{M} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/47510 |
| R112 | $10 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10010 |
| R113 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/22410 |
| R114 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/27310 |
| R115 | $5 \cdot 6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56210 |
| R116 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R117 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27210 |
| R118 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/22210 |
| R119 | $120 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/12410 |
| R121 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTT} / 47310$ |
| R122 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1.5 W | ITB. $3501 / 3101 / 2 \cdot 7 \mathrm{k} \Omega / 10$ |
| R123 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | $1 \cdot 5 \mathrm{~W}$ | ITB. $3501 / 3101 / 2 \cdot 7 \mathrm{k} \Omega / 10$ |
| R124 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5 \cdot 6 \mathrm{k} \Omega / 10$ |
| R125 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R126 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R127 | $100 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/10110 |
| R128 | $39 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/39310 |
| R129 | 390 ת | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/39110 |
| R130 | $1 \cdot 2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/12210 |
| R131 | $1 \cdot 2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 12210$ |
| R132 | 390 ת | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39110 |
| R133 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R134 | $220 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/22110 |
| R135 | $56 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/56010 |
| R136 | $56 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/56010 |
| R137 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R138 | $470 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/47110 |
| R139 | $470 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/47110 |
| R140 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5 \cdot 6 \mathrm{k} \Omega / 10$ |
| R141 | $220 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 22110$ |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R142 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R143 | $100 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10110 |
| R144 | $100 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10110 |
| R145 | $270 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27410 |
| R146 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R147 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R148 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R149 | $27 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27010 |
| R150 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/27310 |
| R200 | $667 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.75 W | ITB.3505/C23/667 kS/02 |
| R201 | $233 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C21/233 k $/$ /02 |
| R202 | $66 \cdot 7 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.3505/C21/66.7 k $/$ /02 |
| R203 | $23.3 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C21/23.3 k $/ 02$ |
| R204 | $6.67 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.3505/C21/6.67 k $/$ /02 |
| R205 | $2.33 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.3505/C21/2.33 k $/ 02$ |
| R206 | $1 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.3500/C21/10202 |
| R207 | $100 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10110 |
| R208 | $100 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10110 |
| R211 | $4.7 \mathrm{M} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/47510 |
| R212 | $10 \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 10010$ |
| R213 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R214 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27310 |
| R215 | $5 \cdot 6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56210 |
| R216 | $56 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/56010 |
| R217 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/27210 |
| R218 | $2 \cdot 2 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/22210 |
| R219 | $56 \Omega$ | $+10 \%$ | 0.5 W | ITB.3507/BTT/5601 |
| R220 | $82 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/82310 |
| R221 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R223 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5 \cdot 6 \mathrm{k} \Omega / 10$ |
| R224 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5.6 \mathrm{k} \Omega / 10$ |
| R225 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R226 | $100 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/10110 |
| R227 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R228 | $39 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 39310$ |
| R229 | $390 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB. $3507 / \mathrm{BTT} / 39110$ |
| R230 | $1.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 12210$ |
| R231 | $1.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/12210 |
| R232 | $390 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39110 |
| R233 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R234 | $220 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22110 |
| R235 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R236 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R238 | $470 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 47110$ |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R239 | $470 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/47110 |
| R240 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5 \cdot 6 \mathrm{k} \Omega / 10$ |
| R241 | $220 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/22110 |
| R242 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R243 | $150 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/15410 |
| R244 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27210 |
| R245 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27210 |
| R246 | $150 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/15410 |
| R247 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R248 | $27 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27010 |
| R249 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/27310 |
| R300 | $500 \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 500 \Omega / 10$ |
| R301 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47310 |
| R302 | $390 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39410 |
| R303 | $68 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/68310 |
| R304 | $56 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/56010 |
| R305 | $820 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 82410$ |
| R306 | $390 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/39410 |
| R307 | $390 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. 3507/BTA/39410 |
| R308 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10510 |
| R309 | $5.6 \mathrm{M} \Omega$ | $\pm 5 \%$ | 2 W | ITB.3500/C25/56505 |
| R311 | $10 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10310 |
| R312 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47410 |
| R313 | $10 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10310 |
| R314 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R315 | $680 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/68410 |
| R316 | $680 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/68410 |
| R317 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R318 | $150 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/15410 |
| R319 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R320 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R321 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R322 | $560 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56410 |
| R323 | $68 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 68310$ |
| R324 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47410 |
| R325 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 47410$ |
| R326 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R327 | $22 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 22310$ |
| R328 | $100 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/10110 |
| R329 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47410 |
| R330 | $680 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/68410 |
| R331 | $22 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22310 |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R401 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47310 |
| R402 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 10410$ |
| R403 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/33310 |
| R406 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R407 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R408 | $1 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10210 |
| R409 | $1 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/10210 |
| R410 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 33310$ |
| R411 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. 3507/BTA/33310 |
| R412 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R413 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R414 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47410 |
| R415 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R416 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R417 | $120 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/12410 |
| R418 | $1.2 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/12510 |
| R419 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/33310 |
| R420 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/27310 |
| R421 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R422 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27310 |
| R423 | $10 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10310 |
| R424 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R425 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27310 |
| R426 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R427 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22210 |
| R428 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22210 |
| R429 | $18 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/18310 |
| R430 | $2.2 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22510 |
| R431 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R432 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R433 | $6.8 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/68210 |
| R434 | $270 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/27410 |
| R435 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R436 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R437 | $390 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.5 W | ITB.3500/C22/39402 |
| R438 | $390 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39410 |
| R439 | $39 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/39310 |
| R440 | $10 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10310 |
| R441 | $10 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10310 |
| R442 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R443 | $18 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. 3507/BTA/18310 |
| R444 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R445 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R446 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R447 | $1 \mathrm{M} \Omega$ | $\pm 2 \%$ | 0.5 W | ITB.3500/C22/10502 |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R448 | $330 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/33110 |
| R449 | $9 \mathrm{M} \Omega$ | $\pm 2 \%$ | 0.5 W | ITB.3500/C22/90502 |
| R450 | $150 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/15410 |
| R451 | $1 \mathrm{M} \Omega$ | $\pm 2 \%$ | 0.5 W | ITB.3500/C22/10502 |
| R452 | $110 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.3500/C21/11402 |
| R453 | $22 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22310 |
| R455 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R456 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R457 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R458 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/47410 |
| R460 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R461 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/33310 |
| R462 | $1 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10210 |
| R463 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/10510 |
| R464 | $15 \mathrm{k} \Omega$ | $\pm 5 \%$ | $4 \cdot 5 \mathrm{~W}$ | ITB. $3501 / 3111 / 15 \mathrm{k} \Omega / 05$ |
| R465 | $15 \mathrm{k} \Omega$ | $\pm 5 \%$ | 4.5 W | ITB. $3501 / 3111 / 15 \mathrm{k} \Omega / 05$ |
| R466 | $330 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/33410 |
| R467 | $2 \cdot 2 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/22210 |
| R468 | $330 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/33410 |
| R469 | $1 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/10210 |
| R470 | $56 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/56010 |
| R471 | $56 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/56010 |
| R472 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/22210 |
| R473 | $18 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/18310 |
| R474 | $18 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/18310 |
| R475 | $560 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56410 |
| R479 | $56 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/56010 |
| R480 | $68 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/68310 |
| R481 | $22 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22310 |
| R482 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R483 | $1.5 \mathrm{M} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/15510 |
| R484 | $220 \mathrm{k} \Omega$ | $\pm 5 \%$ | 0.25 W | ITB.3500/C21/22405 |
| R485 | $220 \mathrm{k} \Omega$ | $\pm 5 \%$ | 0.25 W | ITB.3500/C21/22405 |
| R486 | $120 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/12410 |
| R487 | $1.2 \mathrm{k} \Omega$ | $\pm 5 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.3500/C21/12205 |
| R489 | $1.5 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/15210 |
| R490 | $330 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/33410 |
| R491 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R492 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R493 | $12 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/12310 |
| R494 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R495 | $56 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/56010 |
| R496 | $270 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/27110 |
| R497 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/33310 |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R501 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R502 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. 3507/BTA/10410 |
| R503 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R504 | $3.9 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39210 |
| R505 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 33310$ |
| R506 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22210 |
| R509 | $680 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/68110 |
| R510 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R511 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| C100 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C101 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C102 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C103 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C104 | 33 pF | $\pm 2 \mathrm{pF}$ | 125 V | ITB.6027/33/2/125 d.c. |
| C105 | 120 pF | $\pm 5 \%$ | 125 V | ITB.6027/120/6/125 d.c. |
| C106 | 430 pF | $\pm 5 \%$ | 125 V | ITB.6027/430/20.5/125 d.c. |
| C107 | 1500 pF | $\pm 5 \%$ | 125 V | ITB.6027/1500/75/125 d.c. |
| C108 | 3200 pF | $\pm 5 \%$ | 125 V | ITB.6027/3200/160/125 d.c. |
| C109 | $8 \mu \mathrm{~F}$ | + $50 \%-20 \%$ | 275 V | ITB.7001/24S |
| C111 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C112 | 120 pF | $\pm 5 \%$ | 125 V | ITB.6027/120/6/125 d.c. |
| C113 | $25 \mu \mathrm{~F}$ | $+100 \%-20 \%$ | 6 V | IVB.7006/75S |
| C114 | 10 pF | $\pm 1 \mathrm{pF}$ | 350 V | ITB.6027/10/1/350 d.c. |
| C116 | 4700 pF | +80\% - $20 \%$ | 500 V | ITB.6045/8 |
| C117 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C118 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C119 | $8 \mu \mathrm{~F}$ | +50\% - $20 \%$ | 275 V | ITB.7001/24S |
| C121 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C122 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C123 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C124 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C125 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C126 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C127 | $0.002 \mu \mathrm{~F}$ | $\pm 20 \%$ | 400 V | IUB.6001/16 |
| C128 | 4700 pF | $\pm 10 \%$ | 125 V | ITB.6027/4700/470/125 d.c. |
| C129 | 500 pF | $\pm 10 \%$ | 125 V | ITB.6027/500/50/125 d.c. |
| C130 | 9.1 pF | $\pm 0.5 \mathrm{pF}$ | 750 V | ITB.6029/17 |
| C131 | 5 pF | $\pm 1 \mathrm{pF}$ | 750 V | ITB.6029/2 |
| C135 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C136 | 330 pF | $\pm 10 \%$ | 125 V | ITB.6027/330//33 125 d.c. |
| C137 | $10-60 \mathrm{pF}$ |  | 250 V | ISB.6510/14 |
| C138 | 800 pF | +80\% - $20 \%$ | 500 V | ITB.6044/4 |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| C200 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C201 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C202 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C203 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C204 | 33 pF | $\pm 2 \mathrm{pF}$ | 125 V | ITB.6027/33/2/125 d.c. |
| C205 | 120 pF | $\pm 5 \%$ | 125 V | ITB. $6027 / 120 / 6 / 125$ d.c. |
| C206 | 430 pF | $\pm 5 \%$ | 125 V | ITB. $6027 / 430 / 20 \cdot 5 / 125$ d.c. |
| C207 | 1500 pF | $\pm 5 \%$ | 125 V | ITB. $6027 / 1500 / 75 / 125$ d.c. |
| C208 | 3200 pF | $\pm 5 \%$ | 125 V | ITB.6027/3200/160/125 d.c. |
| C209 | $8 \mu \mathrm{~F}$ | $+50 \%-20 \%$ | 275 V | ITB. $7001 / 24 \mathrm{~S}$ |
| C210 | 500 pF | $\pm 10 \%$ | 125 V | ITB.6027/500/50/125 d.c. |
| C211 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C212 | 120 pF | $\pm 5 \%$ | 125 V | ITB.6027/120/6/125 d.c. |
| C213 | $25 \mu \mathrm{~F}$ | +100\% -20\% | 6 V | IVB. $7006 / 75 \mathrm{~S}$ |
| C216 | 4700 pF | +80\% -20\% | 500 V | ITB.6045/8 |
| C217 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C218 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C219 | $8 \mu \mathrm{~F}$ | +50\%-20\% | 275 V | ITB.7001/24S |
| C221 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C222 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C223 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C224 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C225 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C226 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C227 | $0.002 \mu \mathrm{~F}$ | $\pm 20 \%$ | 400 V | IUB.6001/16 |
| C230 | $9 \cdot 1 \mathrm{pF}$ | $\pm 0.5 \mathrm{pF}$ | 750 V | ITB.6029/17 |
| C231 | 5 pF | $\pm 1 \mathrm{pF}$ | 750 V | ITB.6029/2 |
| C235 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C236 | 330 pF | $\pm 10 \%$ | 125 V | ITB.6027/330/33/125 d.c. |
| C237 | $10-60 \mathrm{pF}$ |  | 250 V | ISB.6510/14 |
| C300 | $60 \mu \mathrm{~F}$ | +50\% - $20 \%$ | 350 V | 2IUB.7017/4 |
| C302 | $150 \mu \mathrm{~F}$ | +50\%-20\% | 150 V | IUB.7017/3 |
| C303 | $200 \mu \mathrm{~F}$ | +50\%-20\% | 150 V | IUB.7017/2 |
| C304 | $0.5 \mu \mathrm{~F}\}$ | $\pm 20 \%$ | 1 kV | 3ITB.6042/2 |
| C305 | $0.5 \mu \mathrm{~F}\}$ | $\pm 20 \%$ | 1 kV | \} |
| C306 | $0.047 \mu \mathrm{~F}$ | $\pm 20 \%$ | 250 V | ITB.6047/4 |
| C307 | 100 pF | $\pm 20 \%$ | 3500 V | IUB.6005/4 |
| C309 | 22 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB. $6027 / 22 / 2 / 350$ d.c. |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| C310 | $0.03 \mu \mathrm{~F}$ | +80\% -20\% | 1500 V | ISB. 6048 |
| C311 | $9 \cdot 1 \mathrm{pF}$ | $\pm 0.5 \mathrm{pF}$ | 750 V | ITB.6029/17 |
| C312 | $0.03 \mu \mathrm{~F}$ | $+80 \%-20 \%$ | 1500 V | ISB. 6048 |
| C313 | $0.03 \mu \mathrm{~F}$ | + 80\% - $20 \%$ | 1500 V | ISB. 6048 |
| C314 | 1000 pF | $+80 \%-20 \%$ | 500 V | ITB.6044/5 |
| C315 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C316 | $1 \mu \mathrm{~F}$ | $+100 \%-20 \%$ | 350 V | IUB.7017/5 |
| C401 | $1 \mu \mathrm{~F}$ | +100\%-20\% | 350 V | IUB.7017/5 |
| C402 | $3 \cdot 3 \mathrm{pF}$ | $\pm 0.5 \mathrm{pF}$ | 750 V | ITB.6029/16 |
| C403 | $3 \cdot 3 \mathrm{pF}$ | $\pm 0.5 \mathrm{pF}$ | 750 V | ITB.6029/16 |
| C404 | 1000 pF | $+80 \%-20 \%$ | 500 V | ITB.6044/5 |
| C405 | 3300 pF | $\pm 10 \%$ | 350 V | ITB. $6027 / 3300 / 330 / 350$ d.c. |
| C406 | $1 \mu \mathrm{~F}$ | +100\% - $20 \%$ | 350 V | IUB.7017/5 |
| C407 | 120 pF | $\pm 2 \%$ | 350 V | ITB. $6027 / 120 / 2 \cdot 4 / 350$ d.c. |
| C408 | 600 pF | $\pm 2 \%$ | 350 V | ITB.6027/600/12/350 d.c. |
| C409 | 3300 pF | $\pm 10 \%$ | 350 V | ITB.6027/3300/330/350 d.c. |
| C410 | $0.01 \mu \mathrm{~F}$ | $\pm 20 \%$ | 500 V | ITB.6047/3 |
| C411 | 33 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB.6027/33/2/350 d.c. |
| C412 | 800 pF | +80\% -20\% | 500 V | ITB.6044/4 |
| C413 | 1000 pF | $+80 \%-20 \%$ | 500 V | ITB.6044/5 |
| C414 | 39 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB. $6027 / 39 / 2 / 350$ d.c. |
| C416 | $8 \mu \mathrm{~F}$ | $+50 \%-20 \%$ | 275 V | ITB. $7001 / 24 \mathrm{~S}$ |
| C418 | 100 pF | $\pm 5 \%$ | 125 V | ITB.6027/100/5/125 d.c. |
| C419 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C420 | 82 pF | $\pm 2 \mathrm{pF}$ | 125 V | ITB.6027/82/2/125 d.c. |
| C421 | 15 pF | $\pm 1 \mathrm{pF}$ | 350 V | ITB. $6027 / 15 / 1 / 350$ d.c. |
| C422 | 40 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB. $6027 / 40 / 2 / 350$ d.c. |
| C423 | 400 pF | $\pm 2 \%$ | 350 V | ITB.6027/400/8/350 d.c. |
| C424 | 200 pF | $\pm 2 \%$ | 350 V | ITB. 6027/200/4/350 d.c. |
| C425 | 4000 pF | $\pm 2 \%$ | 350 V | ITB.6027/4000/80/350 d.c. |
| C426 | 2000 pF | $\pm 2 \%$ | 350 V | ITB.6027/2000/40/350 d.c. |
| C427 | $0.04 \mu \mathrm{~F}$ | $\pm 2 \%$ | 500 V | ITB. $6027 / 40000 / 800 / 500$ d.c. |
| C428 | $0.02 \mu \mathrm{~F}$ | $\pm 2 \%$ | 500 V | ITB.6027/20000/400/500 d.c. |
| C429 | $0.4 \mu \mathrm{~F}$ | $\pm 2 \%$ | 500 V | ITB.6043/3 |
| C430 | $0 \cdot 2 \mu \mathrm{~F}$ | $\pm 2 \%$ | 500 V | ITB.6043/2 |
| C431 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C432 | 18 pF | $\pm 1 \mathrm{pF}$ | 350 V | ITB.6027/18/1/350 d.c. |
| C433 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C435 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C436 | 1-6 pF |  | 500 V | ISB. 6506 |
| C437 | $0.01 \mu \mathrm{~F}$ | $\pm 20 \%$ | 500 V | ITB.6047/3 |
| C438 | $0.01 \mu \mathrm{~F}$ | $\pm 20 \%$ | 500 V | ITB.6047/3 |


