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# FM/AM SIGNAL GENERATOR

## **TF 995A/5**

FF 5094=1

**OPERATING** AND MAINTENANCE HANDBOOK

> **MARCONI INSTRUMENTS LIMITED** ST. ALBANS HERTFORDSHIRE ENGLAND



## F.M./A.M. Signal Generator

OPERATING AND MAINTENANCE HANDBOOK No. OM 995A/5

**TYPE TF 995A/5** 

(Serial Nos. JA311/001 and above)

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#### Data Summary Frequency 1.5 to 220 Mc/s in five bands as follows: RANGE: Band 1 ... 1.5 to 13.5 Mc/s ... 13.5 to 27.5 Mc/s 2 ... 3 ... 27 to 55 Mc/s ... ... 54 to 110 Mc/s 4 ... ... 108 to 220 Mc/s 5 ... CALIBRATION From 1.5 to 13.5 Mc/s, the main frequency dial calibration has an average ACCURACY: accuracy of $\pm 3^{\circ}$ . From 13.5 to 220 Mc/s, the calibration of this dial is accurate to within $\pm 1^{\circ}_{0}$ . In addition, the built-in crystal calibrator provides 14 check points to an accuracy of 2 parts in 10<sup>4</sup> on each of the four higher-frequency bands. After warm-up, drift is not greater than 0.002° o in a 10-minute period, except on STABILITY . lowest band. FINE TUNING The fine tuning control provided is arbitrarily calibrated -20 to -20. It has a CONTROL: total cover of approximately 6 kc/s on bands 1 and 3, 3 kc/s on band 2, 12 kc/s on band 4, and 24 kc/s on band 5. **INCREMENTAL** Two controls are provided, one stepped, the other continuously variable. The CONTROL: stepped control enables the carrier frequency to be shifted by $\pm$ 20 and $\pm$ 10 kc/s on bands 1 and 3, $\pm$ 10 and $\pm$ 5 kc/s on band 2, and $\pm$ 40 and $\pm$ 20 kc/s on bands 4 and 5. The continuous control has a cover of $\pm 0.75$ of one increment of the stepped control on any band, e.g. cover is $\pm 15$ kc/s on bands 4 and 5. Output Built-in coarse and fine 75-ohm attenuators connected in cascade provide-in **VOLTAGE:** conjunction with the 6-dB Terminating Unit-a source e.m.f. variable in 2-dB steps from $1 \mu V$ to 100 mV. Interpolation between the 2-dB steps is by means of a $\pm$ 1-dB calibration on the r.f. level meter. Source e.m.f.'s up to 200 mV at an impedance of 75 ohms are obtained direct HIGH OUTPUTS: from the Generator output cable. LOW OUTPUTS: Source e.m.f.'s down to a nominal $0.1 \,\mu\text{V}$ at impedances of 75 and 52 ohms are obtained by inserting the 20-dB Attenuator Pad TM 5552 between the Generator output cable and the Terminating Unit. The accuracy of the joint indication of the attenuators and level meter is within ACCURACY: $-1 \text{ dB} + 0.25 \,\mu\text{V}$ up to 100 Mc/s, and within $-2 \text{ dB} + 0.25 \,\mu\text{V}$ up to 220 Mc/s.

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Modulation					
FREQUENCY MODULATION:	Normal deviatio from 0 to 15 kc/ is $\pm 5^{\circ}{}_{0}$ of f.s.c ageing or random	n is continuously v s on all bands; the l., with a possible a n replacement.	ariable in two ran accuracy at maxi additional variatic	nges: from 0 to 5 kc/s and mum deviation at 1000 c/s on of $\pm 10^{\circ}$ due to valve	
	High deviation is $\times$ 2 normal on b Internal modulation with modulation external modulation with respect to 1	s also available:— ands 1 and 3, $\times$ 4 n tion is available at 1 distortion not ex tion characteristic kc/s.	ormal on band 4, a frequencies of 400 acceeding $2^{\circ}$ at r is flat, within 1 c	and $\times 8$ normal on band 5. 0 c/s, 1000 c/s and 1500 c/s naximum deviation. The 1B, from 50 c/s to 15 kc/s	
SPURIOUS F.M. ON C.W.:	The spurious f.n frequency. The of the Generator employing chanr	n. due to hum doe unusually low level r for adjacent-chan nel separations as sr	s not exceed 25 c/ of spurious noise nel testing on rece nall as 22.5 kc/s.	's deviation at any carrier modulation allows full use vivers designed for systems	
AMPLITUDE MODULATION:	Available internally at 400 c/s, 1000 c/s and 1500 c/s to a depth variable up to $50^{\circ}_{0}$ with distortion not exceeding $6^{\circ}_{0}$ at $30^{\circ}_{0}$ depth. External frequency characteristic (with input adjusted for constant modulation-meter reading) is flat within 0.5 dB from 100 c/s to 10 kc/s.				
A.M. DEPTH INDICATION :	Indication accurate to within $5^{\circ}_{,\circ}$ modulation.				
SYNCHRONIZING SIGNAL :	Available from front-panel terminals at 400 c/s, 1 kc/s or 1.5 kc/s.				
Power Supply:	200 to 250 volts. 65 watts. Model at the time of or	or 100 to 150 volutions of the supplied ready for dering.	ts after adjusting r immediate 100-	internal link, 40 to 65 c/s; to 150-volt use if specified	
Dimensions and Weight:	<i>Height</i> 13 in (33 cm)	<i>Width</i> 17½ in (44·5 cm)	<i>Depth</i> 8 <sup>1</sup> / <sub>2</sub> in (22 cm)	Weight 33 lb (15 kg)	

## Schedule of Parts Supplied

The complete equipment comprises the following items:----

1.	One F.M./A.M. Signal Generator Type TF 995A/5 complete with valves, etc., as under:				
	Valves:	One: One: Six: One: One: One: Two: One:	OA2 (150C4), Voltage Stabilizer Tube. 5Z4G (52KU), Full-Wave Rectifier. 6AK5 (EF95), Pentodes. EF86 (6267), Pentode. 6AK6, Pentode. 6AL5 (D77), Double Diode. 6AU6 (EF94), Pentode. 12AT7 (ECC81), Double Triodes. 5651 (OS83/3) Voltage Reference Tube.		
	Lamp:	One:	6·3-volt, 0·3-amp, M.E.S., Pilot Lamp.		
	Oscillator Crystal:	One:	333.3 kc/s, Marconi Type 1655C.		
	Semiconductors:	One: Two:	Type CS2-A Silicon Diode. Type CG1-E Germanium Diodes.		
	Fuses:	Two:	2-amp, Belling-Lee Type O cartridge fuses for 200- to 250-volt operation. (For 100- to 150-volt operation, the 2-amp fuses are replaced by a similar type having a rating of 3 amps.)		
		One:	150-mA Beswick Type TDC11 Surge-Resisting cartridge fuse.		
2.	One Terminating Unit Type TM 5551; 75 ohms in, 52 and 75 ohms out.				
3.	Two Coaxial Free Plugs, Type BNC; one 50-ohm, one 75-ohm; for Terminating Unit outlets.				

- 4. One Telephone Plug, S.T.C. Type 4006; for Crystal Check jack.
- 5. One Operating and Maintenance Handbook No. OM 995A/5.

The following accessory is an optional item supplied only if specially ordered:-

20-dB Attenuator Pad Type TM 5552; for use between output cable and Terminating Unit.

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The Marconi F.M./A.M. Signal Generator TF 995A/5 covers the frequency range of 1.5 to 220 Mc/s in five bands. Its output can be unmodulated, frequency modulated, or amplitude modulated; if required, both frequency and amplitude modulation can be applied simultaneously. The modulation frequency is obtained from either an internal 3-frequency oscillator, or an external source.

The open-circuit output voltage is variable by means of resistive step attenuators from 1  $\mu$ V to 100 mV at 52 ohms and 1  $\mu$ V to 200 mV at 75 ohms. A plug-in 20-dB Attenuator Pad, available as an optional accessory, extends the range down to a nominal 0.1  $\mu$ V at both impedances.

The high-discrimination tuning required for testing narrow-band systems is facilitated by the inclusion of a fine tuning control. In addition, small known changes in carrier frequency can be made by means of two incremental-frequency controls; one of these controls gives a stepped adjustment while the other allows continuous interpolation between steps. On the two highest bands, the stepped control provides shifts of 20 and 40 kc/s in either direction and the calibration marks on the continuous control are only 1 kc/s apart; on the lower bands, the total shift is determined by a simple division of the reading on both dials.

A high degree of frequency stability has been achieved by use of temperature-compensating components; after warm-up, drift is less than 400 c/s per minute at a carrier frequency of 200 Mc/s.

The inclusion of a Carrier on/off switch makes it possible for the Generator output to be temporarily interrupted without affecting the output impedance; this facilitates a number of two-signal receiver tests such as intermodulation and blocking which involves the simultaneous use of two signal generators. Spurious f.m. due to hum is less than 25 c/s deviation, and the low level of noise modulation makes the TF 995A/5 fully suitable for applications such as adjacent-channel testing on receiver systems using a channel separation of 25 kc/s or less.

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- I. Pilot Lamp and Mains Supply Switch
- 2. External Modulation Input for f.m. or a.m. and Sync Output from internal modulation oscillator
- 3. Normal: deviation is as shown on meter High: multiply meter reading by factor on Range switch
- 4. Coarse Tuning Control
- 5. Incremental Frequency Controls Carrier shift is given by dial readings multiplied by factor on Range switch
- 6. Fine Tuning Control
- 7. Range Selector
- 8. Main Tuning Dial Knurled boss adjusts cursor to standardize scale against
- crystal check points 9. Set Carrier Control For adjusting unmodulated carrier to Set R.F. mark on meter

- 10. Meter indicates carrier level, f.m. deviation, or a.m. depth depending on setting of Meter Reads switch
- II. Crystal Check Jack oscillator
- 12. Case Handle Recess stowage for mains supply plug
- 13. Modulation Frequency Selector Choice of 3 frequencies from internal oscillator
- 14. Set Mod Control Adjusts f.m. deviation or a.m. depth
- 15. Interrupts Output without switching off filaments
- 16. Output Attenuators
  - Unit when carrier is adjusted to Set R.F. mark on meter
- 17. Modulation Selector
- 18. Meter Function Selector
- 19. Deviation Range Selector Read deviation from corresponding scale on meter

Fig. 2.1 Controls.

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### Operation

#### 2.1 INSTALLATION

Unless otherwise specified, the Signal Generator is dispatched with its valves in position and with its mains input circuit adjusted for immediate use with a 240-volt, 40- to 65-c/s mains supply. The instrument can be adjusted for operation from any other 40- to 65-c/s supply voltage in the ranges 200 to 250 and 100 to 150 volts. To check or alter the settings of the mains transformer tappings, refer to MAINTENANCE, Section 5.3.

#### 2.2 SWITCHING ON AND WARMING UP

Before switching on, be quite sure that the instrument is correctly adjusted to suit the particular mains supply to which it is to be connected. Then proceed as follows:—

- Connect the mains lead—stowed in the lefthand case-handle recess—to the mains supply socket.
- (2) Switch ON by means of the SUPPLY switch; the red pilot lamp should now glow.
- (3) Before proceeding further, allow a short time —say five minutes—to elapse for the internal circuits to warm up. If a particularly high standard of frequency stability is required, this time should be increased to about 60 minutes.

#### 2.3 OUTPUT CONNECTIONS

The r.f. output from the Signal Generator is derived, at a source impedance of 75 ohms, via a permanently attached coaxial lead fitted with a BNC free socket; the lead is stowed in the righthand case-handle recess.

The TERMINATING UNIT, which will normally be plugged on to the output lead, has two outlets, one of 75 ohms impedance and the other of 52 ohms. Two free plugs are supplied for making connection to the TERMINATING UNIT outlets.

The 20-dB ATTENUATOR PAD, available as an optional accessory, can be inserted between the Generator output socket and the TERMINATING UNIT input plug when low outputs are required.

Details on the use of the TERMINATING UNIT and ATTENUATOR PAD are given in Section 2.6, R.F. OUTPUT ARRANGEMENTS.

Equivalents to the free plugs supplied, and illustrated in Fig. 2.3, are as follows:—

	75 ohm	50 ohm
Great Britain,		
Air Ministry:	10H/20946	10H/20935
Films and Equipment:	UG-260/U	UG-88/U
Transradio Ltd.:	BN. 1/7	BN. 1/5
Belling and Lee:		L. 1331/FP
United States,		
Military No.:	UG-260/U	UG-88/U

#### 2.4 TUNING

The various aspects of tuning the Generator are dealt with in the following sections.

General tuning: Section 2.4.1.

- Standardizing frequency against crystal oscillator: Section 2.4.2.
- Use of incremental frequency controls: Section 2.4.3.

Interpolation of main frequency scales: Section 2.4.4.

#### 2.4.1 GENERAL TUNING

The TF 995A/5 covers the range 1.5 to 220 Mc/s in five bands as follows:—

Band 1	 	1.5 to 13.5 Mc/s
2	 	13.5 to 27.5 Mc/s
3	 	27 to 55 Mc/s
4	 	54 to 110 Mc/s
5	 	108 to 220 Mc/s



Fig. 2.2 Details of Tuning Arrangements.

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The particular band required is selected by means of the RANGE switch. Rotation of the COARSE TUNE control varies the output frequency within the limits of the band selected, and moves the main dial relative to its cursor.

The FINE TUNE control has a very small coverage and is incorporated to assist in the precise tuning required in tests involving narrow-band equipment. The total coverage of this control on each band is as follows:—

Band 1	 	6 kc/s
2	 	3 kc/s
3	 	6  kc/s
4	 	12 kc/s
5	 	24 kc/s
		,

The Signal Generator has a built-in crystal calibrator, and the cursor of the main tuning dial is mounted so that its angular position relative to that of the dial is variable over a small arc by movement of a milled boss at the centre of the dial. This movable cursor enables the operator to standardize the frequency scale of the Signal Generator at any time; the cursor is used in conjunction with the crystal calibrator in the manner described in Section 2.4.2.

In addition to the RANGE switch and the TUNE controls, the instrument is fitted with calibrated incremental-frequency controls; the method of using these controls is described fully in Section 2.4.3. Section 2.4.4 deals with the method of interpolating between main dial markings by means of the linearly calibrated dial on the COARSE TUNE control.

#### 2.4.2 USE OF THE CRYSTAL CALIBRATOR (a) Description

Accurate calibration of the main tuning dial may be effected with the built-in crystal oscillator. This oscillator has a fundamental frequency of  $333\cdot3$  kc/s with an accuracy of 2 parts in  $10^4$  and is coupled to the basic 4.5- to 9.16-Mc/s r.f. oscillator which drives the multiplier chain. The calibrator circuit is automatically brought into use when a pair of high-resistance headphones are plugged into the CRYSTAL CHECK jack socket; with the aid of the headphones, the difference frequency between the basic oscillator and the harmonic multiples of the calibrator's  $333 \cdot 3 \text{ kc/s}$  can be monitored aurally.

Because the outputs on the four higher-frequency bands are all derived directly from the multiplier chain, their frequencies have an exact integral relationship to the frequency of the basic oscillator. It follows, therefore, that setting the COARSE TUNE control to bring the basic-oscillator frequency to that of a crystal harmonic will also bring the frequency of the outputs from the multiplier chain to a known relationship with the crystal harmonic, and allow the frequency dial to be standardized with a high degree of accuracy.

Outputs on the lowest-frequency band are not derived directly from the multiplier chain; their generation involves a heterodyne action between the 27- to 55-Mc/s multiplier and a 30-Mc/s fixed oscillator which is not locked to the basic oscillator. For this reason, although use is made of the crystal calibrator when setting up for 1.5- to 13.5-Mc/s outputs, the accuracy of standardization is of a lower order than that obtained on the four higherfrequency bands.

#### (b) Check-Point Frequencies

The calibrator provides a total of 56 check points between 13.5 and 220 Mc/s; these occur as follows:—

- Band 2, 13.5 to 27.5 Mc/s: at all multiples of 1 Mc/s from 14 to 27 Mc/s inclusive.
- Band 3, 27 to 55 Mc/s: at all multiples of 2 Mc/s from 28 to 54 Mc/s inclusive.
- Band 4, 54 to 110 Mc/s: at all multiples of 4 Mc/s from 56 to 108 Mc/s inclusive.
- Band 5, 108 to 220 Mc/s: at all multiples of 8 Mc/s from 112 to 216 Mc/s inclusive.