| Ref. | Value | Tolerance |  | Rating | Part Number |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C439 | 4700 pF | +80\% | $\begin{aligned} & -20 \% \\ & -20 \% \end{aligned}$ | 500 V | ITB.6045/8 <br> ITB.6044/5 <br> ITB.6027/100/5/125 d.c. <br> ITB.6047/2 |  |
| C440 | 1000 pF | +80\% |  | 500 V |  |  |
| C441 | 100 pF | $\pm 5 \%$ |  | 125 V |  |  |
| C442 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ |  | 500 V |  |  |
| C443 | 33 pF | $\begin{aligned} & \pm 2 \mathrm{pF} \\ & \pm 10 \% \\ & +50 \% \end{aligned}$ | -20\% | 350 V | ITB. $6027 / 33 / 2 / 350$ d.c. <br> ITB.6047/2 <br> ITB. $7001 / 24 \mathrm{~S}$ <br> ISB. 6506 |  |
| C444 | $0 \cdot 1 \mu \mathrm{~F}$ |  |  | 500 V |  |  |
| C445 | $8 \mu \mathrm{~F}$ |  |  | 275 V |  |  |
| C446 | $1-6 \mathrm{pF}$ |  |  | 500 V |  |  |
| RV100 | $500 \Omega$ | $\begin{aligned} & \pm 20 \% \\ & \pm 20 \% \\ & +20 \% \end{aligned}$ |  | 0.1 W | IUB. $8021 / 50120 / 15 \mathrm{~F}$ <br> IUB.8026/5 <br> ITB. 8025/174/10420 |  |
| RV101 | $250 \mathrm{k} \Omega$ |  |  | 0.5 W |  |  |
| RV102 | $100 \mathrm{k} \Omega$ |  |  | $0 \cdot 25 \mathrm{~W}$ |  |  |
| RV200 | $500 \Omega$ | $\begin{aligned} & \pm 20 \% \\ & \pm 20 \% \end{aligned}$ |  | 0.1 W | ITB.8021/50120/15F IUB.8026/5 |  |
| RV201 | $250 \mathrm{k} \Omega$ |  |  | $0 \cdot 5 \mathrm{~W}$ |  |  |
| RV300 | $500 \mathrm{k} \Omega$ | $\begin{aligned} & \pm 20 \% \\ & \pm 20 \% \\ & \pm 20 \% \\ & \pm 20 \% \\ & \pm 20 \% \end{aligned}$ |  | 0.25 W | $\begin{aligned} & \text { ITB. } 8038 / 2 \\ & \text { ITB. } 8025 / 174 / 25420 \\ & \text { ITB. } 8038 \\ & \text { ITB. } 8038 \\ & \text { ISB. } 8000 / 30320 \end{aligned}$ |  |
| RV301 | $250 \mathrm{k} \Omega$ |  |  | 0.25 W |  |  |
| RV302 | $1 \mathrm{M} \Omega$ |  |  | 0.25 W |  |  |
| RV303 | $1 \mathrm{M} \Omega$ |  |  | 0.25 W |  |  |
| RV304 | $30 \mathrm{k} \Omega$ |  |  | $0 \cdot 5 \mathrm{~W}$ |  |  |
| RV305 | $50 \Omega$ | $\begin{aligned} & \pm 10 \% \\ & \pm 20 \% \end{aligned}$ |  | 2 W | $\begin{aligned} & \text { IUB. } 8002 / 50010 / 11 \\ & \text { ITB. } 8038 / 2 \end{aligned}$ |  |
| RV306 | $500 \mathrm{k} \Omega$ |  |  | $0 \cdot 25 \mathrm{~W}$ |  |  |
| RV401 | $220 \mathrm{k} \Omega$ | $\pm 20 \%$$\pm 20 \%$$\pm 20 \%$$\pm 20 \%$$\pm 20 \%$ |  | $0 \cdot 5 \mathrm{~W}$ | ITB. 8043/2 (with RV404) IUB.8026/4 <br> ITB.8025/174/10420 <br> ITB.8043/2 (with RV401) <br> ITB.8043/3 (with RV408) |  |
| RV402 | $1 \mathrm{M} \Omega$ |  |  | $0 \cdot 5 \mathrm{~W}$ |  |  |
| RV403 | $100 \mathrm{k} \Omega$ |  |  | 0.25 W |  |  |
| RV404 | $500 \mathrm{k} \Omega$ |  |  | 0.5 W |  |  |
| RV405 | $250 \mathrm{k} \Omega$ |  |  | 0.5 W |  |  |
| RV406 | $100 \mathrm{k} \Omega$ | $\begin{aligned} & \pm 20 \% \\ & \pm 20 \% \\ & \pm 20 \% \end{aligned}$ |  | 0.25 W | ITB.8025/174/10420 <br> ITB.8025/174/27310 <br> ITB. $8043 / 3$ (with RV405) |  |
| RV407 | $27 \mathrm{k} \Omega$ |  |  | 0.25 W |  |  |
| RV408 | $10 \mathrm{k} \Omega$ |  |  | $0 \cdot 5 \mathrm{~W}$ |  |  |
| RV409 | $200 \Omega$ | $\begin{aligned} & \pm 10 \% \\ & \pm 10 \% \\ & \pm 10 \% \end{aligned}$ |  | 0.5 W | $\begin{aligned} & \text { ITB. } 8025 / 196 / 20110 \\ & \text { ITB. } 8025 / 196 / 20210 \\ & \text { ITB. } 8025 / 196 / 20210 \end{aligned}$ |  |
| RV410 | $2 \mathrm{k} \Omega$ |  |  | 0.5 W |  |  |
| RV411 | $2 \mathrm{k} \Omega$ |  |  | $0 \cdot 5 \mathrm{~W}$ |  |  |
| Valve | Type | Valve |  | Type | Valve | Type |
| V100 | CC3L | V102 |  | ECC88 | V104 | EF184 |
| V101 | ECF80 | V103 |  | EF184 | V105 | ECC81 |
| V200 | CC3L | $\begin{aligned} & \text { V203 } \\ & \text { V204 } \\ & \text { V205 } \end{aligned}$ |  | EF184 | $\begin{aligned} & \text { V206 } \\ & \text { V207 } \end{aligned}$ | $\begin{aligned} & \text { CC3L } \\ & \text { CC3L } \end{aligned}$ |
| V201 | ECF80 |  |  | EF184 |  |  |
| V202 | ECC88 |  |  | CC3L |  |  |