#### (c) Standardization Procedure

As shown above, the calibrator allows the frequency scale to be checked at 14 different points on each of the above bands, and the adjustable cursor can be set to correspond exactly with any one of these points.

When the Signal Generator is to be used above 13.5 Mc/s to provide an output at a single spot frequency, or over a narrow band of frequencies, the cursor should be set up at the nearest crystal check point.

When the Signal Generator is to be used over a wide range of frequencies, and it is inconvenient to

reset the cursor for each material frequency change, or, alternatively, when using the 1.5- to 13.5-Mc/s band, the procedure is varied to reduce the mean error to a minimum. The method of standardizing the frequency scale for subsequent general use is as follows:—

- (1) Set the INC. FREQ. controls to zero and the FINE TUNE control to mid-position.
- (2) Set the RANGE switch to 13.5-27 Mc/s.
- (3) Using the headphones plugged into the CRYSTAL CHECK jack, tune the main dial to a crystal check point near the centre of the band; e.g. 20 Mc/s.

When using the calibrator, the MOD. SELECTOR must be set to a position other than INT. MOD.— F.M. or EXT. MOD.—F.M. This ensures that the variable oscillator is not being frequency modulated —a condition which prevents precise setting of the COARSE TUNE control for the lowest-frequency beat note in the headphones, since it gives rise to a fluctuating tone.

After using the calibrator, the Signal Generator can, of course, be set up for f.m. without invalidating this frequency standardization.

(4) Adjust the milled boss in the centre of the dial to bring the cursor exactly in line with the calibration mark corresponding to the crystal check point.

If the Signal Generator has been out of use for some time, it may be necessary to use a coin in the slot provided in order to rotate the milled boss.

- (5) Check the calibration accuracy at several crystal check points both above and below the check point at which the cursor was set in (4) above.
- (6) Readjust the cursor setting to equalize the errors over the band; e.g. it might be found that, with the frequency scale indication correct at 20 Mc/s, the indication was high at both 15 and 25 Mc/s—in such a case, the errors would be equalized by making the indication a little low at 20 Mc/s, and thus not so high at 15 and 25 Mc/s.

It will be noted that, in the above procedure, the frequency scale is standardized on the 13.5- to 27-Mc/s band. This band is specified since its corresponding scale calibrations occupy the longest arc on the dial. The dial can therefore be read with a high degree of discrimination on this band and the correct cursor setting most easily determined. Once the frequency scale has been standardized on the 13.5- to 27-Mc/s band, the cursor is correctly set to give the minimum mean error on the other three direct-multiple bands. It is also correctly set for the 1.5- to 13.5-Mc/s band.

When standardized in this way, the main tuning dial indication for frequencies above 13.5 Mc/s is accurate to at least  $1^{\circ}_{0}$ , and will generally be within  $\pm 0.5^{\circ}_{0}$ ; for frequencies below 13.5 Mc/s, the average error does not exceed  $\pm 3^{\circ}_{0}$ .

#### 2.4.3 INCREMENTAL FREQUENCY CONTROLS

These controls are well suited to performing bandwidth or similar measurements since they are a convenient means of producing small, accuratelyknown changes in carrier frequency. They are not connected directly to the r.f. oscillator either mechanically or electrically, but operate by varying the d.c. potential at the grid of the reactor valve so that they are completely free from backlash of any kind.

To utilize these controls, proceed as follows:-

- (1) With the INC. FREQ. controls set to their centrezero position, tune the Signal Generator to the required centre-frequency by means of the RANGE switch and the TUNE controls.
- (2) Rotate the INC. FREQ. controls to produce the required shift or the required change in response depending on the method of measurement.

The scales of the INC. FREQ. dials are directreading on bands 4 and 5. For each of the other bands, a multiplying factor must be applied, the appropriate factor for each frequency band is engraved on the front panel adjacent to the RANGE switch marking. The multiplying factors are also given below in Table 1.

#### 2.4.4 THE INTERPOLATING DIAL

The COARSE TUNE dial is calibrated linearly from 0 to 100 and makes approximately 17 revolutions as the main dial is tuned through a complete band.

This dial may be used to subdivide linearly any part of the frequency scale in order to tune accurately to a frequency which lies between two crystal check points. To do this, proceed as follows:—

- (1) Set the INC. FREQ. controls to zero.
- (2) Set the RANGE switch to whichever of the four higher-frequency bands includes the required frequency.
- (3) Tune the Signal Generator to the nearest crystal check point *below* the required frequency—as indicated on the main tuning dial—identifying the point with the aid of headphones plugged into the CRYSTAL CHECK jack, and noting the interpolating dial reading for the lowest-frequency beat note.
- (4) Tune the Signal Generator to the nearest crystal check point *above* the required frequency and note the change of reading of the interpolating dial. It is important that the *total* change is noted when the dial is turned through more than one revolution.

The relationship should be determined between the crystal check points which embrace the particular section of the frequency band over which incremental variations are to be made. Also, the relationship should be redetermined for each different section of the frequency band, since it varies, not only from band to band, but also for different sections of any one band.

- (5) From the difference in frequency between the two crystal check points, and the total number of interpolating dial divisions traversed, calculate the frequency change per interpolating dial division; this change may be conveniently expressed in kc/s per division.
- (6) With the aid of the headphones, reset the main tuning dial to the crystal check point below the required frequency.

RANGE switch setting	Total coverage of INC, FREQ.	Multiply INC. FREQ.	Incremental Frequency change per division (kc s per div)		
(Mc/s)	(Mc/s) controls (kc/s) dial readings		CO.4RSE	FINE	
1.5-13.5 (Band 1)	- 27.5	0.5	10	0.5	
13.5-27.5 (Band 2)	$\pm$ 13.75	0.25	5	0.25	
27-55 (Band 3)	<u>+</u> 27-5	0.5	10	0.5	
54-110 (Band 4)	- 55	1	20	1	
108–220 (Band 5)	<del>1</del> 55	1	20	1	

#### TABLE I

(7) Rotate the COARSE TUNE control so that the interpolating dial traverses the correct number of divisions to give the required frequency.

It is recommended that the required frequency should always be approached from the lowfrequency side in order to eliminate all possibility of error due to backlash.

The following example illustrates the use of the interpolating dial to obtain an output from the instrument at an accurate frequency of 74.25 Me/s.

*Example:* With the TUNE control set to the crystal check point at 72 Mc/s, the interpolating dial reading was 17. With the TUNE control set to the crystal check point of 76 Mc/s the new reading on the auxiliary dial was 40. The total number of interpolating dial divisions traversed was 123, the dial having rotated through slightly more than one revolution for the frequency change of 4 Mc/s, i.e. 4,000 kc/s. In this case, a change of 1 division on the interpolating dial corresponded, *between 72 and 76 Mc/s*, to a nominal frequency change of

$$\frac{4,000}{123} = 32.5 \text{ kc/s.}$$

Therefore, by starting from the original auxiliary dial setting at 72 Mc/s (72,000 kc/s) the required frequency of 74.25 Mc/s (74,250 kc/s) was obtained by rotating the auxiliary dial through

$$\frac{74,250}{32\cdot5} \frac{72,000}{32\cdot5} = \frac{2.250}{32\cdot5} = 69$$
 divisions.

Since it will be appreciated that only typical figures could be quoted above, it follows that the relationship between frequency change and change in interpolating dial setting should be determined —in the manner outlined above—for the particular TF 995A/5 in use.

#### 2.5 SETTING UP FOR C.W. OR MODULATED OUTPUT

The Signal Generator will give the following types of r.f. output:--

- (1) Continuous wave (see Section 2.5.1).
- (2) Amplitude modulated (see Section 2.5.2), variable to  $50^{\circ}_{0}$  depth.
  - (a) from the internal a.f. oscillator at 400, 1.000, or 1.500 c/s,
  - (b) from an external sinewave source, within the range 100 c/s to 10 kc/s.
- (3) Frequency modulated (see Section 2.5.3), variable to maximum frequency deviations ranging from 15 kc/s to 120 kc/s,
  - (a) from the internal a.f. oscillator at 400, 1,000. or 1.500 c/s,
  - (b) from an external sinewave source, within the range 50 c/s to 15 kc/s.
- (4) Simultaneous frequency and amplitude modulation (see Section 2.5.4); the amplitude modulation being obtained from the internal a.f. oscillator, and the frequency modulation from an external source as (3) (b), above.

When setting up for amplitude or frequency modulation as described in Sections 2.5.2 and 2.5.3, it may be observed that, with the METER READS key held to either A.M. or F.M. as applies, the apparent modulation as measured on external apparatus is



Fig. 2.4 C.W. Operation.

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less than that indicated on the meter. This is quite in order; the meter indicates the modulation which will be obtained when the switch is returned to its central position and the meter reverts to its normal function of monitoring the r.f. level.

#### 2.5.1 CONTINUOUS WAVE

- (1) Set the MOD. SELECTOR switch to C.W.
- (2) Adjust the SET CARRIER control to bring the meter pointer to the SET R.F. mark.

#### 2.5.2 AMPLITUDE MODULATION

#### (a) From the internal 3-frequency oscillator

- (1) Set the MOD. SELECTOR switch to INT. MOD.—A.M.
- (2) Turn the SET MOD. FREQ. switch to give the

required modulation frequency-400, 1,000, or 1,500 c/s.

- (3) Adjust the SET CARRIER control to bring the meter pointer to the SET R.F. mark.
- (4) With the METER READS key switch held in the A.M. position, adjust the SET MOD. control to the required modulation depth, as indicated on the top scale of the panel meter. Amplitude modulation is variable to a maximum depth of 50%.
- (5) Release the METER READS key switch and, if necessary, repeat (3) above.

#### (b) From an external a.f. source

(1) Set the MOD. SELECTOR switch to EXT. MOD.—A.M.



Fig. 2.5 (b) Internal A.M. Operation. (ii) Setting Modulation Depth.

Fig. 2.6 (a) 107 Internal F.M. Operation. (i) Setting Carrier Level. MODUL ATION SETRE SET CARRIER Adjust for INT MO SET R.F. reading AM C W FM METER READS MOD. SELECTOR

- (2) Adjust the SET CARRIER control to bring the meter pointer to the SET R.F. mark.
- (3) Connect the external modulation source to the EXT. MOD. and E terminals.
- (4) With the METER READS key switch held in the A.M. position, adjust the SET MOD. control to the required modulation depth, as indicated on the top scale of the panel meter. With the SET MOD. control at maximum, an input of approximately 15 volts r.m.s. is required at the EXT. MOD. and E terminals to produce 30% modulation depth within the modulation frequency range 100 c/s to 10 kc/s.
- (5) Release the METER READS key switch and, if necessary, repeat (2) above.

#### 2.5.3 FREQUENCY MODULATION

In addition to the MOD. SELECTOR switch, there are three other controls concerned in setting up the carrier deviation when the output from the Signal Generator is to be frequency modulated. These controls are the continuously-variable SET MOD. potentiometer, the DEVIATION RANGE switch, and the DEVIATION-NORMAL/HIGH switch. When the METER READS key switch is held to F.M., the panel meter indicates deviation. The meter has two deviation scales: one calibrated from 0 to 5 kc/s, and the other from 0 to 15 kc/s.

With the DEVIATION-NORMAL/HIGH switch set to NORMAL, the meter scale appropriate to the setting of the DEVIATION RANGE switch is used and the



(ii) Setting Deviation.

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RANGE	DEVIATION	DEVIATION—NORMAL HIGH switch set to HIGH		
switch setting (Mc s)	RANGE switch setting (kc/s)	Multiply meter reading by	Maximum deviation obtainable (kc s)	
1.5 13.5 (Bund 1)	1 5	. 2	10	
1 2 <sup>-1</sup> 2 <sup>-2</sup> (Dand 1)	115	2	30	
13.5-27.5 (Band 2)	15	1	5	
100~270 (Danie 2)	15	1	15	
27-55 (Band 3)	j 5	2	10	
27 00 (Dana 0)	115	2	30	
54-110 (Band 4)	[ 5	4	20	
of file (build f)	115	4	60	
108-220 (Band 5)	∫ 5	8	40	
roo 120 (Dinid 5)	115	8	120	

TABLE 2

deviation is as indicated by the meter for all settings of the carrier-frequency RANGE switch.

With the DEVIATION--- NORMAL HIGH switch set to HIGH, the deviation obtained on the 13-5- to 27-Mc/s band is the same as with the switch set to NORMAL. For all other carrier-frequency bands the deviation is increased and the meter readings---again taken on the scale appropriate to the settings of the DEVIATION RANGE switch--must be multiplied in accordance with Table 2 above.

The following example shows the method of determining the meter reading for a required deviation greater than 15 ke s and thus necessitates setting the DEVIATION—NORMAL HIGH switch to HIGH.

Example: A deviation of 36 kc/s is required at a carrier frequency of 80 Mc s.

The carrier frequency lies within the 54- to 110-Mc's band. The meter multiplying factor for this band is 4: therefore, for 36-kc's deviation, the meter should be set (by means of the SET MOD, control) to read

$$\frac{36}{4} = 9$$
 kc/s.

Do this on the bottom scale of the meter with the DEVIATION RANGE switch set to 15 kc s.

### (a) F.M. from the internal 3-frequency oscillator

- (1) Set the MOD. SELECTOR switch to INT. MOD.—F.M.
- (2) Turn the SET MOD. FREQ. switch to give the required modulation frequency---400, 1.000, or 1,500 c s.
- (3) Set the DEVIATION RANGE switch as required. If, at carrier frequencies less than 13.5 Mc/s, or greater than 27.5 Mc/s, more than 15 kc/s deviation is required, set the DEVIATION---

NORMAL/HIGH switch to HIGH. (Deviations greater than 15 kc/s are not obtainable on the 13.5- to 27.5-Mc/s carrier-frequency band, the maximum deviations obtainable on the other carrier-frequency bands are given in Table 2.)

- (4) Adjust the SET CARRIER control to bring the meter pointer to the SET R.F. mark.
- (5) With the METER READS key switch held to F.M., adjust the SET MOD, control until the required deviation is indicated on the panel meter; read the meter on its middle scale when the DEVIA-TION range switch is at 5 kc/s, and read on the lower scale when the switch is at 15 kc/s. If the DEVIATION-NORMAL/HIGH switch is set to HIGH, the meter readings must be multiplied by the appropriate factor given in Table 2.
- (6) Release the METER READS key switch and, if necessary, repeat (5) above.

#### (b) F.M. from an external source

- (1) Set the MOD. SELECTOR switch to EXT. MOD. -- F.M.
- (2) Set the DEVIATION RANGE switch as required. If at carrier frequencies less than 13.5 Mc/s, or greater than 27.5 Mc/s, more than 15 kc/s deviation is required, set the DEVIATION— NORMAL/HIGH switch to HIGH. (Deviations greater than 15 kc/s are not obtainable on the 13.5- to 27.5 Mc/s carrier-frequency band; the maximum deviations obtainable on the other carrier-frequency bands are given in Table 2.)
- (3) Adjust the SET CARRIER control to bring the meter pointer to the SET R.F. mark.
- (4) Couple the external modulation source to the EXT. MOD. and E terminals.
- (5) With the METER READS key switch held to F.M., adjust the SET MOD, control until the required deviation is indicated on the panel meter; read

the meter on its middle scale when the DEVIA-TION RANGE switch is set to 5 kc/s, and read on the lower scale when the switch is set to 15 kc/s. If the DEVIATION—NORMAL/HIGH switch is set to HIGH, the meter readings must be multiplied by the appropriate factor given in Table 2.

For any settings of the DEVIATION RANGE and DEVIATION—NORMAL/HIGH switches, and within the modulation frequency range 50 c/s to 15 kc/s, approximately 25 volts r.m.s. is required between the EXT. MOD. and E terminals for full deviation. With respect to 1 kc/s, the frequency characteristic of the modulation system is flat to within  $\pm$  1 dB from 50 c/s to 15 kc/s.

#### 2.5.4 SIMULTANEOUS FREQUENCY AND AMPLITUDE MODULATION

- (1) Set up the required depth of amplitude modulation as detailed in Section 2.5.2 (a).
- (2) Leaving the MOD. SELECTOR switch at INT. MOD. —A.M., and without altering the setting of the SET MOD. control, set up the required deviation in a similar manner to that detailed in Section 2.5.3 (b); in this case, adjust the amount of deviation by variation of the audio input from the external modulation source.