| Valve | Type | Valve | Type | Valve | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
| V300 | ECF80 | V303 | CC3L | V306 | CC3L |
| V301 | CC3L | C304 | ECC88 | V307 | CC3L |
| V302 | CC3L | V305 | CC3L | V308 | CC3L |
| V401 | ECC88 |  |  |  |  |
| V402 | ECC88 | V405 | ECC88 | V408 | ECC88 |
| V403 | ECC88 | V406 | ECF80 | V409 | CC3L |
| V404 | ECC88 | V407 | ECC88 | V410 | CC3L |
| Ref. | Descrip |  |  |  | Part Number |
| L100 | Inducto |  |  |  | KA.88112/4 |
| L101 | Inducto |  |  |  | KA.88112/4 |
| L200 | Inducto |  |  |  | KA.88112/4 |
| L201 | Inducto |  |  |  | KA.88112/4 |
| L300 | Inducto |  |  |  | ITB. 3017 |
| $\begin{aligned} & \text { L301 } \\ & \text { L302 } \end{aligned}$ | Inducto |  |  |  | ISA.262/63 |
| L403 | Inducto |  |  |  | KA.88089/10 |
| T300 | Transfo |  |  |  | IUB. 3016 |
| LP300 | Lamp, | g, 0.36 |  |  | ISB. 5021 |
| LP301 | Lamp, | g, 0.63 |  |  | ISB. 5021 |
| F. 300 | Fuse, 2 |  |  |  | ISB.5002/2 |
| CRT | Cathode |  |  |  | 4SP31 |
| MR300 | Rectifier |  |  |  | ISB.9013/6 |
| MR301 | Rectifier |  |  |  | ISB.9013/6 |
| MR302 | Rectifier |  |  |  | ISB.9013/6 |
| MR303 | Rectifier |  |  |  | ISB.9013/6 |
| $\begin{aligned} & \text { MR304 } \\ & \text { MR305 } \\ & \text { MR306 } \\ & \text { MR307 } \end{aligned}$ | Rectifier (manufa | ct cooled a sing |  |  | ISB. 9006 |
| $\begin{aligned} & \text { MR308 } \\ & \text { MR309 } \\ & \text { MR310 } \end{aligned}$ | Rectifie <br> Rectifier <br> Rectifie | ar ${ }_{\text {ar }}^{\text {ar }}$ |  |  | $\begin{aligned} & \text { ISB. } 9004 / 2 \\ & \text { ISB. } 9004 / 2 \\ & \text { ISB. } 9012 \end{aligned}$ |