#### 2.6 R.F. OUTPUT ARRANGE-MENTS

Five factors affect the output level from the Signal Generator:—

- (a) The SET CARRIER control whose setting determines the input level to the attenuator cascade.
- (b) The 'coarse' or OUTPUT VOLTAGE attenuator.
- (c) The ' fine ' or MULTIPLY BY attenuator.
- (d) The TERMINATING UNIT which plugs on the end of the output cable from the fine attenuator.
- (e) ATTENUATOR PAD Type TM 5552, which is an optional accessory designed for insertion between the output cable and TERMINATING UNIT when especially low output levels are required.

The SET CARRIER control is adjusted in conjunction with the panel meter; with the METER READS key switch in its central position, the panel meter forms part of a crystal voltmeter which monitors the input to the coarse attenuator. The panel meter has three main marks on its scale; these marks are -1 dB, SET R.F., and -1 dB, respectively. Normally, the SET CARRIER control should be adjusted to bring the meter pointer to the SET R.F. mark.

Four 20-dB steps give the coarse or OUTPUT VOLTAGE attenuator a total range of 80 dB; each setting of the attenuator control has markings in yellow and in white, the yellow markings being in decibels relative to  $1 \mu V$ ; the white markings are directly in units of voltage.

Ten 2-dB steps give the fine or MULTIPLY BY attenuator a total range of 20 dB; each setting of the attenuator control has markings in yellow and white, the yellow markings being in terms of decibels relative to  $1 \mu V$ , and the white markings, multiplying factors for the white voltage markings on the coarse attenuator.

Both attenuators have a characteristic impedance of 75 ohms and, 'looking into' the coaxial socket at the end of the output cable, the instrument appears as a generator with a source impedance of 75 ohms at all attenuator settings.

The TERMINATING UNIT is, essentially, a 6-dB attenuator pad; 'looking into' its input socket, with its output sockets unterminated, the TERMI-NATING UNIT presents an impedance of 75 ohms, while the two outlets present impedances of 52 and 75 ohms respectively.

The ATTENUATOR PAD has a characteristic impedance of 75 ohms and provides an optional, additional, 20-dB attenuation of the output signal.

It should be noted particularly that the r.f. output controls on the Signal Generator are calibrated in terms of source e.m.f. or open-circuit output voltage. The significance of quoting the output of a signal generator in this way will be apparent when it is remembered that one of the primary functions of a signal generator is to simulate a received signal as it would come from an aerial.

To take a simple case—that in which a 75-ohm receiver is fed from a 75-ohm dipole—the e.m.f. induced in the aerial is shared between its inherent 75-ohm radiation resistance and the matched 75-ohm receiver input. Clearly, when the same receiver is fed from a signal generator, the corresponding signal strength is given by the source e.m.f. of the signal generator, and not by the onload p.d. at the receiver terminals.

#### 2.6.1 OUTPUTS FROM I μV TO 100 mV AT 52 AND 75 OHMS

It is intended that the Signal Generator should normally be used with the SET CARRIER control adjusted to bring the meter pointer to the SET R.F. mark; with the TERMINATING UNIT coupled directly to the output cable; and without the ATTENUATOR PAD Type TM 5552.

Used in this way, the Signal Generator should be regarded as a source of zero impedance in series with a resistance of either 75 ohms or 52 ohms, the open-circuit output level, or source e.m.f., being variable in 2-dB steps from 1  $\mu$ V to 100 mV and being given:



Fig. 2.7 Outputs via Terminating Unit.

- (a) directly in terms of decibels relative to  $1 \mu V$ , by the sum of the yellow settings of the OUTPUT VOLTAGE and MULTIPLY BY attenuators;
- (b) *directly in voltage*, by the product of the white settings of the OUTPUT VOLTAGE and MULTIPLY BY attenuators.

The +1-dB and -1-dB marks on the panel meter allow interpolation between the 2-dB steps of the MULTIPLY BY attenuator. Setting the meter pointer to either the +1-dB or -1-dB mark increases or decreases the input to the attenuator cascade by 1 decibel. Thus, using the SET CARRIER control and panel meter in conjunction with the OUTPUT VOLT-AGE and MULTIPLY BY attenuators, the output level from the Signal Generator can be varied in 1-dB steps over the range 0 to +100 dB relative to 1  $\mu$ V.

It should be noted that the white voltage indication given by the attenuator controls is not directly applicable when the meter is set to other than the SET R.F. mark; with the meter at -1 dB, the source e.m.f. at the TERMINATING UNIT outlets is 0.89 of the indicated voltage; with the meter at +1 dB, the source e.m.f. is 1.12 of the indicated voltage.

#### 2.6.2 OUTPUTS FROM 2 μV TO 200 mV AT 75 OHMS ONLY

With the TERMINATING UNIT detached and with the meter at the SET R.F. mark, the output level obtained directly from the plug at the end of the r.f. output cable is variable in the range 2  $\mu$ V to 200 mV and is derived via a source impedance of 75 ohms.

Under these conditions, the open-circuit level, or source e.m.f., in terms of decibels relative to  $1 \mu V$  is obtained by adding 6 dB to the sum of the meter reading and the yellow indications of the OUTPUT VOLTAGE and MULTIPLY BY attenuators; the source e.m.f. is given directly in voltage by doubling the product of the white indications of the OUTPUT VOLTAGE and MULTIPLY BY attenuators.

#### 2.6.3 OUTPUTS FROM 0.1 μV TO 10 mV AT 52 AND 75 OHMS

With the TERMINATING UNIT coupled to the r.f. output cable via the optional 20-dB ATTENUATOR PAD and with the meter at the SET R.F. mark, the output level from the TERMINATING UNIT is variable in the range 0.1  $\mu$ V (nominal) to 10 mV.

In this case, the source e.m.f. in terms of decibels relative to  $1 \mu V$  is obtained by subtracting 20 dB from the sum of the meter reading and the yellow indications of the OUTPUT VOLTAGE and MULTIPLY BY attenuators; the source e.m.f. is given directly in voltage by dividing the product of the white indications of the OUTPUT VOLTAGE and MULTIPLY BY attenuators by 10.



Fig. 2.8 Output Direct from Output Lead.



Fig. 2.9 Outputs via 20-dB Pad and Terminating Unit.

#### 2.6.4 OUTPUT IN TERMS OF VOLTAGE DEVELOPED ACROSS AN EX-TERNAL LOAD

For some particular applications, it may be desired to work not in terms of source e.m.f. as indicated by the meter and attenuator controls, but in terms of actual voltage developed across the external load. This on-load, or terminal voltage, is given by the expression

where  $V_L$  = actual voltage developed across the external load.

- E = the source e.m.f. of the Signal Generator.
- $Z_L$  = the impedance of the external load.
- $Z_0$  = the source impedance of the Signal Generator; (with the TERMINATING UNIT in use,  $Z_0 = 75$  or  $52\Omega$ ; with the TERMINATING UNIT removed,  $Z_0 = 75\Omega$ ).

A series of multiplying factors, which can be used to convert from source e.m.f. to actual voltage developed across an external *resistive* load, and which have been derived with the aid of the above expression, are given in Table 3 for a selection of typical load values.

#### 2.6.5 MATCHING TO EXTERNAL LOADS OTHER THAN 52 OR 75 OHMS

The TERMINATING UNIT supplied with the Signal Generator allows r.f. outputs to be obtained from a source impedance of either 52 or 75 ohms.

If the equivalent under test has an input impedance of other than 52 or 75 ohms, and if it is required to present the equipment with a signal derived from a matched source, then it is necessary to modify the output arrangements of the Signal Generator. The simple modifications required are described in sub-sections (a) and (b) which follow. These expressions are based on the assumption that the external load impedance  $Z_L$  is essentially resistive. Where  $Z_L$  is not essentially resistive, it may be necessary for the user to revise these expressions to take account of the reactive component of the load.

In these sub-sections it is assumed that the TERMINATING UNIT is in circuit, and that the 20-dB ATTENUATOR PAD is out of circuit.

(a) External load less than that of the TERMINATING UNIT outlet in use.

The impedance presented to the load can be made equal to the load impedance by shunting the TERMINATING UNIT outlet with a single resistor,  $R_p$ , where

#### TABLE 3

External load impedance	Approximate multiplying factor convert from source e.m.f. to a voltage developed across an ext resistive load			
in ohms	Ζο 75Ω	$Z_0 52\Omega$		
10	0.12	0.16		
20	0.21	0.28		
30	0.29	0.36		
40	0.35	0.43		
50	0.4	0.49		
52	0.41	0.5		
60	0.44	0.53		
70	0.48	0.57		
75	0.5	0.59		
80	0.51	0.61		
100	0.57	0.65		
150	0.67	0.74		
200	0.73	0.79		
300	0.8	0.85		
600	0.89	0.92		



and where Z<sub>0</sub> = the source impedance of the Signal Generator at the TERMINATING UNIT outlet in use;

 $Z_L$  = the impedance of the external load. Under these conditions, the relationship between E<sub>SG</sub>, the e.m.f. indicated by the attenuator controls on the Signal Generator, and E<sub>E</sub>, the effective source e.m.f. presented to the external load, is given by the expression

*Example:* It is required to provide a signal of 25  $\mu$ V effective source e.m.f. at a source impedance of 20 ohms.

Since the new source impedance is to be 20 ohms, the output is taken from the 52-ohm outlet on the TERMINATING UNIT, the 52-ohm outlet being chosen in preference to the 75-ohm outlet to obtain the minimum reduction from  $E_{SG}$  to  $E_E$ .

From expression (2), the value of  $R_p$  to be connected in parallel with the 52-ohm outlet of the TERMINATING UNIT is

$$\frac{52\times20}{52-20}=32\cdot5\Omega.$$

From expression (3), the attenuator controls on the Signal Generator should be set to indicate

$$25 \times \frac{32 \cdot 5 - 52}{32 \cdot 5} = 65 \ \mu \text{V}.$$

The attenuators cannot be set to indicate exactly 65  $\mu$ V and they should therefore be set to 63  $\mu$ V the setting nearest to the required value for E<sub>SG</sub>. 63  $\mu$ V is approximately -0.3 dB relative to 65  $\mu$ V and, if desired, the user may obtain an E<sub>SG</sub> nearer to 65  $\mu$ V by adjustment of the SET CARRIER control to bring the meter pointer to an estimated -0.3 dB.

As a result of shunting the output of the TER-MINATING UNIT with 32.5 ohms and setting the attenuator controls in the manner described, the equipment under test is fed from a source whose effective output impedance is 20 ohms and whose effective source e.m.f. is  $25 \mu V$ ; the actual voltage developed across the input impedance of the equipment under test is, of course,  $12.5 \mu V$ .

(b) External load greater than that of the TER-MINATING UNIT outlet in use.

The impedance presented to the load can be made equal to the load impedance by connecting a single resistor,  $R_s$ , in series with the Signal Generator output. The value of  $R_s$  is given by the expression

where  $Z_L$  = the impedance of the external load.  $Z_0$  = the source impedance of the Signal Generator at the TERMINATING UNIT outlet in use.

Under these conditions, the effective source e.m.f.  $(E_E)$  of the Signal Generator and series resistor combined, equals the source e.m.f.  $(E_{SG})$  of the Signal Generator alone, i.e.

*Example:* It is required to provide a signal of 10  $\mu$ V effective source e.m.f. at a source impedance of 300 ohms.

Since the new output impedance is greater than either 52 or 75 ohms, there is no advantage to be gained by using one of the TERMINATING UNIT outlets in preference to the other; in this example it is assumed that the 75-ohm outlet is used.



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Fig. 2.12 Matching to Balanced Loads.



From expression (4) the value of  $R_s$  to be connected in series with the 'live' connection between the Signal Generator and the equipment under test, is

$$300 - 75 = 225 \Omega$$
.

From expression (5), the attenuators on the Signal Generator should be set to indicate

#### $10 \ \mu V.$

In this way, the equipment under test is fed from a source whose effective impedance is 300 ohms and whose effective source e.m.f. is  $10 \mu V$ ; the actual voltage developed across the input impedance of the equipment under test is, of course,  $5 \mu V$ .

#### 2.6.6 MATCHING TO BALANCED LOADS

The preceding Sections dealing with r.f. output arrangements are based on the supposition that the equipment being fed from the Signal Generator has an unbalanced input circuit.

With certain types of equipment, the input circuit is in the form of a balanced winding; such equipment can be fed from the unbalanced output of the Signal Generator by interposing two loading resistors between the TERMINATING UNIT outlet and the ends of the balanced input winding. This method makes use of the auto-transformer effect of the centre-tapped winding, and is *not* suitable for resistive balanced inputs.

One resistor,  $R_1$ , is connected in series between the earth connection of the TERMINATING UNIT outlet in use and one side of the balanced winding; the other resistor,  $R_2$ , is connected in series between the 'live' connection of the TERMINATING UNIT outlet in use and the other side of the balanced winding.

Values for  $R_1$  and  $R_2$  may be computed from the following expressions:

$$R_2 = \frac{Z_{LB}}{2} - Z_0$$
 .....(7)

where  $Z_{LB}$  = the total line-to-line impedance of the balanced winding.

$$Z_0$$
 = the source impedance of the Signal Generator at the TERMINATING UNIT outlet in use.

With the equipment under test and the TER-MINATING UNIT of the Signal Generator interconnected via  $R_1$  and  $R_2$  as described above, the source e.m.f. ( $E_{SG}$ ) indicated by the Signal Generator controls is equal to the effective line-to-line source e.m.f. ( $E_E$ ) 'seen' by the equipment under test.

*Example:* It is required to match the 75-ohm outlet to a balanced winding whose total line-to-line impedance is 200 ohms.

From expression (6), the value of  $R_1$  is

$$\frac{200}{2} = 100 \Omega.$$

From expression (7), the value of  $R_2$  is

$$\frac{200}{2} - 75 = 25\Omega.$$

 $R_1$  is connected in series with the earth connection of the TERMINATING UNIT and one side of the balanced winding;  $R_2$  is connected in series with the 'live' connection between the TERMINATING UNIT and the other side of the balanced winding.

#### 2.7 SYNCHRONIZING SIGNAL

An audio sinewave signal, derived from the internal a.f. oscillator, is available between the SYNC and E terminals of the instrument when the MOD. SELECTOR switch is set at either of the INT. MOD. positions. The frequency of the signal will depend on the setting of the SET MOD. FREQ. switch; it has an open-circuit level which varies from about 30 volts at 400 c/s to about 100 volts at 1500 c/s, and is derived via a source impedance of approximately 250 k  $\Omega$ .

When an output from the equipment under test is being viewed on a cathode-ray oscilloscope, it will often be found convenient to lock the c.r.o. time base directly with the SYNC signal rather than with the actual signal being viewed.

The sync output can, of course, also be used when an audio-frequency signal is required for the equipment under test.

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## 3 Operational Summary

When the user is familiar with the principles and techniques of operation detailed in Section 2 of this handbook, the following abridged operating instructions may be found convenient.

Check correctness of mains transformer tappings before use.

### STANDARDIZING THE FREQUENCY SCALE

Switch mains ON and set RANGE switch to 13.5–27.5; with MOD. SELECTOR switch set to other than INT. MOD.—F.M. or EXT. MOD.—F.M., and using headphones plugged into CRYSTAL CHECK socket, tune main dial to crystal check point near centre of band. Bring movable cursor in line with dial calibration corresponding to crystal check point. Check accuracy of frequency indication above and below point to which cursor was originally set, equalize errors over band by readjusting cursor. See Section 2.4.2.

#### TUNING

Set RANGE switch to band required; rotate TUNE control until cursor indicates required frequency. For higher frequency-accuracy, compute relationship of frequency change to change in auxiliary dial setting between crystal check points or scale markings embracing required frequency. Starting from selected point below required frequency, rotate TUNE control so that incremental dial traverses calculated number of divisions. See Sections 2.4.1 and 2.4.4.

#### INCREMENTAL FREQUENCY ADJUSTMENT

Make small carrier changes by means of INC. FREQ. control, using multiplying factors as shown on front panel. See Section 2.4.3.

#### C.W. OPERATION

With MOD. SELECTOR switch set to C.W., adjust SET CARRIER to bring meter pointer to SET R.F.; adjust step attenuators to obtain required output level. See Section 2.5.1.