| Ref. | Description | Part Number |
| :---: | :---: | :---: |
| $\left.\begin{array}{l}\text { MR401 } \\ \text { MR402 } \\ \text { MR403 } \\ \text { MR404 } \\ \text { MR405 } \\ \text { MR406 }\end{array}\right\}$ | Rectifiers, Germanium Diodes | ISB. 9009 |
| $\left.\begin{array}{l} \text { MR407 } \\ \text { MR408 } \\ \text { MR409 } \end{array}\right\}$ | Rectifier, Miniature H.F. <br> Rectifiers, Germanium Diodes | ITB. 9012 ISB. 9009 |
| $\begin{aligned} & \text { S100 } \\ & \text { S101 } \end{aligned}$ | Switch, Rotary, AC-DC-CAL Switch, Rotary, ATTENUATOR | $\begin{aligned} & \text { ITB. } 262 / 25 \\ & \text { ITB.262/22 } \end{aligned}$ |
| $\begin{aligned} & \text { S200 } \\ & \text { S201 } \end{aligned}$ | Switch, Rotary, AC-DC-CAL Switch, Rotary, ATTENUATOR | $\begin{aligned} & \text { ITB. } 262 / 25 \\ & \text { ITB. } 262 / 22 \end{aligned}$ |
| $\begin{aligned} & \text { S300 } \\ & \text { S301 } \end{aligned}$ | Switch, Rotary, INTENSITY MOD. Switch, Toggle, MAINS ON/OFF | $\begin{aligned} & \text { ISB. } 4014 \\ & \text { ISB. } 4013 / 6 \end{aligned}$ |
| S400  <br> S401 $\}$ <br> S402 $\}$ <br> S403 $\}$ <br> S405  | Switch, Rotary, TRIG. SYSTEM \& TRIG. SELECTOR Switch, Rotary, TIME/CM \& MULTIPLIER Switch, Rotary, DELAY RANGE | ITB.262/20 ITB.262/21 ITB.262/24 |
| SKT100 SKT101 SKT102 | Terminal, (Maroon) Socket, Coaxial (Amphenol) Terminal, (Black) | $\begin{aligned} & \text { ISB. } 5504 / 3 \\ & \text { ISB. } 2516 \\ & \text { ISB. } 5504 \end{aligned}$ |
| $\begin{aligned} & \text { SKT200 } \\ & \text { SKT201 } \\ & \text { SKT202 } \end{aligned}$ | Terminal, (Maroon) <br> Socket, Coaxial (Amphenol) <br> Terminal, (Black) | $\begin{aligned} & \text { ISB. } 5504 / 3 \\ & \text { ISB. } 2516 \\ & \text { ISB. } 5504 \end{aligned}$ |
| SKT300 | Terminal (Black) | ISB. 5504 |
| $\begin{aligned} & \text { SKT401 } \\ & \text { SKT403 } \end{aligned}$ | Terminal, (Maroon) Terminal, (Maroon) | $\begin{aligned} & \text { ISB.5504/3 } \\ & \text { ISB.5504/3 } \end{aligned}$ |

## CIRCUIT COMPONENTS - MODEL 2100

N.B. When ordering components, always quote the instrument serial number that is marked at the rear of the instrument.

| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R100 | $667 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.75 W | ITB. $3505 / \mathrm{C} 23 / 667 \mathrm{k} \Omega / 02$ |
| R101 | $233 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C21/233 k $\Omega / 02$ |
| R102 | $66.7 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25$ W | ITB.3505/C21/66.7 k $/$ /02 |
| R103 | $23.3 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C21/23.3 k $/$ /02 |
| R104 | $6.67 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB. $3505 / \mathrm{C} 21 / 6.67 \mathrm{k} \Omega / 02$ |
| R105 | $2.33 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.3505/C21/2.33 k $/$ /02 |
| R106 | $1 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25$ W | ITB.3500/C21/10202 |
| R107 | $91 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3500/C21/91302 |
| R108 | $9 \cdot 1 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.3500/C21/91202 |
| R109 | $1 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3500/C21/10202 |
| R111 | $4.7 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47510 |
| R112 | $10 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10010 |
| R113 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R114 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27310 |
| R115 | $5 \cdot 6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 56210$ |
| R116 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R117 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27210 |
| R118 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22210 |
| R119 | $120 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/12410 |
| R121 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 47310$ |
| R122 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1.5 W | ITB. $3501 / 3101 / 2 \cdot 7 \mathrm{k} \Omega / 10$ |
| R123 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1.5 W | ITB. $3501 / 3101 / 2 \cdot 7 \mathrm{k} \Omega / 10$ |
| R124 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5 \cdot 6 \mathrm{k} \Omega / 10$ |
| R125 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R126 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 10110$ |
| R127 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/10110 |
| R128 | $39 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTT} / 39310$ |
| R129 | $390 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39110 |
| R130 | $1.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/12210 |
| R131 | $1.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 12210$ |
| R132 | $390 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39110 |
| R133 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R134 | $220 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22110 |
| R135 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R136 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/56010 |
| R137 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R138 | $470 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/47110 |
| R139 | $470 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47110 |
| R140 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5 \cdot 6 \mathrm{k} \Omega / 10$ |
| R141 | $220 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22110 |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R142 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R143 | $100 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10110 |
| R144 | $100 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10110 |
| R145 | $270 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27410 |
| R146 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R147 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R148 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R149 | $27 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27010 |
| R150 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/27310 |
| R151 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R152 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R200 | $667 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.75 W | ITB. $3505 / \mathrm{C} 23 / 667 \mathrm{k} \Omega / 02$ |
| R201 | $233 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.3505/C21/233 k $/ 02$ |
| R202 | $66.7 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C21/66.7 k $/$ /02 |
| R203 | $23.3 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB. $3505 / \mathrm{C} 21 / 23.3 \mathrm{k} \Omega / 02$ |
| R204 | $6.67 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB. $3505 / \mathrm{C} 21 / 6 \cdot 67 \mathrm{k} \Omega / 02$ |
| R205 | $2.33 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3505/C21/2.33 kS/02 |
| R206 | $1 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 25$ W | ITB.3500/C21/10202 |
| R207 | $100 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10110 |
| R208 | $100 \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10110 |
| R211 | $4.7 \mathrm{M} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/47510 |
| R212 | $10 \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 10010$ |
| R213 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R214 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27310 |
| R215 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56210 |
| R216 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R217 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/27210 |
| R218 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22210 |
| R219 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/5601 |
| R220 | $82 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/82310 |
| R221 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R223 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5 \cdot 6 \mathrm{k} \Omega / 10$ |
| R224 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5 \cdot 6 \mathrm{k} \Omega / 10$ |
| R225 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R226 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R227 | $100 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/10110 |
| R228 | $39 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 39310$ |
| R229 | 390 ת | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39110 |
| R230 | $1.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/12210 |
| R231 | $1.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/12210 |
| R232 | 390 ת | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39110 |
| R233 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R234 | $220 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22110 |
| R235 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R236 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R238 | $470 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 47110$ |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R239 | $470 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/47110 |
| R240 | $5.6 \mathrm{k} \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 5.6 \mathrm{k} \Omega / 10$ |
| R241 | $220 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22110 |
| R242 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R243 | $150 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/15410 |
| R244 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27210 |
| R245 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27210 |
| R246 | $150 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/15410 |
| R247 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R248 | $27 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27010 |
| R249 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/27310 |
| R250 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R251 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R252 | $330 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/33410 |
| R300 | $500 \Omega$ | $\pm 10 \%$ | 3 W | ITB. $3501 / 3115 / 500 \Omega / 10$ |
| R301 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47410 |
| R302 | $390 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39410 |
| R304 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R305 | $680 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/68410 |
| R306 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R307 | $390 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/39410 |
| R308 | $2.7 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27510 |
| R309 | $5.6 \mathrm{M} \Omega$ | $\pm 5 \%$ | 2 W | ITB.3500/C25/56505 |
| R310 | $680 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/68410 |
| R311 | $10 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10310 |
| R312 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47410 |
| R313 | $10 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10310 |
| R315 | $680 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/68410 |
| R316 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/22410 |
| R317 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R318 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R319 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R320 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R321 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R322 | $180 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/18410 |
| R324 | $560 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/56410 |
| R326 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R327 | $22 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/22310 |
| R328 | $100 \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/10110 |
| R329 | $2.7 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 27510$ |
| R330 | $680 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/68410 |
| R331 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47410 |
| R333 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R334 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R335 | $2.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27210 |
| R336 | $1 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10210 |
| R337 | $2.7 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27510 |
| R338 | $3.3 \mathrm{M} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB. 3507/BTT/33510 |
| R401 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47310 |
| R402 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R403 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/33310 |
| R406 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R407 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 47210$ |
| R408 | $1 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10210 |
| R409 | $1 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10210 |
| R410 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/33310 |
| R411 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/33310 |
| R412 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R413 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R414 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47410 |
| R415 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R416 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R417 | $120 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/12410 |
| R418 | $1.2 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/12510 |
| R419 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/33310 |
| R420 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. 3507/BTA/27310 |
| R421 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R422 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/27310 |
| R423 | $10 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10310 |
| R424 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R425 | $27 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27310 |
| R426 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R427 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22210 |
| R428 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22210 |
| R429 | $18 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 18310$ |
| R430 | $2 \cdot 2 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22510 |
| R431 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R432 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 47310$ |
| R433 | $6.8 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 68210$ |
| R434 | $270 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27410 |
| R435 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R436 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R437 | $390 \mathrm{k} \Omega$ | $\pm 2 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3500/C22/39402 |
| R438 | $390 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39410 |
| R439 | $39 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/39310 |
| R440 | $10 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/10310 |
| R441 | $22 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. 3507/BTA/22310 |
| R442 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/22410 |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R443 | $18 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/18310 |
| R444 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R445 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R446 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R447 | $1 \mathrm{M} \Omega$ | $\pm 2 \%$ | 0.5 W | ITB.3500/C22/10502 |
| R448 | $330 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 33110$ |
| R449 | $9 \mathrm{M} \Omega$ | $\pm 2 \%$ | 0.5 W | ITB.3500/C22/90502 |
| R450 | $150 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/15410 |
| R451 | $1 \mathrm{M} \Omega$ | $\pm 2 \%$ | 0.5 W | ITB.3500/C22/10502 |
| R452 | $110 \mathrm{k} \Omega$ | $\pm 2 \%$ | 0.25 W | ITB.3500/C21/11402 |
| R453 | $22 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22310 |
| R455 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R456 | $220 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22410 |
| R457 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R458 | $470 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47410 |
| R461 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/33310 |
| R462 | $1.8 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/18210 |
| R463 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R464 | $15 \mathrm{k} \Omega$ | $\pm 5 \%$ | 4.5 W | ITB. $3501 / 3111 / 15 \mathrm{k} \Omega / 05$ |
| R465 | $15 \mathrm{k} \Omega$ | $\pm 5 \%$ | 4.5 W | ITB. $3501 / 3111 / 15 \mathrm{k} \Omega / 05$ |
| R466 | $330 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/33410 |
| R467 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R468 | $330 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/33410 |
| R469 | $1.8 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/18210 |
| R470 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R471 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R472 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R473 | $18 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/18310 |
| R474 | $18 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/18310 |
| R475 | $560 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56410 |
| R479 | $330 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 33410$ |
| R480 | $68 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/68310 |
| R481 | $22 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22310 |
| R482 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R483 | $330 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/33410 |
| R485 | $18 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/18310 |
| R486 | $1.8 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/18210 |
| R489 | $1.5 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/15210 |
| R490 | $1.8 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/18510 |
| R491 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R492 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R493 | $12 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/12310 |
| R494 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R495 | $56 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/56010 |
| R496 | $270 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/27110 |
| R497 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/33310 |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| R501 | $47 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/47310 |
| R502 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/10410 |
| R503 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R504 | $4.7 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/47210 |
| R505 | $33 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 33310$ |
| R506 | $2.2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/22210 |
| R509 | $680 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. $3507 / \mathrm{BTT} / 67110$ |
| R510 | $1 \mathrm{M} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10510 |
| R511 | $100 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10110 |
| R512 | $39 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39310 |
| R513 | $330 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/33110 |
| R514 | $330 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/33110 |
| R515 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R516 | $100 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/10410 |
| R517 | $390 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB. 3507/BTT/39410 |
| R518 | $560 \mathrm{k} \Omega$ | $\pm 10 \%$ | $0 \cdot 5 \mathrm{~W}$ | ITB.3507/BTT/56410 |
| R519 | $68 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB. $3507 / \mathrm{BTA} / 68310$ |
| R520 | $68 \mathrm{k} \Omega$ | $\pm 10 \%$ | 1 W | ITB.3507/BTA/68310 |
| R521 | $3.9 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.3507/BTT/39210 |
| C100 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C101 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C102 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C103 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C104 | 33 pF | $\pm 2 \mathrm{pF}$ | 125 V | ITB.6027/33/2/125 d.c. |
| C105 | 120 pF | $\pm 5 \%$ | 125 V | ITB.6027/120/6/125 d.c. |
| C106 | 430 pF | $\pm 5 \%$ | 125 V | ITB. $6027 / 430 / 20 \cdot 5 / 125$ d.c. |
| C107 | 1500 pF | $\pm 5 \%$ | 125 V | ITB.6027/1500/75/125 d.c. |
| C108 | 3200 pF | $\pm 5 \%$ | 125 V | ITB. $6027 / 3200 / 160 / 125$ d.c. |
| C109 | $8 \mu \mathrm{~F}$ | $+50 \%-20 \%$ | 275 V | ITB.7001/24S |
| C111 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C112 | 120 pF | $\pm 5 \%$ | 125 V | ITB.6027/120/6/125 d.c. |
| C113 | $25 \mu \mathrm{~F}$ | $+100 \%-20 \%$ | 6 V | IVB. $7006 / 75 \mathrm{~S}$ |
| C114 | 10 pF | $\pm 1 \mathrm{pF}$ | 350 V | ITB.6027/10/1/350 d.c. |
| C116 | 4700 pF | $+80 \%-20 \%$ | 500 V | ITB.6045/8 |
| C117 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C118 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C119 | $8 \mu \mathrm{~F}$ | $+50 \%-20 \%$ | 275 V | ITB.7001/24S |
| C121 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C122 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C 123 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C124 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C125 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C126 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C127 | $0 \cdot 002 \mu \mathrm{~F}$ | $\pm 20 \%$ | 400 V | IUB.6001/16 |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| C129 | 500 pF | $\pm 10 \%$ | 125 V | ITB.6027/500/50/125 d.c. |
| C130 | $9 \cdot 1 \mathrm{pF}$ | $\pm 0.5 \mathrm{pF}$ | 750 V | ITB.6029/17 |
| C131 | 5 pF | $\pm 1 \mathrm{pF}$ | 750 V | ITB.6029/2 |
| C135 | $0.1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C136 | 330 pF | $\pm 10 \%$ | 125 V | ITB.6027/330/33/125 d.c. |
| C137 | $10-60 \mathrm{pF}$ |  | 250 V | ISB.6510/14 |
| C138 | 800 pF | +80\% - $20 \%$ | 500 V | ITB.6044/4 |
| C200 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C201 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C202 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C203 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C204 | 33 pF | $\pm 2 \mathrm{pF}$ | 125 V | ITB.6027/33/2/125 d.c. |
| C205 | 120 pF | $\pm 5 \%$ | 125 V | ITB.6027/120/6/125 d.c. |
| C206 | 430 pF | $\pm 5 \%$ | 125 V | ITB.6027/430/20.5/125 d.c. |
| C207 | 1500 pF | $\pm 5 \%$ | 125 V | ITB. $6027 / 1500 / 75 / 125$ d.c. |
| C208 | 3200 pF | $\pm 5 \%$ | 125 V | ITB.6027/3200/160/125 d.c. |
| C209 | $8 \mu \mathrm{~F}$ | +50\%-20\% | 275 V | ITB.7001/24S |
| C210 | 500 pF | $\pm 10 \%$ | 125 V | ITB.6027/500/50/125 d.c. |
| C211 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C212 | 120 pF | $\pm 5 \%$ | 125 V | ITB.6027/120/6/125 d.c. |
| C213 | $25 \mu \mathrm{~F}$ | +100\% - $20 \%$ | 6 V | IVB.7006/75S |
| C216 | 4700 pF | +80\% - $20 \%$ | 500 V | ITB.6045/8 |
| C217 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C218 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C219 | $8 \mu \mathrm{~F}$ | +50\%-20\% | 275 V | ITB.7001/24S |
| C221 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C222 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C223 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C224 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C225 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C226 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C227 | $0.002 \mu \mathrm{~F}$ | $\pm 20 \%$ | 400 V | IUB.6001/16 |
| C230 | $9 \cdot 1 \mathrm{pF}$ | $\pm 0.5 \mathrm{pF}$ | 750 V | ITB.6029/17 |
| C231 | 5 pF | $\pm 1 \mathrm{pF}$ | 750 V | ITB.6029/2 |
| C235 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C236 | 330 pF | $\pm 10 \%$ | 125 V | ITB.6027/330/33/125 d.c. |
| C237 | $10-60 \mathrm{pF}$ |  | 250 V | ISB.6510/14 |
| C300 | $60 \mu \mathrm{~F}$ | +50\% - $20 \%$ | 350 V | IUB.7017/4 |
| C301 | $250 \mu \mathrm{~F}$ | +50\% - $20 \%$ | 350 | IUB. $717 / 4$ |
| C302 | $150 \mu \mathrm{~F}$ | $+50 \%-20 \%$ | 150 V | IUB.7017/3 |
| C303 | $200 \mu \mathrm{~F}$ | +50\%-20\% | 150 V | IUB.7017/2 |
| C304 C305 | $\begin{aligned} & 0.5 \mu \mathrm{~F} \\ & 0.5 \mu \mathrm{~F} \end{aligned}$ | $\pm 20 \%$ | 1 kV | ITB.6042/2 |
| C306 | $0.047 \mu \mathrm{~F}$ | $\pm 20 \%$ | 250 V | ITB.6047/4 |
| C307 | 100 pF | $\pm 20 \%$ | 3500 V | IUB.6005/4 |
| C309 | 22 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB.6027/22/2/350 d.c. |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| C310 | $0.03 \mu \mathrm{~F}$ | +80\% - $20 \%$ | 1500 V | ISB. 6048 |
| C312 | $0.03 \mu \mathrm{~F}$ | +80\% - $20 \%$ | 1500 V | ISB. 6048 |
| C313 | $0.03 \mu \mathrm{~F}$ | +80\%-20\% | 1500 V | ISB. 6048 |
| C314 | 5000 pF | +80\% - $20 \%$ | 3 kV | IUB.6005/6 |
| C315 | 5000 pF | +80\% - $20 \%$ | 3 kV | IUB.6005/6 |
| C316 | 5000 pF | +80\% - $20 \%$ | 3 kV | IUB.6005/6 |
| C317 | 5000 pF | + $80 \%-20 \%$ | 3 kV | IUB.6005/6 |
| C318 | 5000 pF | + $80 \%-20 \%$ | 3 kV | IUB.6005/6 |
| C319 | 5000 pF | + $80 \%-20 \%$ | 3 kV | IUB.6005/6 |
| C320 | 5000 pF | +80\%-20\% | 3 kV | IUB.6005/6 |
| C321 | 5000 pF | +80\% - $20 \%$ | 3 kV | IUB.6005/6 |
| C322 | 5000 pF | + $80 \%-20 \%$ | 3 kV | IUB.6005/6 |
| C323 | 5000 pF | + 80\% - $20 \%$ | 3 kV | IUB.6005/6 |
| C324 | 1000 pF | $+80 \%-20 \%$ | 500 V | ITB.6044/5 |
| C325 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C326 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C327 | 1000 pF | + $80 \%-20 \%$ | 500 V | ITB.6044/5 |
| C328 | 10 pF | $\pm 20 \%$ | 6 kV | IUB.6005/7 |
| C329 | 47 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB.6027/47/2/350 d.c. |
| C401 | $1 \mu \mathrm{~F}$ | +100\%-20\% | 350 V | IUB.7017/5 |
| C402 | $3 \cdot 3 \mathrm{pF}$ | $\pm 0.5 \mathrm{pF}$ | 750 V | ITB.6029/16 |
| C403 | 3.3 pF | $\pm 0.5 \mathrm{pF}$ | 750 V | ITB.6029/16 |
| C404 | 1000 pF | +80\% - $20 \%$ | 500 V | ITB.6044/5 |
| C405 | 3300 pF | $\pm 10 \%$ | 350 V | ITB. $6027 / 3300 / 330 / 350$ d.c. |
| C406 | $1 \mu \mathrm{~F}$ | +100\% - $20 \%$ | 350 V | IUB.7017/5 |
| C407 | 120 pF | $\pm 2 \%$ | 350 V | ITB.6027/120/2.4/350 d.c. |
| C408 | 600 pF | $\pm 2 \%$ | 350 V | ITB.6027/600/12/350 d.c. |
| C409 | 3300 pF | $\pm 10 \%$ | 350 V | ITB.6027/3300/330/350 d.c. |
| C410 | $0.01 \mu \mathrm{~F}$ | $\pm 20 \%$ | 500 V | ITB.6047/3 |
| C411 | 33 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB. $6027 / 33 / 2 / 350$ d.c. |
| C413 | 33 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB. $6027 / 33 / 2 / 350$ d.c. |
| C414 | 39 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB.6027/39/2/350 d.c. |
| C416 | $8 \mu \mathrm{~F}$ | +50\%-20\% | 275 V | ITB.7001/24S |
| C418 | 100 pF | $\pm 5 \%$ | 125 V | ITB.6027/100/5/125 d.c. |
| C419 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C420 | 82 pF | $\pm 20 \%$ | 125 V | ITB.6027/82/16.4/125 d.c. |
| C421 | 15 pF | $\pm 1 \mathrm{pF}$ | 350 V | ITB. $6027 / 15 / 1 / 350$ d.c. |
| C422 | 40 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB. $6027 / 40 / 2 / 350$ d.c. |
| C423 | 400 pF | $\pm 2 \%$ | 350 V | ITB. $6027 / 400 / 8 / 350$ d.c. |
| C424 | 200 pF | $\pm 2 \%$ | 350 V | ITB.6027/200/4/350 d.c. |
| C425 | 4000 pF | $\pm 2 \%$ | 350 V | ITB.6027/4000/80/350 d.c. |
| C426 | 2000 pF | $\pm 2 \%$ | 350 V | ITB.6027/2000/40/350 d.c. |
| C427 | $0.04 \mu \mathrm{~F}$ | $\pm 2 \%$ | 500 V | ITB.6027/40000/800/500 d.c. |
| C428 | $0.02 \mu \mathrm{~F}$ | $\pm 2 \%$ | 500 V | ITB.6027/20000/400/500 d.c. |