### AMPLITUDE MODULATION Internal:

With MOD. SELECTOR switch at INT. MOD.—A.M., select required modulation frequency on SET

MOD. FREQ. switch, adjust SET CARRIER to bring meter pointer to SET R.F. With METER READS switch at A.M., adjust SET MOD. to bring meter pointer to required modulation depth. Release METER READS switch and, if necessary, readjust SET CARRIER; adjust step attenuators to obtain required output level.

#### External:

As for internal, except that MOD. SELECTOR switch is set to EXT. MOD.—A.M.; SET MOD. FREQ. switch is inoperative, and external signal is injected between EXT. MOD. and E terminals. Approximately 15 volts r.m.s. (100 c/s to 10 kc/s) is required to produce 30% modulation. See Section 2.5.2.

#### FREQUENCY MODULATION

#### Internal:

With MOD. SELECTOR switch at INT. MOD.—F.M., select required modulation frequency on SET MOD. FREQ. switch. Set DEVIATION RANGE switch as required, and adjust SET CARRIER control to bring meter pointer to SET R.F. With METER READS switch at F.M., adjust SET MOD. to bring meter pointer to required deviation on meter scale appropriate to DEVIATION RANGE switch setting. (For deviations greater than 15 kc/s, set DEVIATION—NORMAL/HIGH switch to HIGH and multiply meter readings by factor given in Table 2, Section 2.5.3.) Release METER READS switch and, if necessary, readjust SET CARRIER; adjust step attenuators to obtain required output level.

#### External:

As for internal, except that MOD. SELECTOR switch is set to EXT. MOD.—F.M., SET MOD. FREQ. switch is inoperative, and external signal is injected between EXT. MOD. and E terminals. Approximately 25 volts r.m.s. (50 c/s to 15 kc/s) is required to produce full deviation. See Section 2.5.3.

### SIMULTANEOUS FREQUENCY AND AMPLITUDE MODULATION

Set up as for Amplitude Modulation Internal. Then, with MOD. SELECTOR switch still set at INT. MOD.—A.M., apply external signal (50 c/s to 15 kc/s) between EXT. MOD. and E terminals. Adjust level of external signal to produce required deviation; do not readjust SET MOD. control. See Section 2.5.4.

#### 4.1 R.F. CIRCUITS

The r.f. oscillator itself (V3) is variable only over a fundamental frequency range of 4.5 to 9.16 Mc/s; the four higher frequency bands are obtained from a chain of four ganged harmonic multipliers (V6, V8, V10, and V12) giving multiplying factors of  $\times 3$ ,  $\times 2$ ,  $\times 2$ , and  $\times 2$  respectively. The setting of the frequency RANGE switch determines which of the multipliers acts as the output stage. Output over the 1.5- to 13.5-Mc/s band is obtained by applying the 27- to 55-Mc/s output of the second multiplier to a single valve circuit (V7a) which combines the functions of mixer and 30-Mc/s oscillator. The variable-frequency output from the second multiplier is thus heterodyned with a fixed 30-Mc/s signal, and the output from the oscillator/ mixer stage contains a difference-frequency component which is utilized-after filtering and amplification (by V7b)-to provide outputs between 1.5 and 13.5 Mc/s.

The main tuning dial has five scales, all directreading in output frequency. To facilitate tuning, a slow-motion worm-and-wheel drive is incorporated; this control is fitted with a dial marked linearly from 0 to 100 to assist the operator in subdividing the frequency scales of the main tuning dial. In addition, there is a fine-tuning control. Fine tuning is achieved by varying the reactorscreen supply voltage. The frequency coverage on the highest-frequency band is approximately 24 kc/s and proportionately less on the lower bands.

A carrier on/off switch (S11) is included to enable the r.f. signal to be interrupted without affecting the output circuits of the generator. This switch interrupts the h.t. supply to the r.f. oscillator valve and also the supply to the screens of the multiplier valves for the band in use.

For all the r.f. bands, the output is taken via two resistive 75-ohm ladder-network attenuators in cascade. The first attenuator has a range of 80 dB and is variable in 20-dB steps; the second has a range of 20 dB in 2-dB steps. The input to the cascade is adjustable by means of the SET CARRIER control (R44), and is monitored by the MODULATION meter M1. The meter scale has a SET R.F. mark, and, respectively above and below this mark, +and -1-dB marks to allow interpolation between the 2-dB steps of the attenuator. The output from the second attenuator is applied to a coaxial cable which is permanently attached to the instrument; the direct open-circuit output obtainable from this



Fig. 3.1 Block Schematic Diagram.

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cable is at a source impedance of 75 ohms and is variable between 2  $\mu$ V and 200 mV. By using the plug-on TERMINATING UNIT supplied, outputs 6 dB down on this range are obtainable at source impedances of both 75 and 52 ohms. With the optional ATTENUATOR PAD interposed between the output cable and the TERMINATING UNIT, outputs down to 0.1  $\mu$ V are obtainable.

To provide for incremental carrier shift and for frequency modulation, a reactor valve (V2) is included in the tuned circuit of the r.f. oscillator. Movement of the INC. FREQ. controls (R112 and the S10 potentiometer network) varies the d.c. bias applied to the grid of V2, causing a change in its mutual conductance and thus a change in the r.f. oscillator frequency. Both the d.c. shift voltage and the a.f. modulating signal are applied to the grid of the reactor valve via a tracking potentiometer (R7); this is ganged to the main tuning capacitor so that the deviation or carrier shift is kept constant as the Signal Generator is tuned over any one band.

The built-in crystal calibrator—the crystal unit of which has a fundamental frequency of 333.3 kc/s —is coupled to the variable-frequency r.f. oscillator and provides 14 checking points on each of the four upper frequency bands covered by the Signal Generator. The h.t. supply to the calibrator is automatically switched on by the insertion of a telephone plug into the CRYSTAL CHECK jack on the front panel; the heterodyne beats at the checking points may then be heard in the headphones or via the receiver under test. The cursor of the tuning dial is adjustable so that it may be set to correspond exactly with the nearest crystal checking point.

#### 4.2 MODULATION SYSTEMS

Either internal or external a.f. modulation (f.m. or a.m.) may be applied; the SET MOD. FREQ. switch (S12) brings into circuit the appropriate tuning capacitor to give 400, 1,000, or 1,500 c/s modulation as required. For frequency modulation the a.f. signal passes through V5, switched as a cathode follower, and is applied to the reactor-valve input via the switched potentiometer network at S2ba and S2ca (part of the RANGE switch), and the tracking potentiometer R7. By this means, the ratio of the a.f. input voltage to f.m. deviation is maintained constant at all frequencies on each band, and is independent of the setting of either the RANGE switch or the TUNE controls.

The normal deviation ranges on all carrier bands are 0 to 5 kc/s and 0 to 15 kc/s. By means of the DEVIATION switch S5, the switched potentiometer system can be by-passed, thus enabling the deviation to be increased proportionally with increase in frequency multiplication and permitting a maximum deviation on the highest-frequency band of  $15 \times 8$ = 120 kc/s. On the 1.5- to 13.5-Mc/s band, the maximum deviation obtainable is 30 kc/s.

Amplitude modulation to a depth continuously variable up to 50% is applied to the highest harmonic multiplier which is operating for the particular r.f. output band in use; this method helps to reduce the spurious frequency modulation often encountered when modulating an r.f. oscillator directly. The modulation is effected by supplying the anodes and screens of the multipliers from the tapped choke output of V5 which is switched to function as an a.f. amplifier.

Simultaneous amplitude and frequency modulation, for use, for example, when investigating the performances of limiter stages in f.m. receivers, is obtained by setting up the instrument for internal a.m. and then applying f.m. from an external source.

#### 4.3 MONITORING ARRANGE-MENTS

A two-stage amplifier-voltmeter provides monitoring facilities for a.m. depth and f.m. deviation. When S3 is switched to F.M., deviation is indicated on the panel meter by sampling the modulating voltages injected into the reactor valve V2: when switched to A.M., the input to the attenuators is sampled via the demodulating diode X2. When S3 is in the C.w. position, to which it is spring-biased, the voltmeter continuously monitors the r.f. input to the attenuators by means of its connection via the contacts S3b, and the silicon diode X2.

The design of the modulation monitoring circuits is such that with the Signal Generator set up for simultaneous a.m. and f.m., both percentage depth, and deviation, can be read independently.

#### 4.4 POWER UNIT

The secondary winding of the mains transformer T4, in conjunction with the full-wave rectifier V11, provides for the positive d.c. h.t. requirements of the instrument; the h.t. supply to the reactor and r.f. oscillator valves is stabilized by means of a gas-filled stabilizer V9. The negative supply for the reactor-valve bias is drawn from a voltage-doubling circuit employing double-diode valve V15, and gas-filled stabilizer V14.

The primary of T4 is tapped to allow for operation from 100 to 150 volts, or 200 to 250 volts. Adequate filtering is introduced into the a.c. input circuit by means of the network C84, L24, C86 and C85, L25, C87.

### Maintenance

#### 5.1 GENERAL

Section 4, TECHNICAL DESCRIPTION, of this handbook deals with the internal circuits of the Signal Generator and it is strongly recommended that the user should familiarize himself with the principles described there before commencing the adjustment or replacement of component parts of the instrument.

The Circuit Diagrams show all the electrical components contained in the instrument together with their values. The full description of these components is given in the Spares Ordering Schedule; the Schedule also lists certain selected mechanical components.

The physical location of the electrical components is shown on the Component Layout Illustrations.

#### 5.2 REMOVAL OF CASE

To remove the Signal Generator case:-

(1) Remove the screw securing the small plate in the left-hand side pocket; the mains lead is cleated to the case by means of this plate.

- (2) Extract the eight screws from around the edge of the front panel.
- (3) Pull the instrument clear of its case and disconnect the six-way interconnecting cable from the power unit chassis.
- (4) Detach the screw, from the inside of the case, which holds the cleating plate for the r.f. output cable to the right-hand side pocket.
- (5) After removing the seven screws from the underside of the case, lift out the power unit.

#### 5.3 MAINS INPUT ARRANGE-MENTS

The instrument is fitted with a mains transformer which has a double-wound primary; each primary section is tapped and the two sections can be connected in series-parallel for 100- to 150-volt operation or in series for 200- to 250-volt operation.

The 100- to 150-volt or the 200- to 250-volt range is selected by links on the coil of the transformer. Selection of intermediate voltages within either range is made by means of fly leads on the



Fig. 5.1 Mains Transformer Tappings.

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transformer tags. These tags are common to both ranges and are, therefore, annotated with two voltages; the applicable voltage depends on the position of the range links.

One fly lead must always be connected to either the '0' or the '10' tag; the other is connected to the tag whose voltage, added to 0 or 10 as appropriate, equals the mains supply voltage. Do not connect the fly leads to the tags marked TAP A or TAP B.

In order to examine the connections to the transformer and, if necessary, make adjustments, the instrument must be removed from its case in the manner described in Section 5.2. With the instrument out of its case, the transformer (T4 on Circuit Diagram, Fig. 8.2, and on Component Layout Illustration, Fig. 6.7) is immediately accessible.

For Supply Voltages within the range 200 to 250 volts, the tags on the transformer *must* be linked in the following manner:—

'TAP A' to 'TAP B'

For Supply Voltages within the range 100 to 150 volts, the tags on the mains transformer *must* be linked in the following manner:—

#### 5.4 ACCESS TO ENCLOSED SUB-ASSEMBLIES

General tests or some peculiarity in the performance of the Signal Generator may suggest the desirability of inspecting the interior of one of the enclosed sub-assemblies which form part of the instrument. Any of these sub-assemblies can be dismantled by following the appropriate procedure as detailed in the sections below.

#### 5.4.1 R.F. UNIT

To remove the screening cover from the r.f. unit:---

- (1) Remove the instrument from its case and lay it face downwards.
- (2) Extract the two screws which secure the screening cover of the r.f. unit.
- (3) Grip the sides of the screening cover and draw it off; the cover is held by earthing contact springs and will consequently offer some resistance to removal.

#### 5.4.2 'MULTIPLY BY' ATTENUATOR

A view of the MULTIPLY BY (fine) attenuator with the screening cover removed is shown in Component Layout Illustration, Fig. 6.6. To dismantle the attenuator:—

- (1) Remove the attenuator screening cover after extracting the single securing screw.
- (2) Remove the front-panel control knob after slackening the two grub screws which secure it to its associated spindle.
- (3) Detach the main body of the attenuator from the front panel by extracting five screws; three of these screws are visible on removal of the control knob as in (2) above; the two remaining screws are located immediately above the 8-dB and 12-dB panel markings.

With the attenuator thus detached, it remains coupled to the body of the instrument by two coaxial leads; these leads are normally long enough to permit inspection and, if necessary, replacement of the attenuator resistors without completely disconnecting the attenuator.

Reassemble the attenuator in the reverse order to that detailed above.

#### 5.4.3 'OUTPUT VOLTAGE' ATTENUA-TOR AND MONITOR DIODE

In addition to the actual attenuator components, the r.f. monitor diode, X2, and its associated filter components are mounted in the OUTPUT VOLTAGE attenuator casing. When dismantling the attenuator, the user should refer to Component Layout Illustration, Fig. 6.6. Access to the diode, X2, resistors R71 and R72, and capacitors C88, C89, and C90 can be obtained by removing the cover of the attenuator in the following manner:

- (1) Disconnect R70 from the small insulated spigot projecting through the cover of the attenuator.
- (2) Remove the central securing screw and lift the screening cover clear of the attenuator body.
- To obtain access to the attenuator resistors, R73 to R82, detach the attenuator from the front panel
- of the Signal Generator in the following manner:-
- (3) Remove the control knob by slackening the two grub screws securing it to its spindle.
- (4) Extract the five fixing screws securing the attenuator to the front panel; three of these screws are immediately visible on removing the control knob as in (3) above; the two remaining screws are located immediately above and to the right of the coarse-attenuator panel markings.

With the attenuator detached as in (4) above, it remains coupled to the body of the instrument by two coaxial cables. These cables are, however, long enough to permit inspection and, if necessary, replacement of the attenuator-resistors without completely disconnecting the attenuator.

Reassemble the attenuator in the reverse order to that detailed above.

#### 5.4.4 MAINS INPUT FILTER UNIT

To gain access to the components comprising the mains input filter:--

- (1) Remove the nut and screw which secure, at the open end, the two halves of the mains filter unit screening cover.
- (2) Separate the push-fit screening channel from the fixed half of the screening cover.

Reassemble the screening cover in the reverse order to that detailed above.

#### 5.4.5 POWER UNIT

To remove the power unit from the instrument case:—

- (1) Remove, from the underside of the instrument case, the five screws which engage with nuts along the front and left-hand flanges of the power unit chassis.
- (2) Holding the power unit with one hand, remove the remaining two screws which engage with the tapped bushes on the right-hand flange of the power unit.

Replace the power unit in the reverse order to that detailed above.

#### 5.5 WORKING VOLTAGES

The voltages given in this section for guidance when servicing the instrument were obtained from

TABLE A

	IADL	L 7	
Valve No.	Va	$V_{g2}$	$V_k$
V1	245	50	1.5
V2	150	150	4
V3	150	75	
V4	55	55	
<b>V</b> 5	250	250	3.6*
V6	125	160	
V7†	Pin 1 235		
$V7^{\dagger}$	Pin 6 255		2.5
V8	105	145	
V9	150		
V10	145	145	
V11‡	Pin 4 260		295
	Pin 6 260		
V12	150		
V13	Pin 1 260		Pin 3 110
V13	Pin 6 90		Pin 8 16
	, I		

\*The cathode potential of V5 will increase to 45 volts when the MOD. SELECTOR switch is set to INT. MOD.—F.M.

<sup>†</sup>When checking the voltages on V7, set the RANGE Mc/s switch to 1.5–13.5.

‡All voltages shown are d.c. except for V11 anodes.

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measurements made with a 20,000 ohms/volt meter on a representative Signal Generator Type TF 995A/5.

Primary winding of T4 (Supply Voltage)

240 volts a.c. H T secondary winding and chassis

11.1. secondary winding and c	1143313
-	260-0-260 volts a.c.
Heater winding LTR	5 volts a.c.
Heater winding LT	6.3 volts a.c.
Pin 1 on plug PL1 and chassis	260 volts d.c.
Junction of R117/R118 and ch	assis -85 volts d.c.
Junction of L16/L17 and chase	sis 280 volts d.c.
Cathode of V11 and chassis	295 volts d.c.

Table 4 lists certain valve electrode voltages in the TF 995A/5. When checking the instrument against these voltages, the MOD. SELECTOR switch should be set to INT. MOD.—A.M., the RANGE switch (unless otherwise specified) should be set to 108– 220 Mc/s, and the SET CARRIER and SET MOD. controls should be turned to their maximum and minimum settings respectively.

#### 5.6 REPLACEMENT OF VALVES AND SEMICONDUCTORS

The types of valve used in the instrument, their base connections, and some guidance as to suitable alternatives if the types originally fitted are not readily available, are given in Table 5.

The valves and semiconductor diodes may normally be replaced without special selection. Valves V1, V5, V9, V11, and V13 to V15 are immediately accessible on removing the instrument from its case. To gain access to the 333·3-kc/s oscillator crystal, X1, and to the remaining valves, remove the R.F. Unit screening cover. The crystal diode, X2, forms part of the OUTPUT VOLTAGE attenuator assembly and can be removed by the procedure detailed in Section 5.4.3.

Replacement of valves or semiconductors may necessitate either the reselection of associated components or readjustment of associated preset controls; aspects of this reselection and readjustment are discussed in the following Section.

#### 5.7 PRESET AND SPECIALLY SELECTED COMPONENTS

During the factory calibration of the instrument, certain of its performance characteristics are brought within fine limits by means of preset components. Following the replacement or ageing of certain fixed components, it may become necessary to repeat the calibration procedure by which the presets were adjusted.

The Description column of the Spares Ordering Schedule shows which of the components are of

#### TABLE 5

Any valve which becomes faulty should preferably be replaced by a valve of the type originally supplied in the instrument and designated in the following table. If this is not possible, the additional data given by the table may be used as a guide to suitable alternatives.

Valve	Type	Base		British Commercial Equivalent	British Services Equivalent	U.S. Equivalent
V1	6AK6 Power Pentode		(B7G)		CV1762	6AK6
V2, V4, V6, V8, V10, V12	6AK5 H.F. Pentode		(B7G)	EF95	CV850	6AK5
V3	EF86 Pentode		(B9A)	2729	CV2901	6267
V5	6AU6 Pentode		(B7G)	EF94	CV2524 CV4023	6AU6
V7, V13	12AT7 Double Triode		(B9A)	ECC81	CV455	12AT7
V9	OA2 Voltage Stabilizer		(B7G)	OA2 150C2 150C4 QS1207	CV1832 CV4020	OA2

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TABLE 5	(conti	inued)	
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Valve	Туре	Base		British Commercial Equivalent	British Services Equivalent	U.S. Equivalent
V11	5Z4G Full-Wave Rectifier		(IO)	R52 GZ30 52KU U50	CV1863	5Z4G
V14	5651 Voltage Stabilizer		(B7G)	QS1209 QS83/3 85A2	CV2573 CV449	5651 OG3
V15	6AL5 Double Diode		(B7G)	D77 6D2 D152 DD6 EB91	CV140	6AL5

the preset type; components which are individually selected are distinguished in that column by a single asterisk.

If, in servicing a TF 995A/5, it is necessary to replace any of these components, it will also be necessary, if the performance or accuracy of the instrument is not to be impaired, to repeat the factory calibration procedure by which the components were originally selected.

Section 5.8 gives a range of tests by which the main points of the performance of the instrument can be checked; this section also deals with the adjustment of preset components and with the choice of value for individually selected components.

It will be appreciated that it may sometimes be necessary to reselect a selected component even though that component itself has not been found faulty and replaced in initial servicing operations. To take an example—the internal modulation oscillator is tuned to 1,000 c/s by T1 and C6. In manufacture, C6 is selected to give an oscillator frequency of 1,000 c/s  $\pm$  5%. In servicing the instrument it might be found that T1 was faulty but that C6 was not. If T1 was replaced then it

TABLE 6

Com- ponent	Section Describing Adjustment or Selection	Com- ponent	Section Describing Adjustment or Selection
R5	5.8.10	<b>R</b> 150	5.8.12
<b>R</b> 7	5.8.10	R153	5.8.12
<b>R</b> 8	5.8.10	R163	5.8.12
R9	5.8.10	C6	5.8.9
<b>R</b> 11	5.8.10	C35	5.8.5
R12	5.8.10	C40	5.8.7
R13	5.8.10	C47	5.8.6
<b>R</b> 14	5.8.10	C59	5.8.7
R19	5.8.10	C66	5.8.6
R24	5.8.11	C76	5.8.6
R25	5.8.11	C83	5.8.6
R27	5.8.4	C93	5.8.4
R44	5.8.6	C101	5.8.9
R63	5.8.11	C102	5.8.9
R65	5.8.15	L18	5.8.6
<b>R</b> 70	5.8.8	L22	5.8.6
R112	5.8.12	L23	5.8.6
R119	5.8.12	T2	5.8.5
R124	5.8.11	T3	5.8.6
			•

would be quite likely that with the original C6 the oscillator frequency would be outside the specified limits of  $\pm$  5% and that a new value of capacitance would have to be chosen.

It therefore follows that, in all servicing involving replacement of components, the user should consider carefully the possible effects on the performance of the stage or stages involved.

Table 6 on page 29 lists the circuit reference numbers of both types of component together with the numbers of the sections in which their adjustment or selection is described.

#### 5.8 SCHEDULE OF TESTS

The following information, based on abstracts from the internal Factory Test Schedule, is included to enable the user to carry out a series of tests by which the main points of performance of the instrument can be checked; it also gives details concerning the adjustment to preset components and the choice of value for individually selected components.

#### 5.8.1 APPARATUS REQUIRED

- (a) 750-volt Insulation Tester.
- (b) Avometer, Model 8.
- (c) Wave Analyser; Marconi Type TF 455 (Series).
- (d) Signal Generator, with standardized output; Marconi Types TF 801 (Series) or TF 995 (Series).
- (e) Valve Voltmeter; Marconi Type TF 1041B.
- (f) Audio-Frequency Oscillator; Marconi Types TF 195 (Series), TF 885 (Series), TF 894 (Series), or TF 1101.
- (g) Cathode-Ray Oscilloscope; Marconi Type TF 1330 (Series).
- (h) Deviation Meter; Marconi Type TF 791 (Series).
- (i) Counter-type Frequency Meter; Marconi Type TF 13452.
- (j) Crystal Calibrator: Marconi Type TF 1374.
- (k) Standardized Wavemeter; Marconi Type TF 975.
- (1) A.M. Communications Receiver, covering the range 1.5 to 220 Mc/s.
- **Note:** For the F.M. on C.W. check (Section 5.8.17), where deviations of less than 50 c/s have to be measured, it is essential that the deviation meter should be modified to operate from battery supplies, or incorporate facilities allowing its local oscillator to be brought under crystal control.

#### 5.8.2 INSULATION

(Apparatus required: Item a) Test the insulation between each pin of the supply plug and chassis with SKT1 engaged with PL1. This reading should not normally be less than 40 M $\Omega$ .

#### 5.8.3 HUM LEVEL

(Apparatus required: Item c) Measure the 100 c/s hum level at HT1 using a Wave Analyser isolated from the TF 995A/5 by a  $4-\mu$ F capacitor. The hum level should not normally exceed 10 mV.

#### 5.8.4 CRYSTAL OSCILLATOR

(Apparatus required: Items e and i) Plug headphones into the CRYSTAL CHECK socket and, by means of a loop of wire slipped over V4, take an output to the Counter-type Frequency Meter. Check the crystal frequency, it should usually lie between  $333\cdot266$  c/s and  $333\cdot400$  c/s. C93 may be padded with a value not exceeding 10  $\mu\mu$ F to achieve this.

Using the Valve Voltmeter, measure the r.f. voltage across R27; it should normally lie between 8 and 10 volts.

#### 5.8.5 BASIC OSCILLATOR

(Apparatus required: Items e and k) Set the MOD. SELECTOR switch to C.W. and the RANGE switch to Band 2, 13.5 to 27 Mc/s. Coarse tune to 13.5 Mc/s (on Band 2) and adjust the dust core of T2 until the circuit oscillates at 4.5 Mc/s as indicated by the Wavemeter. Set the main tuning dial to 27 Mc/s and tune the trimmer C35 until the circuit oscillates at 9 Mc/s. Repeat these two adjustments for the most accurate frequency calibration; a calibration accurate to within  $\pm 1\%$  is usually to be expected if this procedure is carried out. Check the tuning adjustments against the crystal by means of headphones plugged into the CRYSTAL CHECK jack socket.

Measure the r.f. voltages at the anode and grid of V3; these should be of the following order:--

	4.5 Mc/s	9∙0 Mc/s
Grid	2.65 volts	9 volts
Anode	21 volts	41 volts

#### 5.8.6 FREQUENCY MULTIPLIERS

(Apparatus required: Item j)

#### (1) 13.5- to 27-Mc/s band

Set the MOD. SELECTOR switch to C.W., the RANGE switch to 13.5-27 Mc/s, and the SET CARRIER control fully clockwise.

Set the main dial to 13.5 Mc/s, and adjust the core of T3 for maximum deflection on the panel meter. The SET CARRIER control, R44, should be readjusted if necessary.

Set the main dial to 27 Mc/s, and adjust C47 for maximum deflection on the meter.

Repeat these two adjustments several times until no further change is required, finishing with C47. Check that the output as indicated on the frontpanel meter is sensibly constant over the whole band.

#### (2) 27- to 54-Mc/s band

Set the RANGE switch to 27–54 Mc/s, and the SET CARRIER control fully clockwise.

Set the main dial to 27 Mc/s, and adjust the spacing of the turns of L18 for maximum deflection on the panel meter. The SET CARRIER control should be readjusted if necessary.

Set the main dial to 54 Mc/s, and adjust C66 for maximum deflection on the meter.

Repeat these two adjustments several times until no further change is required, finishing with C66. Check that the output as indicated on the frontpanel meter is sensibly constant over the whole band.

#### (3) 54- to 108-Mc/s band

Set the RANGE switch to 54–108 Mc/s and, using a similar procedure to (2) above, adjust L22 and then C76 at 54 and 108 Mc/s respectively.

#### (4) 108- to 220-Mc/s band

Set the RANGE switch to 108–220 Mc/s and, using a similar procedure to (2) above, adjust L23 and then C83 at 108 and 220 Mc/s respectively.

With the R.F. Box cover in position, check the frequency accuracy on all the above bands with the Crystal Calibrator. The frequency accuracy of the TF 995A/5 should be about  $\pm 1\%$ .

#### 5.8.7 1.5- TO 13.5-Mc/s BAND

(Apparatus required: Item l) This test must be made with the r.f. unit cover in position.

By means of a suitable jack plug, connect a pair of headphones to the CRYSTAL CHECK socket.

Set the RANGE switch to 1.5-13.5, and adjust the TUNE control to bring the 30 Mc/s main dial marking (on the 27-54 Mc/s arc) to the cursor; then, using the Crystal Calibrator, tune for zero beat.

With the SET CARRIER control in its fully clockwise position, adjust C40 and C59 alternately to give minimum deflection on the panel meter. These capacitors are accessible through two holes, slightly larger than the ventilation holes, in the top of the r.f. unit cover. Connect the output of the Signal Generator to a receiver, and tune the receiver to some convenient accurately-known frequency between 1.5 and 13.5 Mc/s.

Set the main dial of the TF 995A/5 to this frequency, and adjust C40 for maximum receiver response.

In the absence of any other frequency standard, the receiver tuning may be standardized at frequencies between 4.5 and 9 Mc/s by loosely coupling its input to the basic oscillator of the TF 995A/5. This oscillator should first be standardized against the internal crystal calibrator, the basic-oscillator frequency being given by dividing by three the indication on the 13.5–27 scale.

#### 5.8.8 R.F. OUTPUT VOLTAGE ACCURACY

(Apparatus required: Item e) This test should be carried out with the instrument in its case.

Set the MOD. SELECTOR switch to C.W., and tune to 25 Mc/s. Set the OUTPUT VOLTAGE and MULTIPLY BY attenuators to give a joint indication of 100 dB above 1  $\mu$ V (i.e. both fully clockwise). Connect the Signal Generator to the TERMINATING UNIT, and connect the 75-ohm outlet of the TERMINATING UNIT to the voltmeter. Adjust the SET CARRIER control to give an output level of 100 mV as indicated on the Voltmeter; if the front-panel meter pointer is not exactly at the SET R.F. mark, reselect R70.

Check that the output from the 52-ohm socket is also 100 mV. The maximum obtainable output over all bands should also be checked, it will usually be found to be greater than 1 dB above the SET R.F. mark.

#### 5.8.9 MODULATION OSCILLATOR

Apparatus required: Items e, f and g) With the MOD. SELECTOR switch set to INT. MOD. —A.M. and the SET MOD. FREQ. control at 1,000, monitor the a.f. signal between the SYNC and E terminals. With the Cathode-Ray Oscilloscope, and using the Audio Oscillator as a standard frequency source, verify, by the method of Lissajous figures, that the oscillator frequency lies within the limits 1,000 c/s  $\pm$  5%. If it does not, reselect C6.

Check the modulation-oscillator frequency at 400 c/s and 1,500 c/s by the above method. If necessary, the following capacitors may have to be reselected to obtain the required frequencies: for 400 c/s modulation, C101; for 1,500 c/s modulation, C102.

#### 5.8.10 REACTANCE VALVE INPUT POTENTIOMETER

(Apparatus required: Items c and h) Select the minimum frequency on Band 2 and check that the position of the sliding contact on R7 is such that it will give about 4/5 of maximum resistance; switch to INT. MOD.—F.M., DEVIATION— NORMAL and 15 kc/s DEVIATION RANGE.

Connect the output of the Signal Generator to the Deviation Meter, tune both to 13.5 Mc/s (on Band 2). Adjust the SET MOD. control to give a deviation reading of 15 kc/s and select R19 for minimum f.m. distortion: minimum distortion will be indicated by the best agreement obtained between the two f.m. readings, one on either side of the zero-deviation dip, when using the TF 791 (Series) Carrier Deviation Meter.

The distortion of the modulated signal at the a.f. output terminals should now be measured with a Wave Analyser; distortions in excess of 2% are not normally encountered.

Adjust the SET MOD. control to give 15-kc/s deviation at 13.5 Mc/s. Tune to 27 Mc/s and check that the same deviation is obtained—if not, R7 will require adjustment.

- (1) Loosen the three small Allen screws which secure the spring-loaded gear to the spindle of R7.
- (2) Adjust the setting of R7 relative to the gear by means of a screwdriver inserted in the slot at the end of the spindle.
- (3) Re-tighten the Allen screws.

If 15 kc/s deviation is not obtainable at 27 Mc/s by adjustment of R7, it will be necessary to reselect R8. Reselection of R8 will, of course, entail further adjustment of R7 in the manner already described. In addition, check that the deviation remains reasonably constant over the whole band. To obtain 15-kc/s deviation on Bands 3, 4, and 5, the following may have to be reselected or padded: R13 for Band 3, R11 for Band 4, and R5 for Band 5.

If it is found necessary to select a value very different from the nominal value for one of the above components, one of the following resistors may also have to be re-chosen: R9, R12, or R14; these resistors are included to maintain reasonably constant the load presented by the reactor valve input potentiometer as a whole.

#### 5.8.11 FREQUENCY MODULATION

(Apparatus required: Items h or l) With the DEVIATION RANGE switch (S6) at 15 kc/s, connect the output of the Signal Generator to the Deviation Meter and tune both instruments to 20 Mc/s to obtain a deviation reading. Set the METER READS key switch (S3) to c.w., and adjust the SET MOD. potentiometer (R25) to obtain 15-kc/s deviation as indicated on the deviation monitor. Depress the METER READS switch to F.M. If necessary, adjust R124 to maintain a 15-kc/s deviation reading with the METER READS switch in this position.

Return the METER READS switch to C.W., and set the DEVIATION RANGE switch to 5 kc/s. If necessary, adjust R24 to obtain 5-kc/s deviation. Depress the METER READS switch to F.M.; if the Deviation Meter no longer indicates 5-kc/s deviation, R63 should be reselected.