| Ref. | Value | Tolerance | Rating | Part Number |
| :---: | :---: | :---: | :---: | :---: |
| C429 | $0.4 \mu \mathrm{~F}$ | $\pm 2 \%$ | 500 V | ITB.6043/3 |
| C430 | $0 \cdot 2 \mu \mathrm{~F}$ | $\pm 2 \%$ | 500 V | ITB.6043/2 |
| C431 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C432 | 18 pF | $\pm 1 \mathrm{pF}$ | 350 V | ITB.6027/18/1/350 d.c. |
| C433 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB. $6047 / 2$ |
| C434 | 1000 pF | +80\% - $20 \%$ | 500 V | ITB.6044/5 |
| C435 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C436 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C437 | $0.01 \mu \mathrm{~F}$ | $\pm 20 \%$ | 500 V | ITB.6047/3 |
| C438 | $0.01 \mu \mathrm{~F}$ | $\pm 20 \%$ | 500 V | ITB.6047/3 |
| C439 | 4700 pF | +80\% - $20 \%$ | 500 V | ITB.6045/8 |
| C440 | 1000 pF | +80\% -20\% | 500 V | ITB.6044/5 |
| C441 | 100 pF | $\pm 5 \%$ | 125 V | ITB.6027/100/5/125 d.c. |
| C442 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C443 | 33 pF | $\pm 2 \mathrm{pF}$ | 350 V | ITB.6027/33/2/350 d.c. |
| C444 | $0 \cdot 1 \mu \mathrm{~F}$ | $\pm 10 \%$ | 500 V | ITB.6047/2 |
| C445 | $8 \mu \mathrm{~F}$ | + $50 \%-20 \%$ | 275 V | ITB.7001/24S |
| C446 | $1-6 \mathrm{pF}$ |  | 500 V | ISB. 6506 |
| C447 | $1 \mu \mathrm{~F}$ | + $100 \%-20 \%$ | 350 V | IUB.7017/5 |
| RV100 | $500 \Omega$ | $\pm 20 \%$ | 0.1 W | IUB.8021/50120/15F |
| RV101 | $250 \mathrm{k} \Omega$ | $\pm 20 \%$ | $0 \cdot 5 \mathrm{~W}$ | IUB.8026/5 |
| RV200 | $500 \Omega$ | $\pm 20 \%$ | 0.1 W | IUB.8021/50120/15F |
| RV201 | $250 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.5 W | IUB.8026/5 |
| RV300 | $500 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.25 W | ITB.8038/2 |
| RV301 | $250 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.25 W | ITB.8025/174/25420 |
| RV302 | $1 \mathrm{M} \Omega$ | $\pm 20 \%$ | 0.25 W | ITB. 8038 |
| RV303 | $1 \mathrm{M} \Omega$ | $\pm 20 \%$ | 0.25 W | ITB. 8038 |
| RV304 | $30 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.5 W | ISB.8000/30320 |
| RV305 | $50 \Omega$ | $\pm 10 \%$ | 2 W | IUB.8002/50010/11 |
| RV306 | $500 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.25 W | ITB.8038/2 |
| RV307 | $250 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.25 W | ITB.8025/174/25420 |
| RV401 | $220 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.5 W | ITB.8043/2 (with RV404) |
| RV402 | $1 \mathrm{M} \Omega$ | $\pm 20 \%$ | 0.5 W | IUB.8026/4 |
| RV403 | $100 \mathrm{k} \Omega$ | $\pm 20 \%$ | $0 \cdot 25 \mathrm{~W}$ | ITB.8025/174/10420 |
| RV404 | $500 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.5 W | ITB.8043/2 (with RV401) |
| RV405 | $250 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.5 W | ITB.8043/3 (with RV408) |
| RV406 | $2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.8025/196/20210 |
| RV407 | $27 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.25 W | ITB.8025/174/27310 |
| RV408 | $10 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.5 W | ITB.8043/3 (with RV405) |
| RV409 | $200 \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.8025/196/20110 |
| RV410 | $2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.8025/196/20210 |
| RV411 | $2 \mathrm{k} \Omega$ | $\pm 10 \%$ | 0.5 W | ITB.8025/196/20210 |
| RV412 | $250 \mathrm{k} \Omega$ | $\pm 20 \%$ | 0.25 W | ITB.8025/174/25420 |