Set to 15-kc/s and 5-kc/s deviation at any three frequencies on each band. Verify, in each case, with the aid of the Deviation Meter that the frequency modulation indication is accurate within 5%.

If a Deviation Meter is not available, the following method may be used to determine the frequency deviation. This method-the disappearing carrier method-depends upon the fact that the carrier, as opposed, of course, to the sidebands, disappears when the modulation index  $\mu$  (the ratio of the frequency deviation  $\delta F$  to the modulation frequency f) has values of 2.4, 5.52, 8.65, 11.79, etc. Therefore, if the modulation frequency, f, is known, since deviation,  $\delta F$ , is equal to  $\mu f$ , deviation can be simply calculated when  $\mu$  is known—i.e. at a carrier disappearance point. For example, if the applied modulation has a frequency of 10 kc/s and the deviation is progressively increased until the carrier disappears, the deviation must be  $2.4 \times 10$ = 24 kc/s, and again  $5.52 \times 10 = 55.2$  kc/s.

To determine these points, apply the output of the TF 995A/5 to a narrow-band (communication) a.m. receiver and tune the latter to the unmodulated output frequency of the TF 995A/5. Set the beat oscillator of the receiver to give an audio note; then frequency modulate the Signal Generator at a fairly high frequency outside the passband of the a.m. receiver—such as 10 kc/s starting from zero deviation and increasing the deviation until the beat with the carrier disappears. At this point the actual deviation can be calculated as described above.

#### 5.8.12 THE INCREMENTAL FREQUENCY CONTROLS

(Apparatus required: Items i and j) Check that the FINE INC. FREQ. dial is positioned so that the 0 coincides with the cursor when the potentiometer wiper is at its mid-travel position. Switch to Band 2 and apply the Generator output to the Crystal Calibrator; tune, by means of the main tuning control, for a zero beat on the Calibrator. If necessary, reselect R119 so that there is no change in zero beat when C42 is short circuited; i.e. with the fine incremental frequency dial at zero, there should be zero volts on the wiper of R112.

At some convenient frequency, say 150 Mc/s, feed the output of the TF 995A/5 to the Electronic Counter and set the fine incremental frequency control to zero. Set the steps of the coarse incremental frequency control to be 20 kc/s and 40 kc/s by adjusting R153 on band 5. Repeat the procedure on Band 4, this time adjusting R150. Next, adjust R163 so that the fine incremental frequency control has a cover of 15 kc/s on bands 5 and 4 and check that its calibrations are at 1-kc/s intervals. It may be necessary to adjust R114 to obtain sufficient incremental shift.

#### 5.8.13 HIGH DEVIATION

(Apparatus required: Item h) Connect the output of the TF 995A/5 to a Deviation Meter and check that, when the TF 995A/5 is set for 9 kc/s deviation with the DEVIATION— NORMAL/HIGH switch set to NORMAL, the indication on the meter rises to approximately the following values when the DEVIATION—NORMAL/HIGH switch is set to HIGH.

BAND	RANGE	HIGH Deviation
	Mc/s	for 9 kc/s
(1)	1.5-13.5	18 kc/s
(2)	13.5-27.5	9 kc/s
(3)	27-55	18 kc/s
(4)	54-110	36 kc/s
(5)	108-220	72 kc/s

#### 5.8.14 EXTERNAL F.M.--METERING ACCURACY

(Apparatus required: Items f and h) Tune the Generator and Deviation Meter to a convenient frequency (say 20 Mc/s). Set the MOD. SELECTOR switch (S1) to EXT. MOD.—F.M. and apply 20 volts r.m.s. at 1,000 c/s from the Audio Oscillator to the EXT. MOD. and E terminals of the TF 995A/5. With the SET MOD. potentiometer (R25) turned fully clockwise, adjust the Audio Oscillator to obtain a deviation of 15 kc/s as indicated on the Deviation Meter.

Vary the audio input frequency over the range 50 c/s to 10 kc/s recording the percentage variation in true deviation and the percentage variation in input volts required from the value at 1,000 c/s to maintain the internal meter constant. The sum of these two variations at any one a.f. is not likely to exceed 10%.

#### 5.8.15 INTERNAL A.M.

#### (Apparatus required: Items g and l)

Apply the output of the TF 995A/5 to a frequency changer circuit which is followed by an i.f. amplifier and Cathode Ray Oscilloscope; the i.f. amplifier should have a centre frequency which will allow its output to be viewed directly on the c.r.o. Set the MOD. SELECTOR switch to INT. MOD.—A.M. and adjust the SET MOD. control for 30% modulation as measured on the c.r.o. screen, using the formula:—

$$M(\%) = \frac{D_{max} - D_{min}}{D_{max} + D_{min}} \times 100\%$$

where  $D_{max}$  = the peak-to-peak dimensions of the c.r.o. display.

 $D_{min}$  = the trough-to-trough dimensions of the c.r.o. display.

Hold the METER READS switch to A.M. and check that the meter reading is correct. If not, select a new value for R65.

#### 5.8.16 EXTERNAL A.M.

(Apparatus required: Items f, g, and l)

Set the MOD. SELECTOR switch (S1) to EXT. MOD.— A.M. and feed the output of the Audio Oscillator to the EXT. MOD. terminals of the TF 995A/5. Tune the Signal Generator to 20 Mc/s and view the modulation envelope as previously described. Adjust the a.f. input voltage control so that the SET MOD. potentiometer is about mid-travel when the meter indicates 30% modulation depth.

Maintaining the meter reading at 30% modulation, record the true modulation depth indicated on the cathode-ray tube. As the input frequency is varied from 100 c/s to 10 kc/s note that the change in the modulation depth does not exceed 0.5 dB.

#### 5.8.17 SPURIOUS F.M. ON C.W.

(Apparatus required: Items c and h)

To measure small amounts of spurious f.m., connect the Wave Analyser, Type TF 455 (Series), to the l.f. output of the Deviation Meter, using it as a tuned l.f. level indicator.

Note its level indication for a measured 2.5 kc/s deviation; then, since the l.f. output of the monitor

varies linearly with deviation, small amounts of f.m. may be calculated directly by noting the l.f. output level; for example, 25 c/s f.m. will give a level 40 dB below that for 2.5 kc/s.

Switch to c.w. on the MOD. SELECTOR switch and,

with the output level adjusted to the SET R.F. mark, check, at carrier frequencies of 90 and 216 Mc/s, that there is negligible frequency modulation of the signal; the spurious deviation is not likely to exceed 25 c/s.

### 6 COMPONENT LAYOUT ILLUSTRATIONS



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OM 995A/5 I-1/61



OM 995A/5 [\*-6/62

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OM 995A/5 1-1/61

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R.F. UNIT CLOSE-UP OF PORTION OF UNDERSIDE

OM 995A/5 1-1/6!

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L.F. UNIT UNDERSIDE VIEW

OM 995A/5 I-1/61





OM 995A/5 1-1/61

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## Spares Ordering Schedule

#### for F.M./A.M. SIGNAL GENERATOR TYPE TF 995A/5

When ordering replacement parts, always quote the TYPE NUMBER and SERIAL NUMBER of the instrument concerned.

To specify the individual parts required, state for each part the QUANTITY required and the appropriate SOS ITEM NUMBER.

For example, to order replacements for the 270-k $\Omega$  resistor, R4, and the 5- $\mu\mu$ F capacitor, C73, quote as follows:—

Spares for TF995A/5, Serial number 000000

1 off, SOS Item 4

1 off, SOS Item 210

It is important that the distinguishing code 'SOS' preceding each item number should not be omitted.

SOS Item No.	Circuit Ref.	Description	Works Ref.
		RESISTORS	
1	<b>R</b> 1	Composition, 470 k $\Omega$ + 20%, $\frac{1}{2}$ W.	4–TM4800/2
2	R2	Composition, $1.5 \text{ k}\Omega^*, \frac{1}{2}\text{W}$ .	58-TM4826/5
3	R3	Composition, 220 k $\Omega \pm 10\%$ , $\frac{1}{2}$ W.	18-TM4800/2
4	R4	Composition, 270 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	5-TM4800/2
5	R5	Composition, 27 k $\Omega^*$ , $\frac{1}{4}W$ .	5–TM4706
6	R6	Composition, 2.2 k $\Omega^*$ , $\frac{1}{2}$ W.	59-TM4826/5
7	R7	Wire-wound, Variable 50 k $\Omega$ + 10%, 3W.	18- <b>TM</b> 4831/2
8	<b>R</b> 8	Composition, 4.7 k $\Omega^* \pm 10\%, \frac{1}{4}W.$	146-TM4826/5
9	R9	Composition, 5.1 k $\Omega^*$ , $\frac{1}{2}W$ .	7– <b>TM</b> 4706
10	R10	Composition, $10 \text{ k}\Omega \pm 10\%$ , $\frac{1}{2}$ W.	6-TM4800/2
11	<b>R</b> 11	Composition, $12 k\Omega^*$ , $\frac{1}{4}W$ .	4-TM4706
12	R12	Composition, $4.7 \text{ k}\Omega^*$ , $\frac{1}{2}$ W.	8-TM4706
13	R13	Composition, 3.9 k $\Omega^*$ , $\frac{1}{4}$ W.	3–TM4706
14	<b>R</b> 14	Composition, $8 \cdot 2 k \Omega^*$ , $\frac{1}{2} W$ .	6-TM4706
15	R15	Composition, $4.7 \text{ k}\Omega \pm 10\%$ , $\frac{1}{4}$ W.	8-TM4800/2
16 17	R16 R18	Wire-wound, $4.7 \text{ k}\Omega \pm 5\%$ , 7W.	113-TM4826/5
18	R 10	Composition, $220 \text{ k}_{22} \pm 10\%, \frac{4}{2} \text{ W}$ .	i = 1 M4800/2
19	R20	Composition $10 k 0 \pm 50/1W$	33-1 1414820/3 62 TN4826/5
20	R21	Composition, 68 k $\Omega \pm 10\%$ , 4W.	66-TF995A/5

\* Nominal value; actual value determined during calibration.

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SOS Item No.	Circuit Ref.	Description	Works Ref.
21	R22	Composition, 68 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	66–TF995A/5
22	R23	Composition, 56 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	63–TM4826/5
23	R24	Composition, 47 k $\Omega^*$ , $\frac{1}{4}$ W.	65–TF995A/5
24	R25	Composition, Variable 20 k $\Omega \pm 20\%$ , $\frac{1}{4}$ W.	74–TF995A/5
25	R26	Composition, 15 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	64–TM4826/5
26	R27	Composition, 2.7 M $\Omega \pm 10\%$ , $\frac{1}{4}W$ .	52–TM4826/5
27	R28	Composition, 220 k $\Omega \pm 10\%$ , $\frac{1}{4}W$ .	10–TM4800/2
28	R29	Composition, 6.8 k $\Omega \pm 10\%$ , $\frac{1}{4}W$ .	65–TM4826/5
29	R30	Composition, 6.8 k $\Omega \pm 10\%$ , $\frac{1}{4}W$ . (Part of Item 266)	9–TM3900/52
30	R31	Composition, 270 k $\Omega \pm 10\%$ , $\frac{1}{4}W$ .	51–TM4826/5
31	R32	Composition, $150\Omega \pm 10\%$ , 1W.	108-TM4826/5
32	R33	Composition, $2\cdot 2 k\Omega \pm 10\%$ , $\frac{1}{4}$ W.	66-TM4826/5
33	R34	Composition, $390\Omega \pm 5\%$ , $\frac{1}{2}$ W.	11-TM4800/2
34	R35	Wire-wound, $15 k\Omega \pm 5\%$ , 7W.	112-TM4826/5
35	R36	Wire-wound, $7\cdot 5 k\Omega \pm 5\%$ , 7W.	111-TM4826/5
36	R37	Wire-wound, $5 \ k\Omega \pm 5\%$ , 7W.	110–TM4826/2
37	R38	Composition, $10\Omega \pm 10\%$ , $\frac{1}{2}$ W.	67–TF995A/5
38	R39	Wire-wound, $47 \ k\Omega^*$ , $10$ W.	110–TF995A/5
39	R40	Composition, $15 \ k\Omega \pm 10\%$ , $\frac{1}{4}$ W.	64–TM4826/5
40	R41	Composition, $6.8 \ k\Omega \pm 10\%$ , $\frac{1}{4}$ W.	65–TM4826/5
41	R42	Composition, $2 \cdot 2 \ k\Omega \pm 10\%$ , $\frac{1}{4}$ W.	66–TM4826/5
42	R43	Composition, $10 \ k\Omega \pm 10\%$ , 1W.	61–TF995A/5
43	R44	Wire-wound, Variable 200 $\ k\Omega + 200 \ k\Omega$ .	75–TF995A/5
44	R45	Composition, $68 \ k\Omega \pm 10\%$ , $\frac{1}{4}$ W.	61–TM4826/5
45	R46	Composition, $6.8 \ k\Omega \pm 10\%$ , $\frac{1}{2}$ W.	109–TM4826/5
46	R48	Composition, $2 \cdot 2 \ k\Omega \pm 10\%$ , $\frac{1}{4}$ W.	66–TM4826/5
47	R49	Wire-wound, $4 \ k\Omega \pm 5\%$ , 7W.	72–TF995A/5
48	R50	Composition, $100 \ k\Omega$ , $\frac{1}{2}$ W.	22–TM4800/5
49	R51	Composition, $4 \cdot 7 \ k\Omega \pm 10\%$ , $\frac{1}{4}$ W.	55–TM4826/5
50	R53	Composition, $270\Omega \pm 10\%$ , $\frac{1}{4}$ W.	54–TM4826/5
51	R54	Composition, 6.8 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	65–TM4826/5
52	R55	Composition, 68 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	115–TM4826/5
53	R56	Composition, 47 k $\Omega \pm 20\%$ , $\frac{1}{2}$ W.; includes L21.	TB23173/9
54	R57	Composition, 2.2 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	66–TM4826/5
55	R58	Composition, 100 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	68–TM4826/5

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SOS Item No.	Circuit Ref.	Description	Works Ref.
56	R59	Composition, 6.8 k $\Omega \pm 10\%$ , $\frac{1}{2}$ W.	65–TM4826/5
57	<b>R60</b>	Composition, $100 \text{ k}\Omega \pm 10\%$ , $\frac{1}{4}$ W.	50-TM4826/5
58	R61	Composition, 2.2 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	66–TM4826/5
59	R62	Composition, 33 k $\Omega \pm 20\%$ , $\frac{1}{2}$ W.; includes L19.	TB23173/10
60	R63	Composition, 39 k $\Omega^*$ , $\frac{1}{4}$ W.	78–TF995A/5
61	R64	Composition. 120 k $\Omega$ + 10%, $\frac{1}{4}$ W.	58-TF995A/5
62	R65	Composition, 33 k $\Omega^*$ , $\frac{1}{4}$ W.	73–TF995A/5
63	R66	Composition, 33 k $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	64-TF995A/5
64	R67	Composition, $470\Omega \pm 10\%$ , $\frac{1}{4}$ W.	63-TF995A/5
65	R68	Composition, $4.7 \text{ k}\Omega \pm 10\%$ , $\frac{1}{4}$ W.	62-TF995A/5
66	R 69	Composition $1 M\Omega + 10\%$ $W$ .	59-TF995A/5
67	R70	Composition, $2.7 \text{ k}\Omega^*$ , $\frac{1}{4}\text{ W}$ .	71–TF995A/5
68	R71	Composition, $1 k\Omega + 10\%$ , $\frac{1}{2}W$ .	39–TM4297A
69	R72	Composition, $1 k\Omega + 10\%$ , $\frac{1}{4}W$ .	39-TM4297A
70	R73	Carbon, High Stability, $82.5 \text{ k}\Omega \pm 1\%, \frac{1}{8}\text{W}.$	36-TM4297A
71	<b>P</b> 74	Carbon High Stability 742.0 $\pm$ 1% 1W	35_TM4297A
72	R75	Carbon, High Stability, $742.0 \pm 1\%$ , $8W$ .	35-TM4297A
73	R76	Carbon, High Stability, $742\Omega \pm 1\%$ , $8W$ .	35-TM4297A
74	R77	Carbon, High Stability, $742\Omega \pm 1\%$ , $\frac{1}{2}W$ .	35–TM4297A
75	R78	Carbon, High Stability, $220\Omega \pm 1\%$ , $\frac{1}{8}W$ .	38-TM4297A
76	<b>D</b> 70	Carbon High Stability 01.60 + 19/ 1W	27 . T.M.4207.4
70	R/9 R80	Carbon, High Stability, 91.60 $\pm$ 1% $\frac{1}{2}$ W	37 - 1 M 4297A 37 - T M 4297A
78	R81	Carbon, High Stability 91.60 $\pm$ 1% $\frac{1}{60}$	37–TM4297A
79	R81 R82	Carbon, High Stability, $91032 \pm 17_0$ , gW.	36-TM4297A
80	R83	Carbon, High Stability, $17.9\Omega \pm 1\%$ , $\frac{1}{8}W$ .	24–TM4298/2
01	<b>D</b> 04	Contract Web State 17.00 + 10/ 1W	24 TM4209/2
81 82	K84	Carbon, High Stability, $17.9\Omega \pm 1\%$ , $\frac{1}{8}W$ .	24-1 M4298/2
82 83	KOJ Doc	Carbon, High Stability, $1792 \pm 1\%$ , $\frac{1}{6}$ , $\frac{1}{8}$ W.	24-1 N14298/2 24. TN14298/2
03 84	KÖÖ D 97	Carbon, fligh Stability, $17.94 \pm 1\%$ , $\frac{3}{8}$ W.	24-1 1414290/2 24_TN14208/2
85	R 8 8	Carbon, High Stability $17.932 \pm 1.70$ , g w.	24-TM2708/2
05	1000	Current, fight statistics, $1.722 \pm 1.70$ , $8.77$ .	2, 11,11,70,2
86	R89	Carbon, High Stability, $17.9\Omega \pm 1\%$ , $\frac{1}{8}W$ .	24-TM4298/2
87	R90	Carbon, High Stability, $17.9\Omega \pm 1\%$ , $\frac{1}{8}W$ .	24–TM4298/2
88	R91	Carbon, High Stability, $17.9\Omega \pm 1\%$ , $\frac{1}{8}W$ .	24-TM4298/2
89	R92	Carbon, High Stability, $17.9\Omega \pm 1\%$ , $\frac{1}{8}W$ .	24-TM4298/2
90	<b>R9</b> 3	Carbon, High Stability, $61.2\Omega \pm 1\%$ , $\frac{1}{8}W$ .	28-1M4298/2