| Valve | Type | Valve | Type | Valve | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
| V100 | CC3L | V102 | ECC88 | V104 | EF184 |
| V101 | ECF80 | V103 | EF184 | V104 | ECC81 |
| V200 | CC3L | V203 | EF184 | V206 | CC3L |
| V201 | ECF80 | V204 | EF184 | V207 | CC3L |
| V202 | ECC88 | V205 | CC3L |  |  |
| V300 | ECF80 | V304 | ECC88 | V308 | CC3L |
| V301 | CC3L | V305 | CC3L | V309 | CC3L |
| V302 | CC3L | V306 | CC3L |  |  |
| V303 | CC3L | V307 | CC3L |  |  |
| V401 | ECC88 | V405 | ECC88 | V409 | CC3L |
| V402 | ECC88 | V406 | ECC88 | V410 | CC3L |
| V403 | ECC88 | V407 | ECC88 | V411 | CC3L |
| V404 | ECC88 | V408 | ECC88 |  |  |
| Ref. | Descrip |  |  |  | Part Number |
| L101 | Inductor |  |  |  | KA.88112/4 |
| L. 102 | Inductor |  |  |  | KA.88112/4 |
| L. 103 | Inductor |  |  |  | KA.88112/4 |
| L. 104 | Inductor |  |  |  | KA.88112/4 |
| L201 | Inductor |  |  |  | KA.88112/4 |
| L202 | Inductor |  |  |  | KA.88112/4 |
| L. 203 | Inductor |  |  |  | $\text { KA. } 88112 / 4$ |
| L. 204 | Inductor |  |  |  | KA.88112/4 |
| L300 | Inductor |  |  |  | $\text { ITB. } 3017$ |
| L301 | Inductor | nominal |  |  | ISA.262/63 |
| L401 | Inductor |  |  |  | KA.88089/10 |
| T300 | Transfor |  |  |  | IUB. 3016 |
| LP300 | Lamp, I | $\text { g, } 0.36 \mathrm{~W}$ |  |  | $\text { ISB. } 5021$ |
| LP301 | Lamp, I | g, 0.36 W |  |  | ISB. 5021 |
| F300 | Fuse, 2 |  |  |  | ISB.5002/2 |
| CRT | Cathode | be (G.E.C |  |  | 1024F |