SOS Item No.	Circuit Ref.	Description	Works Ref.
91	R94	Carbon, High Stability, $332\Omega \pm 1\%$ , $\frac{1}{8}W$ .	26–TM4298/2
92	R95	Carbon, High Stability, $167\Omega \pm 1\%$ , $\frac{1}{8}W$ .	27–TM4298/2
93	R96	Carbon, High Stability, $167\Omega \pm 1\%$ , $\frac{1}{8}W$ .	27–TM4298/2
94	R97	Carbon, High Stability, $167\Omega \pm 1\%$ , $\frac{1}{8}W$ .	27–TM4298/2
95	R98	Carbon, High Stability, $167\Omega \pm 1\%$ , $\frac{1}{8}W$ .	27–TM4298/2
96	R99	Carbon, High Stability, $37.5\Omega \pm 1\%$ , $\frac{1}{8}W$ .	25–TM4298/2
97	R100	Carbon, High Stability, $90\Omega \pm 2\%$ , $\frac{1}{8}W$ .	16–TM5552
98	R101	Carbon, High Stability, $90\Omega \pm 2\%$ , $\frac{1}{8}W$ .	16–TM5552
99	R102	Carbon, High Stability, $360\Omega \pm 1\%$ , $\frac{1}{8}W$ .	17–TM5552
100	R103	Carbon, High Stability, $37.5\Omega \pm 5\%$ , $\frac{1}{8}W$ .	10–TM5551
101	R104	Carbon, High Stability, $75\Omega \pm 5\%$ , $\frac{1}{8}W$ .	11-TM5551
102	R105	Carbon, High Stability, $14\cdot 5\Omega \pm 5\%$ , $\frac{1}{8}W$ .	12-TM5551
103	R106	Composition, $560\Omega \pm 10\%$ , $\frac{1}{4}W$ .	77-TF995A/5
104	R107	Composition, $22 k\Omega \pm 10\%$ , $\frac{1}{4}W$ .	69-TM4826/5
105	R109	Composition, $2\cdot 2 k\Omega \pm 10\%$ , $\frac{1}{4}W$ .	69-TF995A/5
106	R110	Composition, $100\Omega \pm 10\%$ , $\frac{1}{4}W$ . (Part of Item 266)	10–TM3900/52
107	R111	Composition, $10 k\Omega \pm 10\%$ , $\frac{1}{4}W$ .	57–TM4826/5
108	R112	Wire-wound, Variable $20 k\Omega \pm 10\%$ , $2W$ .	81–TF995A/5
109	R113	Composition, $68 k\Omega \pm 10\%$ , $\frac{1}{2}W$ .	23–TM4800/2
110	R114	Composition, $100 k\Omega^* \pm 10\%$ , $\frac{1}{2}W$ .	145–TM4826/5
111	R115	Composition, $1 \text{ k}\Omega \pm 10\%$ , $\frac{1}{4}\text{W}$ .	147–TM4826/5
112	R116	Composition, $330\Omega$ , $\frac{1}{4}\text{W}$ .	60–TM4826/5
113	R117	Composition, $2 \cdot 2 \text{ k}\Omega \pm 10\%$ , $\frac{1}{4}\text{W}$ .	36–TM4299/2
114	R118	Composition, $22 \text{ k}\Omega \pm 10\%$ , $\frac{1}{2}\text{W}$ .	43–TM4299/2
115	R119	Composition, $68 \text{ k}\Omega^* \pm 10\%$ , $\frac{1}{4}\text{W}$ .	34–TM4299/2
116	R120	Composition, $33 \text{ k}\Omega \pm 10\%$ , $\frac{1}{4}\text{W}$ .	35-TM4299/2
117	R121	Wire-wound, $950\Omega \pm 10\%$ , $1\text{W}$ .	82-TF995A/5
118	R122	Composition, $33 \text{ k}\Omega \pm 10\%$ , $\frac{1}{2}\text{W}$ .	44-TM4299/2
119a	R123	Composition, $68 \text{ k}\Omega \pm 10\%$ , $\frac{1}{4}\text{W}$ .	66-TF995A/5
120	R124	Wire-wound, Variable $5 \text{ k}\Omega$ .	134-TF995A/5
121	R125	Composition, $2 \cdot 2 \ k\Omega \pm 10\%$ , $\frac{1}{4}W$ .	135–TF995A/5
122	R126	Composition, $1 \ M\Omega \pm 10\%$ , $\frac{1}{4}W$ .	59–TF995A/5
123	R150	Composition, 560 $k\Omega^*$ , $\frac{1}{4}W$ .	14A–TM4943BR
124	R151	Composition, 120 $k\Omega \pm 2\%$ , $\frac{1}{2}W$ .	14–TM4943BR
125	R152	Composition, 430 $k\Omega \pm 2\%$ , $\frac{1}{2}W$ .	12–TM4943BR

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#### SECTION 7

SOS Item No.	Circuit Ref.	Description	Works Ref.
126	R153	Composition, 3.3 M $\Omega^*$ , $\frac{1}{4}W$ .	12A-TM4943BR
127	R154	Composition, $10 \text{ k}\Omega \pm 1\%$ , $\frac{1}{4}$ W.	121–TF995A/5
128	R155	Composition, 10 k $\Omega \pm 1\%$ , $\frac{1}{4}$ W.	121–TF995A/5
129	R156	Composition, $10 \text{ k}\Omega \pm 1\%$ , $\frac{1}{4}$ W.	121–TF995A/5
130	R157	Composition, $10 \text{ k}\Omega \pm 1\%$ , $\frac{1}{4}$ W.	121–TF995A/5
131	<b>R</b> 158	Carbon, High Stability, 10 k $\Omega \pm 1\%$ , $\frac{1}{4}$ W.	121–TF995A/5
132	R159	Carbon, High Stability, 10 k $\Omega \pm 1\%$ , $\frac{1}{4}$ W.	121–TF995A/5
133	<b>R</b> 160	Carbon, High Stability, 10 k $\Omega \pm 1\%$ , $\frac{1}{4}$ W.	121–TF995A/5
134	<b>R161</b>	Carbon, High Stability, $10 \text{ k}\Omega + 1\%$ , $\frac{1}{4}$ W.	121–TF995A/5
135	R162	Wire-wound, Variable, $25 \text{ k}\Omega$ , $3W$ .	116-TF995A/5
136	<b>R</b> 163	Composition, 56 k $\Omega^*$ , $\frac{1}{4}$ W.	122-TF995A/5
137	R164	Composition, $100 \text{ k}\Omega \pm 10\%$ , $\frac{1}{2}$ W.	137–TF995A/5
138	R165	Composition, $470\Omega + 10\%$ , $\frac{1}{4}W$ .	63-TF995A/5
139	R166	Composition, $10 \text{ k}\Omega + 10\%$ , $\frac{1}{4}$ W.	136–TF995Å/5
140	R167	Carbon, High Stability, $10 \text{ k}\Omega \pm 5\%$ , $\frac{1}{4}W$ .	138-TF995A/5
141	R168	Composition, 1 M $\Omega \pm 10\%$ , $\frac{1}{4}$ W.	15-TM4943BR

\* Nominal value; actual value determined during calibration.

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SOS Item No.	Circuit Ref.	Description	Works Ref.			
CAPACITORS						
142	Cl	Paper, $0.1 \ \mu F + 20\%$ , 350 V d.c.	3-TM4800/2			
143	C2	Paper, 0.1 $\mu$ F $\pm$ 20%, 350 V d.c.	17-TM4800/2			
144	C3	Mica, Special Assembly, 100 µµF, Nominal.	2–TM4826/5			
145	C4	Mica, 100 $\mu\mu$ F $\pm$ 10%, 350 V d.c.	117-TM4826/5			
146	C5	Mica, 100 $\mu\mu$ F $\pm$ 10%, 350 V d.c.	117– <b>TM</b> 4826/5			
147	C6	Paper, 0.02 μF*, 350 V d.c.	12-TM480022			
148	C7	Ceramic, 22 $\mu\mu F \pm 20\%$ , 500 V d.c.	71-TM4826/5			
149	C8	Mica, 100 $\mu\mu$ F $\pm$ 10%, 350 V d.c.	95-TF995A/5			
150	C9	Mica, 100 $\mu\mu$ F $\pm$ 20%, 350 V d.c.	86-TF995A/5			
151	C10	Mica, Special Assembly, 100 $\mu\mu$ F, Nominal.	2-TM4826/5			
152	C12	Mica, Special Assembly, 100 µµF, Nominal.	2-TM4826/5			
153	C13	Mica, 100 $\mu\mu$ F $\pm$ 10%, 350 V d.c.	117– <b>TM4</b> 826/5			
154	C14	Paper, 2 $\mu$ F $\pm$ 25%, 250 V d.c.	87-TF995A/5			
155	C15	Paper, 0.01 $\mu$ F $\pm$ 20%, 400 V d.c.	13-TM4800/2			
156	C16	Paper, 0.01 $\mu$ F $\pm$ 25%, 400 V d.c.	151 <b>M</b> 4800/2			
157	C17	Paper, 0.1 $\mu$ F $\pm$ 20%, 350 V d.c.	14-TM4800/2			
158	C18	Paper, 0.1 $\mu$ F $\pm$ 20%, 350 V d.c.	16–TM4800/2			
159	C19	Mica, Special Assembly, 100 $\mu\mu$ F, Nominal.	3-TM4826/5			
160	C20	Ceramic, 0.01 $\mu$ F $\pm 20\%$ .	135–TM4826/5			
161	C21	Ceramic, 0.001 $\mu$ F ± 20%, 400 V d.c. (Included in Item 247)	12–1 <sup>M3900/75</sup>			
162	C22	Mica, Special Assembly, 100 $\mu\mu$ F, Nominal. (Included in Item 247)	9-TM3900/75			
163	C23	Mica. $100 \mu\mu F + 10\%$ . 350 V d.c.	20-TM3900/75			
164	C24	Paper, 0.001 $\mu$ F + 20%, 600 V d.c.	91-TM4826/5			
165	C25	Mica, $39 \ \mu\mu F \pm 5\%$ , 750 V d.c.	85-TM4826/5			
166	C26	Paper, 0.1 $\mu$ F $\pm$ 20%, 350 V d.c.	78–TM4826/5			
167	C27	Paper, 0.001 $\mu$ F $\pm$ 20%, 600 V d.c.	91-TM4826/5			
168	C28	Paper, 0.01 $\mu$ F $\pm$ 20%, 350 V d.c.	83-TM4826/5			
169	C29	Mica, 47 $\mu\mu$ F $\pm$ 20%, 350 V d.c. (Included in Item 248)	9-TM3900/74			
170	C30	Ceramic, 10 $\mu\mu$ F* $\pm$ 20%, 500 V d.c.	89-TM4826/5			
171	C31	Ceramic, 100 $\mu\mu$ F $\pm$ 5%, 500 V d.c.	88-TM4826/5			

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#### SECTION 7

SOS Item No.	Circuit Ref.	Description	Works Ref.
172	C32	Paper, 2 $\mu$ F $\pm$ 25%, 150 V d.c.	151-TM4826/5
173 174	C33	Two-section ganged capacitor complete with trimmers; includes C34, C35, C46 and C47.	82-1 M4820/3 TC21478/1
175	C34	Air, Variable, 14–200 $\mu\mu$ F, part of Item 174.	
176	C35	Air, Trimmer, 3-30 µµF, part of Item 174.	
177	C36	Ceramic, 47 $\mu\mu$ F $\pm$ 20%, 500 V d.c.	76–TM4826/5
178	C37	Paper, 0.1 $\mu$ F $\pm 20\%$ , 350 V d.c.	9-TM4800/2
179	C38	Ceramic, $100 \ \mu\mu F - 0\%$ , $+100\%$ , $500 \ V \ d.c.$	84-TM4826/5
180	C39	Paper, 0.01 $\mu$ F $\pm$ 20%, 350 V d.c.	11– <b>TM3900/52</b>
181	C40	Air, Trimmer. $1.25-10 \ \mu\mu F$ .	116–TM4826/5
182	C41	Ceramic, $3.3 \ \mu\mu F^* \pm 10\%$ , 500 V d.c.	75TM4826/5
183	C42	Ceramic, 4700 $\mu\mu$ F -0 + 100%, 500 V d.c.	92–1 <sup>°</sup> M4826/5
184	C43	Ceramic, 5 $\mu\mu$ F $\pm$ 20%, 750 V d.c.	134–TM4826/5
185	C44	Ceramic, 10 $\mu\mu$ F $\pm$ 10%, 750 V d.c.	77–TM4826/5
186	C45	Paper, 0.5 $\mu$ F $\pm$ 25%, 150 V d.c.	150-TM4826/5
	C46	Air, Variable, 7–100 $\mu\mu$ F, part of Item 174.	
107	C47	Air, Trimmer, 2–8 $\mu\mu$ F, part of Item 174.	04 3344004/5
187	C48	Ceramic, 100 $\mu\mu$ F $-0\%$ , + 100\%, 500 V d.c.	84-1 M4826/5
100	C49	Ceramic, $22 \ \mu\mu F \pm 20\%$ , 500 v d.c.	87–1M4820/5
189	C50	Ceramic, 47 $\mu\mu$ F $\pm$ 20%, 500 V d.c.	73-TM4826/5
190	C51	Mica, 100 $\mu\mu F \pm 10\%$ , 350 V d.c.	117-TM4826/5
191	C52	Mica, Special Assembly, 100 $\mu\mu$ F, Nominal.	4-TM4826/5
192 193	C53 C54	Electrolytic, 8 $\mu$ F -20% + 50%, 150 V d.c. Paper, 0·1 $\mu$ F $\pm$ 25%, 250 V d.c.	103-TF995A/5 93-TF995A/5
194	C 55	Ceramic 33 $\mu$ = $\pm 20\%$ 500 V d c	72 TM4826/5
195	C56	Mica 100 $\mu_{\rm W} E \pm 10\%$ 350 V d c	117 - TM4826/5
196	C57	Mica, Special Assembly, 100 uuF Nominal	124-127-TM4826/5
197	C58	Electrolytic. 8 $\mu$ F -20% + 50%. 450 V d.c.	33-TM4299/2
198	C59	Air, Trimmer, $1.25-10 \ \mu\mu$ F.	116-TM4826/5
199	C60	Ceramic Stand-off, 820 $\mu$ uF + 20% 750 V d c	79- <b>TM</b> 4826/5
200	C61	Ceramic, $5 \mu\mu F + 20\%$ , 500 V d.c.	118-TM4826/5
201	C62	Electrolytic, $30 \ \mu F - 20\% + 50\%$ , 350 V d.c.	13–TM4299/2
202	C63	Paper, 0.01 $\mu$ F $\pm$ 20%, 350 V d.c.	83-TM4826/5
203	C64	Ceramic, 100 $\mu\mu$ F $\pm$ 10%, 500 V d.c.	81-TM4826/5

\* Nominal value; actual value determined during calibration.

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\* Nominal value; actual value determined during calibration.

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SOS Item No.	Circuit Ref.	Description	Works Ref.

#### SECTION 7

SOS Item No.	Circuit Description Ref.		Works Ref.	
		INDUCTORS		
243	L1	R.F. Filter Inductor.	TM4087/14	
244	L2	R.F. Filter Inductor.	TM4087/14	
245	L3	R.F. Inductor.	TB16363/27	
246	L4	R.F. Filter Inductor.	TM4087/14	
247	16	Main portion of three-section filter assembly; includes L6 and L7, and Items 161 and 162. R.E. Eilter Inductor: part of Item 247	ТМ3900/75	
	L7	R.F. Filter Inductor; part of Item 247.		
248	L8	Screened R.F. Inductor Assembly; includes Item 169.	TM3900/74	
249	L9	Modulation Choke.	TM4159/1	
250	L10	30-Mc/s Oscillator Inductor.	TB23173/1	
251	L11	Screened R.F. Inductor Assembly.	TM4087/14	
252	L14	R.F. Inductor.	TB23173/3	
253	L15	R.F. Inductor.	TB23173/4	
254	L16	H.T. Smoothing Choke.	TM5172/31	
255	L17	H.T. Smoothing Choke.	TM5172/31	
256	L18	Multiplier Tuning Inductor, 27–55 Mc/s.	TA22011	
257	L19	R.F. Inductor; part of Item 59.	TB23173/10	
258	L21	R.F. Inductor; part of Item 53.	TB23173/9	
259	L22	Multiplier Tuning Inductor, 54-110 Mc/s.	TB20309/1	
260	L23	Multiplier Tuning Inductor, 108–220 Mc/s.	TE23048/11	
261	L24	R.F. Inductor (mains filter).	TB22722/21	
262	L25	R.F. Inductor (mains filter).	TB22722/21	
767	1.26	Filter Inductor	TR23173/30	

#### TRANSFORMERS

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264	T1	A.F. Oscillator Transformer.	TM4085/2
265	T2	Master Oscillator R.F. Transformer, 4.5–9 Mc/s.	TM3900/95
266	Т3	Multiplier R.F. Transformer, 13.5–27 Mc/s. (Includes Items 29 and 106)	TM3900/52
267	Τ4	Mains Transformer.	TM5150/25
268	T5	R.F. Output Transformer, 2–13.5 Mc/s.	TB23173/5

SOS Item No.	Circuit Ref.	Circuit Description Ref.	
		SWITCHES	
269	<b>S</b> 1	Rotary, 8 pole, 5 position, 4 wafer.	TC4428/373
270	S2	Rotary, 10 pole, 5 position, 4 wafer.	TC4428/475
271	<b>S</b> 3	Lever-Actuated Rotary, 2 pole, 3 position, 2 wafer, biased to mid-position; includes bakelite handle.	TC4428/342
272	S4	Toggle, 2 pole, 2 position.	TB23903/2
273	S5	Rotary, 2 pole, 2 position, single wafer.	96-TM4826/5
274	<b>S</b> 6	Rotary, 4 pole, 2 position, single active wafer, with extra dummy wafer	TC4428/344
275	S10	Rotary, 2 pole, 5 position, 1 wafer.	117-TF995A/5
276	S11	Toggle, 2 pole, 2 position.	TB23903/2
277	S12	Rotary, 2 pole, 3 position, 2 wafer.	118-TF995A/5

#### VALVES, VALVE HOLDERS, AND RETAINERS

278	V1	6AK6, Pentode.	47–TF995A/5
279		Holder, for V1.	TB26904/2
280		Retainer, for V1.	PC17501/2
281	V2	6AK5, Pentode.	101–TM4826/5
282		Holder, for V2.	TB26904/2
283		Retainer, for V2.	PC17501/2
284	V3	EF86, Pentode.	163–TM4826/5
285		Holder, for V3.	TB26902/2
286		Retainer, for V3.	PC17502/2
287	V4	6AK5, Pentode.	101–TM4826/5
288		Holder, for V4.	TB26904
289		Retainer, for V4.	PC17501/1
290	¥5	6AU6, Pentode.	49–TF995A/5
291		Holder, for V5.	60-TF995A/5
292		Retainer, for V5.	57-TF995A/5
293	V6	6AK5, Pentode.	101–TM4826/5
294		Holder, for V6.	TB26904
295		Retainer, for V6.	PC17502/2

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SOS Item No.	Circuit Ref.	Description	Works Ref.
296	V7	12AT7, Double Triode.	103–TM4826/5
297		Holder, for V7.	TB26905/2
298		Retainer, for V7.	PC17502/2
299	V8	6AK5, Pentode.	101–TM4826/5
300		Holder, for V8.	TB26904
301		Retainer, for V8.	PC17502/2
302	V9	OA2, Voltage Stabilizer.	48-TF995A/5
303		Holder, for V9.	TB26904/2
304		Retainer, for V9.	PC17501/2
305	V10	6AK5, Pentode.	101–TM4826/5
306		Holder, for V10.	TB26904
307		Retainer, for V10.	PC17501/1
308	V11	5Z4G, Full-Wave Rectifier.	16–TM4299/2
309		Holder, for V11.	PC81814/1
310		Retainer, for V11.	TC22774/12
311	V12	6AK5, Pentode.	101–TM4826/5
312		Holder, for V12.	TB26904
313		Retainer, for V12.	PC17501/1
314	V13	12AT7, Double Triode.	46-TF995A/5
315		Holder, for V13.	TB26902/2
316		Retainer, for V13.	PC17502/2
317	V14	5651, Voltage Stabilizer.	20-TM4299/2
318		Holder, for V14.	TB26904/2
319		Retainer, for V14.	PC17501/2
320	V15	6AL5, Double Diode.	21–TM4299/2
321		Holder, for V15.	TB26904/2
322		Retainer, for V15.	PC17501/2

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SOS Item No.	Circuit Ref.	Description	Works Ref.		
		CRYSTALS			
323 324 325	X1 Quartz Oscillator Crystal, 333·33 kc/s. Holder, for X1. Retainer, for X1.				
326 327 328	X2 X3	CS2A, Shicon Rectifier. Retaining Contact, for X2. CV425, Germanium Diode	44–1M4297/A TD27378/1 7A–TM4943BR		
329	X4	CV425, Germanium Diode.	6A-TM4943BR		
		LAMP			
330 331	PLP1	Pilot Lamp, 6.5 V, 0.3 A, M.E.S. Pilot Lamp Holder, with Red Lens.	43–TF995A/5 42–TF995A/5		
		FUSES AND HOLDERS			
331/1 331/2 331/3 331/4	FS1 FS2/FS3 FS2/FS3	<ul><li>150-mA cartridge fuse.</li><li>2-amp cartridge fuses.</li><li>3-amp cartridge fuses (for use on 100 to 150 volts ranges only).</li><li>Holder, for cartridge fuses.</li></ul>	57-TM4299/2 58-TM4299/2 59-TM4299/2		
		METER			
332	M1	0–100 $\mu$ A, Moving Coil, including clamping brackets.	TM3970/73		
		PLUGS, SOCKETS, AND CONNECTING LEADS			
333 334 335	PL1 SKT1	Plug, 6-way. Socket, 6-way. Mains Lead comprising 6-ft, 3-core Flexible Cable and 3-pin	18–TM4299/2 55–TF995A/5 TM2560AQ		
336 337		75Ω Type BNC Socket, coaxial, fixed. 75Ω Type BNC Socket, coaxial, fixed.	30-TM4298/1 6-TM5551		
338 339		50 $\Omega$ Type BNC Socket, coaxial, fixed. 75 $\Omega$ Type BNC Plug (modified), coaxial, fixed.	7–TM5551 8–TM5551 TC27665 TB26997/1		
340 341 342	J1	R.F. Output Cable, coaxial, 4 ft 6 in; includes Item 336. CRYSTAL CHECK Jack, including Telephone Plug. Bush, for Item 341.	38-TM4298/1 54-TF995A/5 TA19742		

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SOS Item Circuit Description No. Ref.		Description	Works Ref.	
		KNOBS, DRIVES, AND DIALS		
343		Knobs, for TUNE and INC. FREQ. controls.	TB29569	
344		COARSE TUNE control dial.	TB4691A/18	
345		FINE TUNE control dial.	TB28875	
346		COARSE INC. FREQ. control dial.	TB26194	
347		FINE INC. FREQ. control dial.	TD27529/5	
348		FREQUENCY DIAL. Pre-calibrated.	TB23189	
349		Dial Escutcheon Mounting Ring.	TD20670/2	
350		Dial Escutcheon (Chromium Plated), with Rubber Tubing.	TD20670/1	
351		Gasket, to fit over Item 349.	8-TM4357/2	
352		Window, including Movable Cursor Assembly, to fit in Item 350.	TC20735/2 TD20670/3 TA20726 TB6775/300	
252		Nulan Duiyo Cond	10 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	
353 354		Knob, for set mod. freq. switch, S12.	TB25460	
355		Knob, for MOD, SELECTOR switch, S1.	TB25460/2	
356		Knob, for RANGE MC/S switch, S2.	TB25460/2	
357		Knob, for deviation—normal/high switch, S5.	TB25460/2	
358		Knob, for deviation range switch, S6.	TB25460/2	
359		Knob, for OUTPUT VOLTAGE attenuator.	TB17848/3	
360		Knob, for MULTIPLY BY attenuator.	TB17848/3	
361		Knob, for set CARRIER control, R44.	TB23920/1	
362	62 Knob, for SET MOD. control, R25.			

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SOS Item No.	Circuit Description Ref.		Works Ref.
		MISCELLANEOUS	
363		Cover Plate, for R.F. Output Cable exit, in Right-Hand Handle Recess.	TA19721
364		Grommet, to fit in Item 363.	TA6515/1
365		Cable Saddle, to secure Item 340 to Item 363.	29-TF995A/5
366		Front Panel.	TD22009/5
367		Set of Eight Screws, complete with Black Fibre Washers for fixing Front Panel to case.	30–TF995A/5 TB6775/183
368		Terminal. EXT. MOD.	TB24330/5
369		Terminal, sync.	TB24330/5
370		Terminal, EARTH.	TB24330/5
371		Case Assembly complete with Handles and Feet.	TM4310 TC17659
372		Handle Escutcheon. Two included in Item 371.	TA11420 TC17659
272		Casa Foot Four included in Item 271	TA 11420
374 374		20-dB Step Attenuator Assembly; includes Items 68 to 79 inclusive, 223, 224, 225, 326, and 327	TM4297A
375		2-dB Step Attenuator Assembly; includes Items 80 to 96 inclusive.	TM4298
376		20-dB ATTENUATOR PAD; includes Items 97 to 99 inclusive, and Items 298 and 300.	TM5552
377		52- and 75-ohm TERMINATING UNIT; includes Items 100 to 102 inclusive, and Items 337 to 339 inclusive.	TM5551
378		R.F. Unit Screening Cover.	26-TM4826/5
379		Contact Spring for earthing R.F. Unit Screening Cover.	TC-20321/3E
380		Set of three Hexagonal Wrenches for Socket Set Screws, sizes 2, 4, and 6BA; complete in linen bag.	104-TF995A/2
381		Operating and Maintenance Handbook.	OM995A/5

## Decibel Conversion Table

Ratio Down				Ratio Up	
VOLTAGE	POWER	DECIBELS	VOLTAGE	POWER	
1·0	1-0	0	1.0	1.0	
·9886	-9772	-1	1.012	1.023	
·9772	-9550	-2	1.023	1.047	
·9661	-9333	-3	1.035	1.072	
·9550	-9120	-4	1.047	1.096	
·9441	-8913	-5	1.059	1.122	
·9333	-8710	·6	1.072	1.148	
·9226	-8511	·7	1.084	1.175	
·9120	-8318	·8	1.096	1.202	
·9016	-8128	·9	1.109	1.230	
·8913	-7943	I·0	1.122	1.259	
-8710	-7586	·2	1·148	1·318	
-8511	-7244	·4	1·175	1·380	
-8318	-6918	·6	1·202	1·445	
-8128	-6607	·8	1·230	1·514	
-7943	-6310	2·0	1·259	1·585	
·7762	-6026	2·2	1·288	1·660	
·7586	-5754	2·4	1·318	1·738	
·7413	-5495	2·6	1·349	1·820	
·7244	-5248	2·8	1·380	1·905	
·7079	-5012	3·0	1·413	1·995	
·6683	-4467	3-5	1-496	2·239	
·6310	-3981	4-0	1-585	2·512	
·5957	-3548	4-5	1-679	2·818	
·5623	-3162	5-0	1-778	3·162	
·5309	-2818	5-5	1-884	3·548	
·5012	·2512	6	1·995	3·981	
·4467	·1995	7	2·239	5·012	
·3981	·1585	8	2·512	6·310	
·3548	·1259	9	2·818	7·943	
·3162	·1000	10	3·162	10·000	
·2818	·07943		3·548	12-59	
·2512	·06310	2	3·981	15-85	
·2239	·05012	3	4·467	19-95	
·1995	·03981	4	5·012	25-12	
·1778	·03162	5	5·623	31-62	

#### DECIBEL CONVERSION TABLE

Ratio Down			Ratio Up		
VOLTAGE	POWER	DECIBELS	VOLTAGE	POWER	
·1585	·02512	16	6.310	39-81	
.1413	·01995	17	7.079	50.12	
.1259	-01.585	18	7.943	63.10	
·1122	01259	19	8.913	79.43	
·1000	·01000	20	10-000	100.00	
·07943	·006310	22	12-59	158-5	
-06310	·003981	24	15-85	251.2	
·05012	·002512	26	19.95	398-1	
·03981	·001585	28	25.12	631·0	
·03162	-001000	30	31.62	1,000	
·02512	·0006310	32	39-81	1,585	
·01995	·0003981	34	50-12	2,512	
·01585	·0002512	36	63-10	3,981	
-01259	·0001585	38	79-43	6,310	
·01000	-0001000	40	100.00	10,000	
·007943	.00006310	42	125.9	15,850	
·006310	·00003981	44	158-5	25,120	
·005012	·00002512	46	199-5	39,810	
·003981	·00001585	48	251.2	63,100	
·003162	-00001000	50	316-2	100,000	
·002512	6·310 × 10 <sup>-6</sup>	52	398-1	158,500	
·001995	3·981 × 10 <sup>-</sup>	54	501-2	251,200	
·001585	2·512 × 10 <sup>-</sup> °	56	631.0	398,100	
·001259	1·585 × 10 <sup>-</sup> °	58	794.3	631,000	
·001000	10⊸	60	1,000	10*	
·0005623	3·162 × 10⁻ <sup>7</sup>	65	1,778	$3.162 imes10^{6}$	
·0003162	· 10 <sup>-7</sup>	70	3,162	107	
·0001778	$3.162 imes10^{-8}$	75	5,623	$3.162 imes10^{7}$	
·0001000	10 <del>-</del> 8	80	10,000	10 <sup>8</sup>	
·00005623	3·162 × 10⁻⁰	85	17,780	3·162 × 10⁵	
·00003162	10-°	90	31,620	10'	
·00001000	10 <sup>-10</sup>	100	100,000	10 <sup>10</sup>	
3·162 × 10 <sup>-</sup>	10-11	110	316,200	10"	
10-	10-12	120	106	1012	
3·162 × 10⁻²	10-13	130	$3.162 imes10^{6}$	10 <sup>13</sup>	
10 <sup>-7</sup>	10-14	140	10 <sup>7</sup>	10'*	

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### CIRCUIT DIAGRAMS



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