| Ref. | Description | Part Number |
| :---: | :---: | :---: |
| MR300 | Rectifier, Diode | ISB.9013/6 |
| MR301 | Rectifier, Diode | ISB.9013/6 |
| MR302 | Rectifier, Diode | ISB.9013/6 |
| MR303 | Rectifier, Diode | ISB.9013/6 |
|  | Rectifiers, contact cooled (manufactured as a single block) | ISB. 9006 |
|  |  |  |
|  |  |  |
|  |  |  |
| MR308 | Rectifier, Tubular | ISB.9004/2 |
| MR309 | Rectifier, Tubular | ISB.9004/2 |
| MR310 | Rectifier, E.H.T. | ITB. 9015 |
| MR311 | Rectifier, E.H.T. | ITB. 9015 |
| MR312 | Rectifier, E.H.T. | ITB. 9015 |
| MR313MR314 | Rectifier, Germanium Diode | ISB. 9009 |
|  | Rectifier, Miniature H.F. Rectifiers, Germanium Diode | ISB. 9012 |
| MR401 | Rectifiers, Germanium Diode | ISB. 9009 |
| MR402 |  | ISB. 9009 |
| MR403 |  | ISB. 9009 |
| MR404 |  | ISB. 9009 |
| MR406 |  | ISB. 9009 |
| MR408 |  | ISB. 9009 |
| MR409 |  | ISB. 9009 |
| S100 | Switch, Rotary, AC-DC-CAL | ITB.262/25 |
| S101 | Switch, Rotary, ATTENUATOR | ITB.262/22 |
| S200 | Switch, Rotary, AC-DC-CAL | ITB.262/25 |
| S201 | Switch, Rotary, ATTENUATOR | ITB.262/22 |
| S300 | Switch, Rotary, INTENSITY MOD. | ISB. 4014 |
| S301 | Switch, Toggle, MAINS ON/OFF | ISB.4013/6 |
| S400 | Switch, Rotary, TRIG. SYSTEM \& TRIG. SELECTOR | ITB.262/20 |
| S401 | Swith, Rotary, TRIG. SYSTEM \& TRIG. SELECTOR | 1-8.262/20 |
| S402 | Switch, Rotary, TIME/CM \& MULTIPLIER | ITB.262/21 |
| S405 | Switch, Rotary, DELAY RANGE | ITB.262/24 |
| SKT100 | Terminal (Maroon) | ISB.5504/3 |
| SKT101 | Socket, Coaxial (Amphenol) | ISB. 2516 |
| SKT102 | Terminal, (Black) | ISB. 5504 |
| SKT200 | Terminal, (Maroon) | ISB.5504/3 |
| SKT201 | Socket, Coaxail (Amphenol) | ISB. 2516 |
| SKT202 | Terminal, (Maroon) | ISB. 5504 |
| SKT300 | Terminal, (Black) | ISB. 5504 |
| SKT401 | Terminal, (Maroon) | ISB.5504/3 |
| SKT403 | Terminal, (Maroon) | ISB.5504/3 |

## MECHANICAL ITEMS

## FOR MODELS 2000 AND 2100

Description
Part Number
Knob (pointer type) small black ..... IVB. 7555
Knob (pointer type) rear of dual-black ..... IVB. 7536
Knob (pointer type) front of dual-maroon ..... IVB.7535/2
Terminal Screening Cover ..... ISA. 278
Graticule ..... IT.236/2
Green Filter ..... ITB. 9506
Handle ..... ITB. 9258
End-piece, Handle ..... ITB.9258/4
Rubber Foot ..... ISB. 8502
Plug, Mains Selector Panel ..... ISB. 2514
Lampholder, Securing Piece ..... ISB. 8530

NOTES

## SPARES AND SERVICE

To assure the prompt dispatch of spare parts, it is essential that the order includes the Model number and serial number of the instrument, the description of the parts), the part numbers) and the quantity required.

Whilst every effort is made by the Cossor Instrument Service Department to maintain an adequate supply of spares, a delay in dispatch of some parts, which are not normally expected to require replacement, may be unavoidable.

Where purchase of the instrument has been made direct from Cossor Instruments Limited, orders and all requests for technical information should be made to :

Cossor Instruments Limited,<br>Cossor House,<br>\section*{Highbury Grove,}<br>London, N. 5

and ENGLAND should be added to this address if the purchaser is writing from a place outside the United Kingdom.

## COSSOR INSTRUMENTS LIMITED

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Telephone: CANonbury $\mathbf{r} 234$ ( 15 lines)
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Cables: Cossor, London, N. 5
Code: "Bentley's Second"




TIME-BASE (MODEL 2000)

## CIRCUIT DIAGRAM




Y1 AMPLIFIER
(MODEL 2100)

CIRCUIT DIAGRAM







## price 20/- Net

